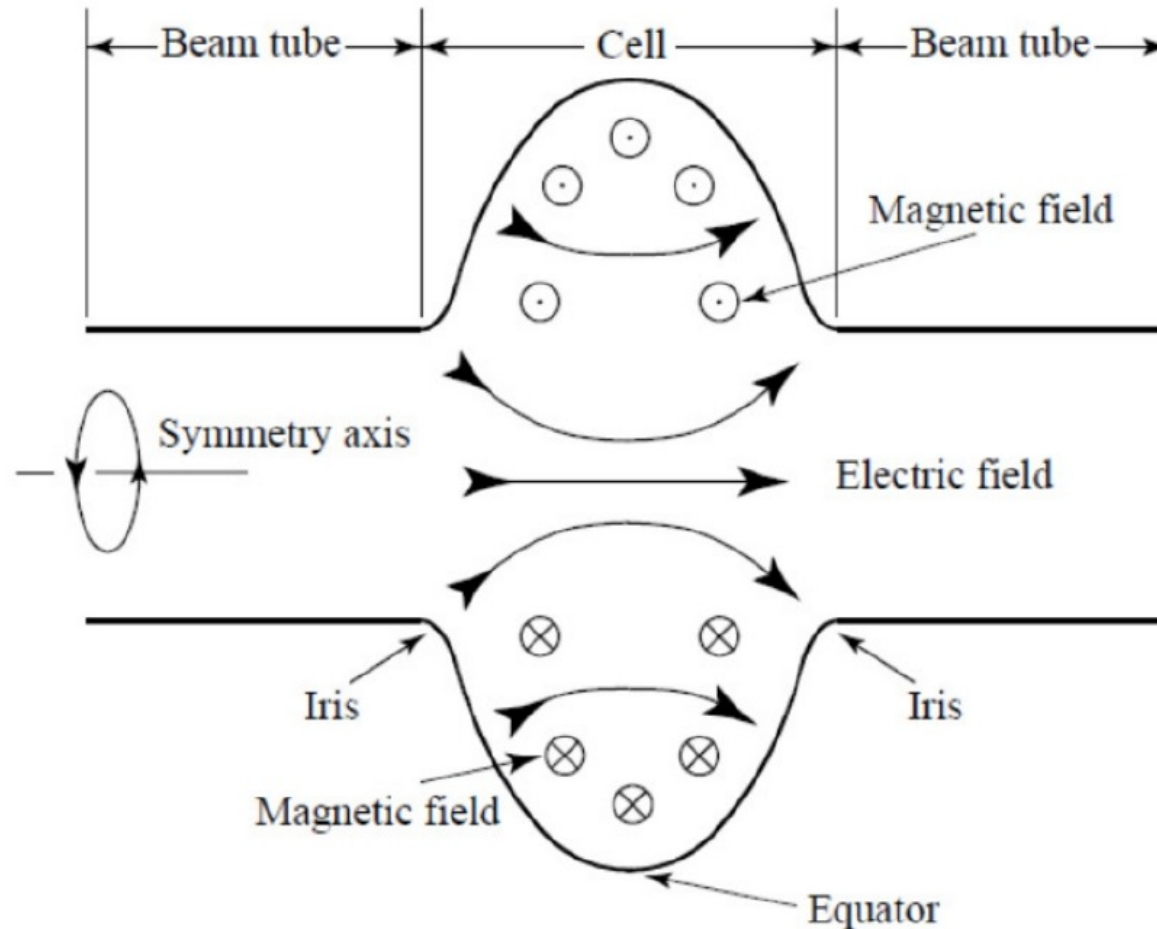


Fundamentals of Accelerator Physics

Lecture 9: Introduction to RF Accelerators

Jun Ma

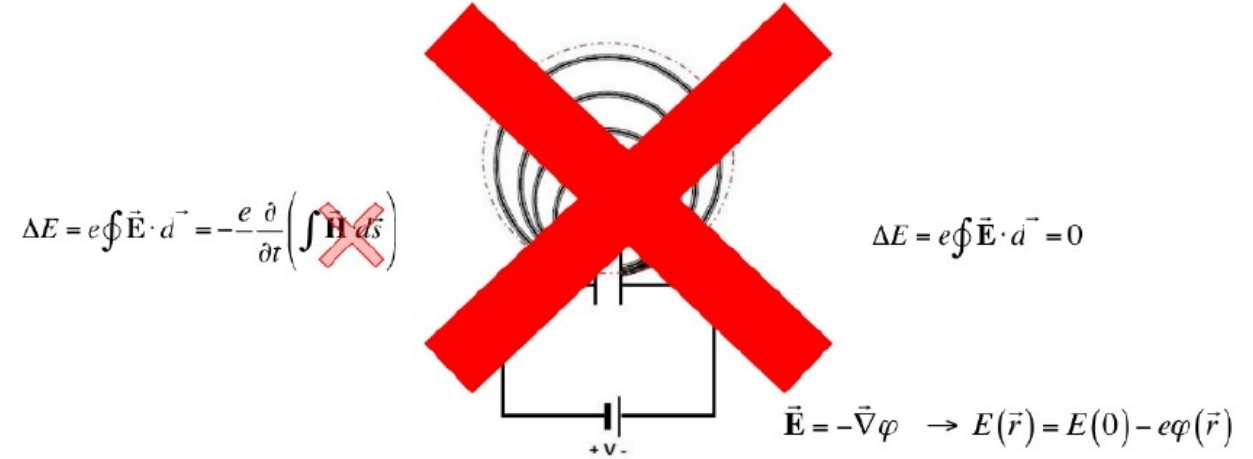


Electrostatic acceleration: what is the limit?

- ▶ In a static electric field, the energy gain is determined by the potential difference:

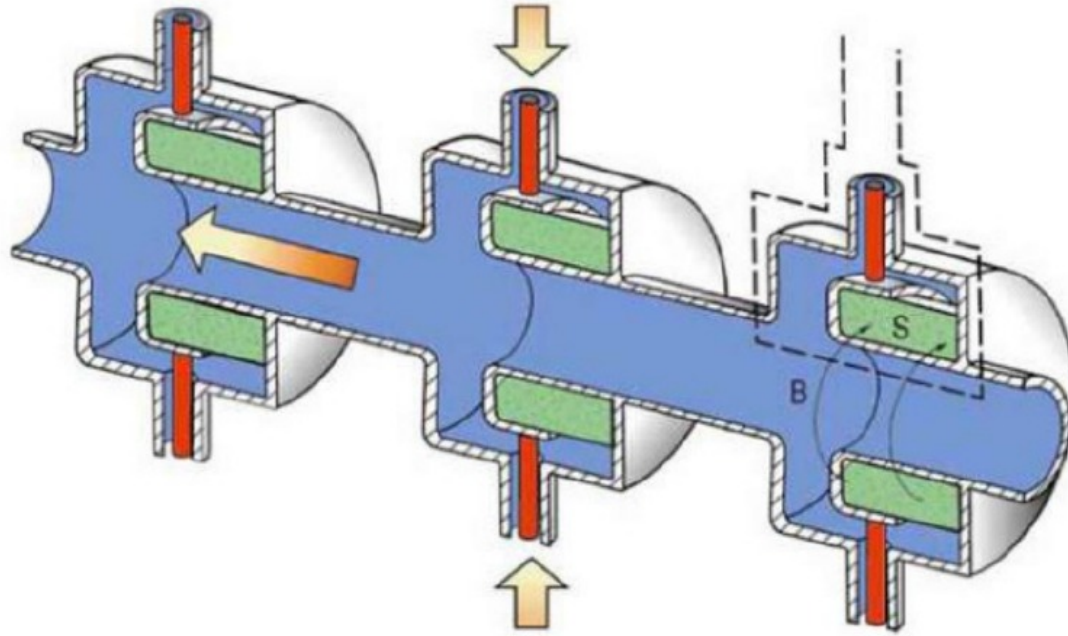
$$\Delta\mathcal{E} = q \int_A^B \mathbf{E} \cdot d\mathbf{l} = q(V_A - V_B).$$

- ▶ Returning through a DC accelerating structure cannot provide unlimited repeated energy gain.
- ▶ Maxwell's equations and energy conservation cannot be bypassed.



Can one gain energy again and again by passing through a DC accelerating gap? No.

Induction linacs: linear betatrons



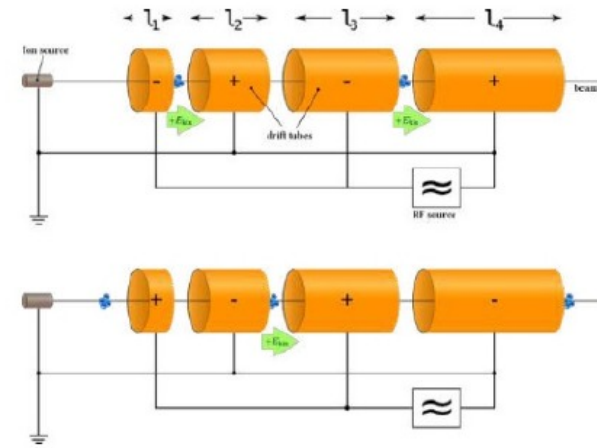
$$\oint \vec{E} \cdot d\vec{s} = -\frac{\partial}{\partial t} \left(\int \vec{H} \cdot d\vec{s} \right)$$

- ▶ Acceleration is produced by a time-varying magnetic flux.
- ▶ Useful for high-power and high-current beams.
- ▶ Accelerating field is limited.
- ▶ Pulsed by nature, with relatively low repetition rate (typically kHz).

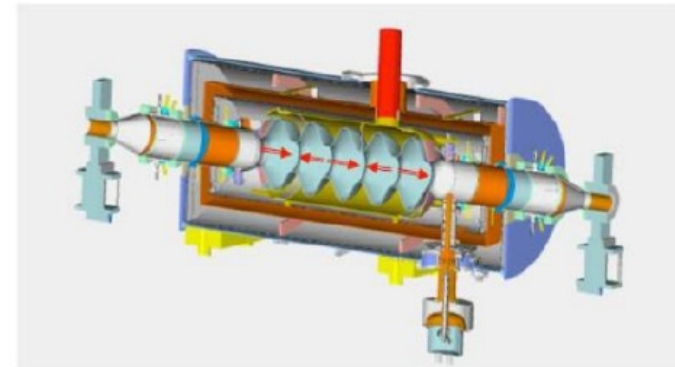
How an RF accelerator works

- ▶ The accelerating field oscillates in time, typically sinusoidally, and has a longitudinal component along the particle trajectory.
- ▶ The structure is divided into cells. Cell geometry and RF phase synchronize the field with the particle arrival.
- ▶ Energy gain from successive cells therefore adds coherently.

$$\frac{d\mathcal{E}}{dt} = q \mathbf{E} \cdot \mathbf{v}.$$



Wideröe linac: $\beta = v/c$ changes along the linac.



Electron linac: $\beta \simeq 1$.

Simple things to remember

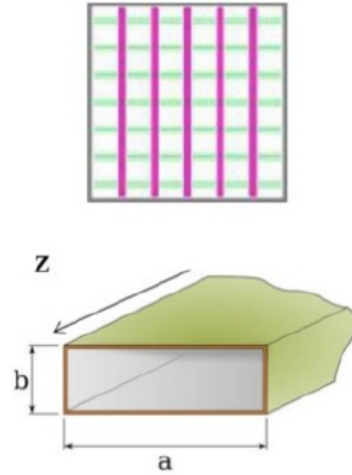
- ▶ DC electrostatic acceleration is limited by the available terminal potential difference.
- ▶ RF linear accelerators are not fundamentally limited in beam energy by a single terminal voltage.
- ▶ Coherent energy gain from cell to cell is achieved by matching the RF oscillation period to the particle travel time between cells.
- ▶ Accurate synchronization of RF phase and beam arrival time is essential for any RF linac.

Maxwell's equations in CGS (Gaussian) units

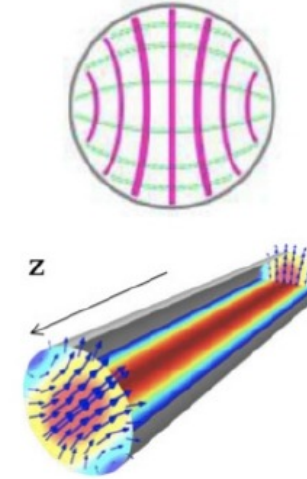
$$\begin{aligned}\nabla \cdot \mathbf{E} &= 4\pi\rho, & \nabla \cdot \mathbf{B} &= 0, \\ \nabla \times \mathbf{E} &= -\frac{1}{c} \frac{\partial \mathbf{B}}{\partial t}, & \nabla \times \mathbf{B} &= \frac{1}{c} \frac{\partial \mathbf{E}}{\partial t} + \frac{4\pi}{c} \mathbf{J}.\end{aligned}$$

Waveguides

Rectangular



Circular



$$\left(\Delta - \frac{1}{c^2} \frac{\partial^2}{\partial t^2} \right) \vec{A} = 0, \quad \Delta \equiv \nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2},$$

$$\vec{A} = \text{Re} \left\{ \vec{A}(\vec{r}_\perp) \exp[i(\omega t - k_z z)] \right\},$$

$$\nabla_\perp^2 \vec{A} + (k_0^2 - k_z^2) \vec{A} = 0, \quad k_0 = \frac{\omega}{c},$$

$$\nabla_\perp^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2}.$$

At the surfaces

$$\vec{n} \times \vec{E}|_s = 0, \quad \vec{n} \cdot \vec{B} = 0 \quad \Rightarrow \quad E_z|_s = 0, \quad \left. \frac{\partial B_z}{\partial n} \right|_s = 0.$$

TE and TM waves: transverse fields from E_z and B_z

$$k_0 = \frac{\omega}{c}, \quad k_c^2 = k_0^2 - k_z^2, \quad \nabla_{\perp} = \hat{x} \partial_x + \hat{y} \partial_y.$$

In source-free CGS units, Maxwell's curl equations become

$$\nabla \times \mathbf{E} = ik_0 \mathbf{B}, \quad \nabla \times \mathbf{B} = -ik_0 \mathbf{E}.$$

Writing $\mathbf{E} = \mathbf{E}_{\perp} + \hat{z}E_z$ and $\mathbf{B} = \mathbf{B}_{\perp} + \hat{z}B_z$, their transverse parts give

$$ik_z \hat{z} \times \mathbf{E}_{\perp} - \hat{z} \times \nabla_{\perp} E_z = ik_0 \mathbf{B}_{\perp},$$

$$ik_z \hat{z} \times \mathbf{B}_{\perp} - \hat{z} \times \nabla_{\perp} B_z = -ik_0 \mathbf{E}_{\perp}.$$

Solving these two coupled equations,

$$\mathbf{E}_{\perp} = \frac{i}{k_c^2} (k_z \nabla_{\perp} E_z - k_0 \hat{z} \times \nabla_{\perp} B_z),$$

$$\mathbf{B}_{\perp} = \frac{i}{k_c^2} (k_z \nabla_{\perp} B_z + k_0 \hat{z} \times \nabla_{\perp} E_z).$$

TE: $E_z = 0, B_z \neq 0$

TM: $B_z = 0, E_z \neq 0$

E_z and B_z therefore completely determine the transverse EM fields.

Cut-off frequency

The longitudinal field satisfies a transverse eigenvalue equation,

$$\nabla_{\perp}^2 \Psi + k_c^2 \Psi = 0,$$

while the longitudinal propagation constant obeys

$$k_z^2 = \frac{\omega^2}{c^2} - k_c^2.$$

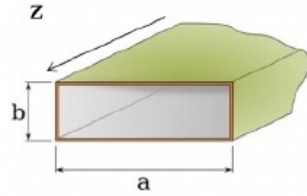
Hence the cut-off frequency is

$$\boxed{\omega_c = c k_c}.$$

- ▶ $\omega > \omega_c$: k_z is real and the mode propagates.
- ▶ $\omega < \omega_c$: $k_z = i\alpha$ and the field is evanescent, $\sim e^{-\alpha z}$.
- ▶ TE and TM modes obey different boundary conditions and therefore have different eigenvalues k_c .

Cut-off frequency: common waveguides

Rectangular



$$\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \psi + \gamma_{mn}^2 \psi = 0$$

$$\text{TE} : \psi_{mn}^{\text{TE}} = \psi_0 \cos k_m x \cos k_n y, \quad m + n \geq 1,$$

$$\text{TM} : \psi_{mn}^{\text{TM}} = \psi_0 \sin k_m x \sin k_n y, \quad m, n \geq 1,$$

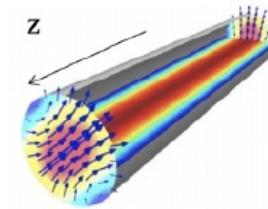
$$k_m = \frac{m\pi}{a}, \quad k_n = \frac{n\pi}{b}, \quad \gamma_{mn}^2 = k_m^2 + k_n^2.$$

Lowest cut-off angular frequency

$$\text{TE}_{10} : a > b, \quad \boxed{\omega_c = \frac{\pi c}{a}},$$

$$\text{TM}_{11} : \quad \boxed{\omega_c = \pi c \sqrt{\frac{1}{a^2} + \frac{1}{b^2}}}.$$

Circular



$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \psi}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \psi}{\partial \theta^2} + \gamma_{mn}^2 \psi = 0,$$

$$\psi_{mn} = \varphi_{mn}(r) e^{in\theta}, \quad \varphi_{mn} = J_n(\gamma_{mn} r).$$

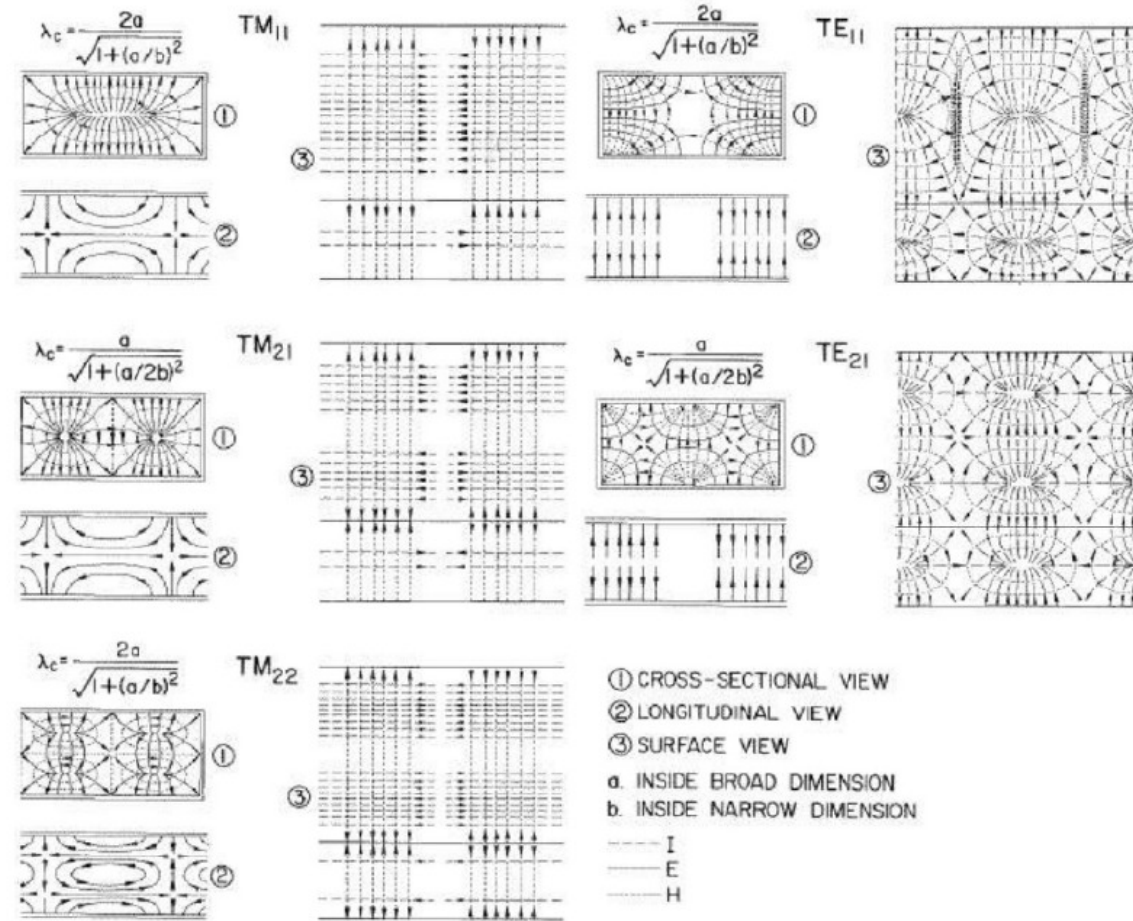
$$\text{Boundary conditions: } \text{TM} : \psi|_s = 0, \quad \text{TE} : \left. \frac{\partial \psi}{\partial n} \right|_s = 0.$$

Lowest cut-off angular frequency

$$\text{TM}_{01} : \gamma_{01} \simeq \frac{2.40483}{R}, \quad \boxed{\omega_c \simeq \frac{2.40c}{R}},$$

$$\text{TE}_{11} : \gamma_{11} \simeq \frac{1.84118}{R}, \quad \boxed{\omega_c \simeq \frac{1.84c}{R}}.$$

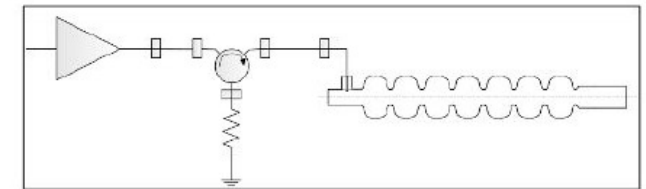
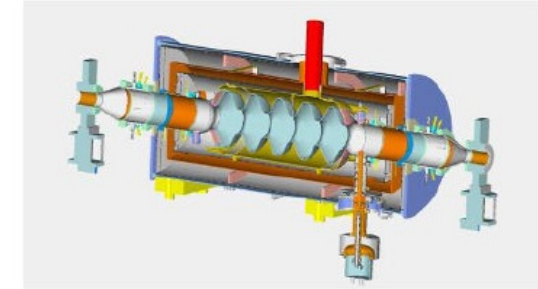
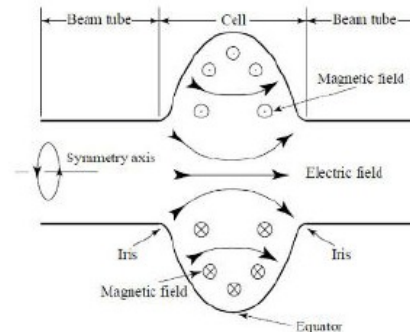
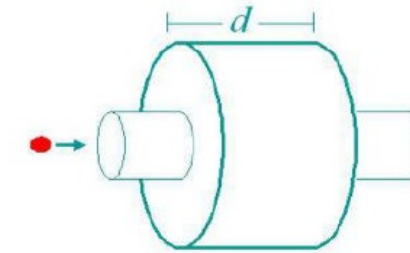
Modes in a rectangular waveguide



Each TE_{mn} or TM_{mn} mode has its own transverse field pattern and cut-off frequency.

RF cavities

- ▶ An RF cavity is a resonator designed to confine electromagnetic energy.
- ▶ Beam pipes attached to the cavity are chosen so that the operating mode is below their cut-off frequency.
- ▶ The RF field then decays evanescently along the beam pipes instead of propagating away.
- ▶ RF power is delivered through waveguides/coaxial lines and an input coupler; circulators and loads protect the RF source.



RF cavity modes: the lowest accelerating mode is TM_{010}

Inside a perfectly conducting cylindrical cavity, the fields satisfy Maxwell's equations and conducting-wall boundary conditions. There are infinitely many TE and TM eigenmodes.

- ▶ Acceleration requires $E_z \neq 0$, so a TM mode is required.
- ▶ The lowest-frequency accelerating mode of a pillbox cavity is TM_{010} .

For TM_{010} , using the field expressions from the source PPTX,

$$E_z(r, t) = E_0 J_0 \left(\frac{2.405 r}{R} \right) e^{i\omega t}$$

$$H_\phi(r, t) = -iE_0 J_1 \left(\frac{2.405 r}{R} \right) e^{i\omega t}$$

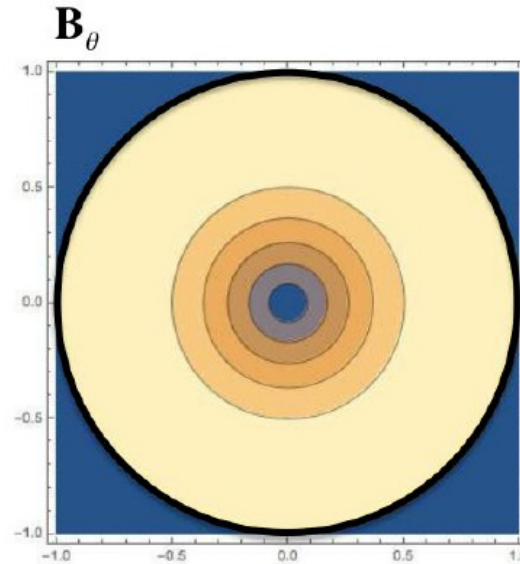
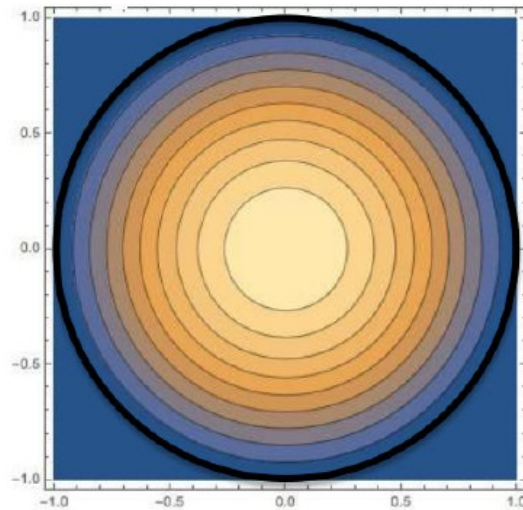
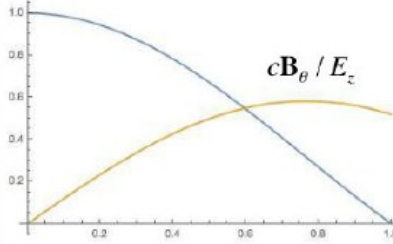
$$\omega_{010} = \frac{2.405 c}{R}, \quad \lambda_{010} = 2.61R.$$

A notable result: for an ideal pillbox without beam tubes, ω_{010} depends on the radius R , not the cavity length d .

Pillbox cavity

- ▶ Similarly to the waveguide case, choose a TM mode to have non-zero E_z .
- ▶ Select the TM_{010} mode with $k_z = 0$.

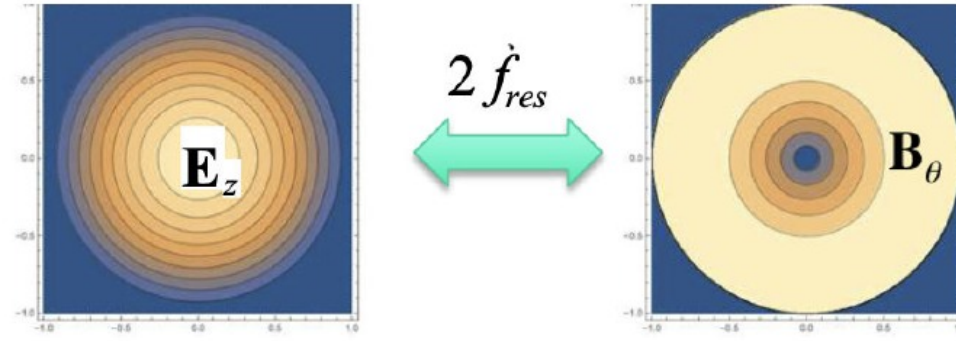
$$\mathbf{E}_z = E_z \cdot J_0\left(2.405 \frac{x}{a}\right) \sin(\omega t);$$
$$\mathbf{B}_\theta = \frac{1}{c} E_z \cdot J_1\left(2.405 \frac{x}{a}\right) \cos(\omega t)$$



Electromagnetic energy oscillates between electric and magnetic fields, peaking at the same stored energy in an ideal lossless cavity.

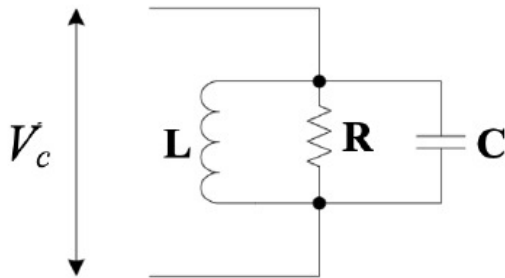
EM cavity

$$\begin{aligned}\vec{\mathbf{E}} &= \vec{\mathbf{E}}_o(\vec{r}) \cos(\omega t + \varphi(\vec{r})) \\ \vec{\mathbf{B}} &= \vec{\mathbf{B}}_o(\vec{r}) \sin(\omega t + \psi(\vec{r})) \\ \int \vec{\mathbf{E}}_o^2 dV &= \int \vec{\mathbf{B}}_o^2 dV \quad (\cdot c^2 \text{ for SI})\end{aligned}$$

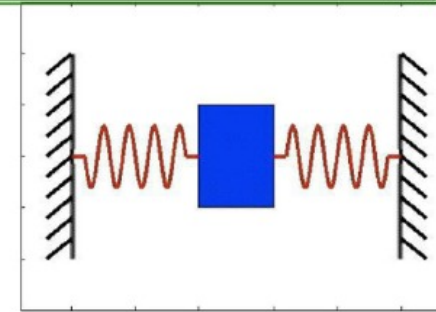


- ▶ Each cavity mode has a full analogy with a resonant LC circuit or a mechanical oscillator.
- ▶ Energy stored in the electric field corresponds to potential energy; energy stored in the magnetic field corresponds to kinetic energy.

$$E_M = \frac{LI^2}{2}; E_E = \frac{Q^2}{2C}; \omega_o = \frac{1}{\sqrt{LC}}$$



$$E_K = \frac{Mv^2}{2}; E_P = \frac{Kx^2}{2}; \omega_o = \sqrt{\frac{K}{M}}$$



Quality factor - definition

Consider a stand-alone cavity without external couplers. Let W be the stored electromagnetic energy and P_{loss} the dissipated power. The quality factor is

$$Q = \omega_0 \frac{W}{P_{\text{loss}}}.$$

With

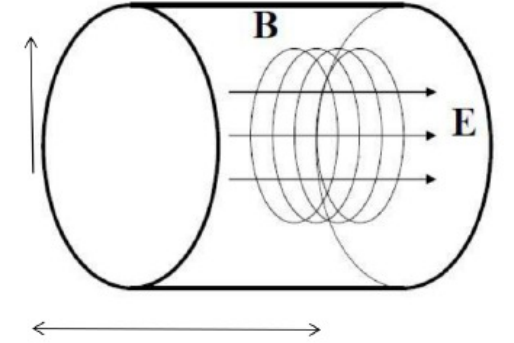
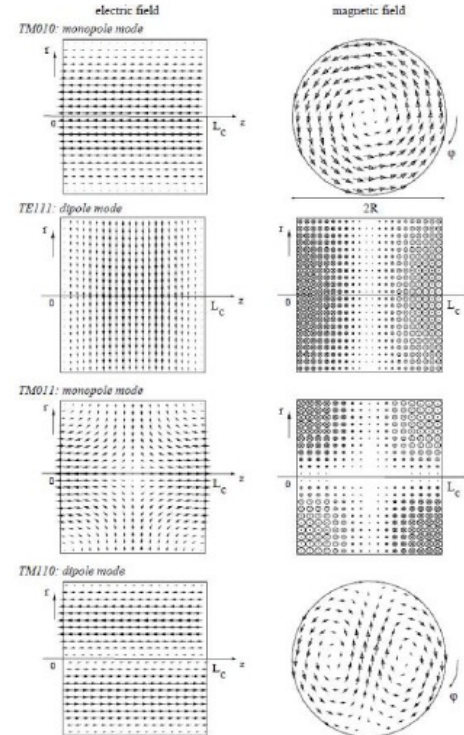
$$W = \int_V \left(\frac{\epsilon_0 E^2}{2} + \frac{B^2}{2\mu_0} \right) dV,$$

Q measures how slowly the stored energy decays. Equivalently, it is 2π times the number of RF oscillations associated with an e-fold reduction of energy.

Fundamental and higher-order modes (HOMs)

- ▶ A cavity supports an infinite spectrum of eigenmodes.
- ▶ The desired accelerating mode is the **fundamental accelerating mode**.
- ▶ Other resonances are higher-order modes (HOMs).
- ▶ Beam excitation of HOMs can produce unwanted longitudinal or transverse fields and may degrade beam quality or stability.

Eigenmodes in a Pill-box cavity



$$TM : \varphi_{mnl} = J_n(\gamma_{mn}r) \cos k_{z,l}z; \quad k_{z,l} = l \frac{\pi}{d}; \quad J_n(\gamma_{mn}R) = 0;$$

$$\omega_{res} = c \sqrt{\gamma_{mn}^2 + l^2 \frac{\pi^2}{d^2}}; \quad l = 0, 1, 2, \dots$$

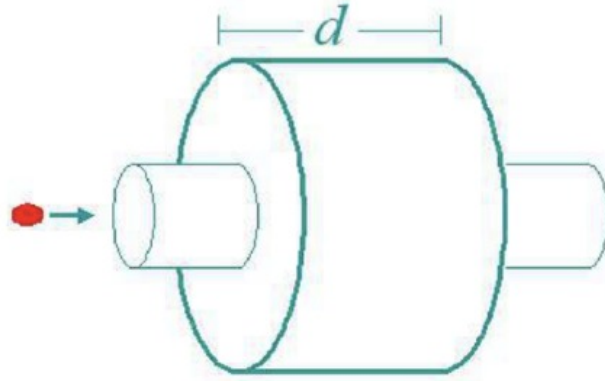
$$TE : \varphi_{mnl} = J_n(\kappa_{mn}r) \sin k_{z,l}z; \quad k_{z,l} = l \frac{\pi}{d}; \quad J'_n(\kappa_{mn}R) = 0;$$

$$\omega_{res} = c \sqrt{\kappa_{mn}^2 + l^2 \frac{\pi^2}{d^2}}; \quad l = 1, 2, \dots$$

Accelerating voltage and transit-time factor

For a particle moving on axis with speed $v = \beta c$,

$$V_c = \left| \int E_z(0, z) e^{i\omega z/(\beta c)} dz \right|.$$



For a uniform pillbox field of length d ,

$$V_c = E_0 d T,$$

$$T = \frac{\sin(\omega d/2\beta c)}{\omega d/2\beta c}.$$

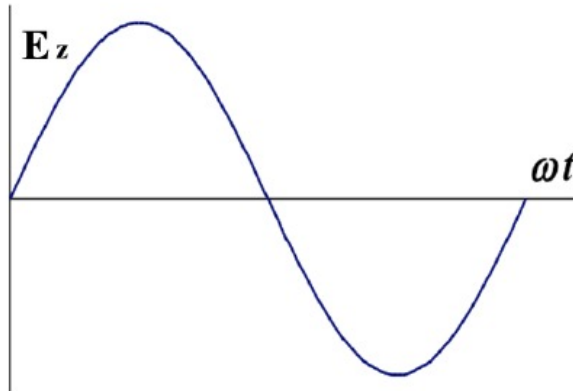
Choosing $d = \beta\lambda/2$ gives

$$T = \frac{2}{\pi}.$$

The accelerating gradient is conventionally

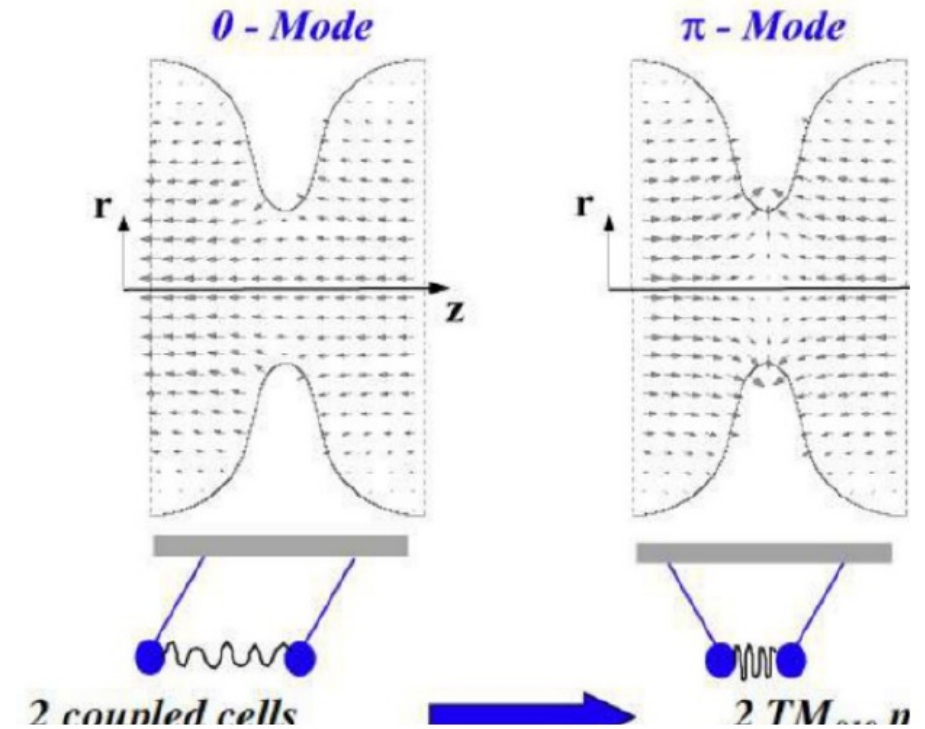
$$E_{\text{acc}} = \frac{V_c}{d}.$$

For practical multicell cavities one often uses $d = \beta\lambda/2$ per cell.



Multicell cavities: coupled oscillators

- ▶ Several cells can be connected to form one multicell cavity.
- ▶ The TM_{010} -like mode of each cell couples to neighboring cells through the irises.
- ▶ Coupling splits a single-cell resonance into a set of closely spaced normal modes - a **passband**.
- ▶ An N -cell cavity has N modes in each passband.



Multi-cell cavities

A single RF cell has limited accelerating voltage.

More energy can be obtained by using many independent cavities, but that requires many RF transmitters, waveguides and controls and gives a lower real-estate gradient.

Therefore, where high accelerating gradient is important, accelerator systems commonly use multicell cavities.

The cell length is chosen to keep the beam synchronized with the accelerating RF phase.

$$\text{Max}(V_{RF}) = \frac{E_0 \lambda_{RF}}{\pi}$$



9-cell Tesla design



7-cell



5-cell



What we learned

- ▶ Resonant cavity modes belong to TE and TM families; an infinite number of eigenmodes exist.
- ▶ Acceleration requires longitudinal electric field, so the lowest-frequency TM mode is commonly used as the fundamental accelerating mode.
- ▶ Other cavity modes are HOMs and can be parasitic for the beam.
- ▶ Important cavity figures of merit include accelerating voltage, transit-time factor and quality factor Q .
- ▶ In an N -cell cavity, each single-cell mode splits into a passband containing N modes; the passband width is set by cell-to-cell coupling.
- ▶ Accelerating cavities operate below the cut-off frequency of their beam pipes, so the RF field decays evanescently along the pipes.
- ▶ Coaxial lines and rectangular waveguides are widely used to deliver RF power to cavities.