PHY 564 Advanced Accelerator Physics Lecture 20

Collective Effects I: Wakefield and Impedances

Vladimir N. Litvinenko Yichao Jing Gang Wang

CENTER for ACCELERATOR SCIENCE AND EDUCATION Department of Physics & Astronomy, Stony Brook University Collider-Accelerator Department, Brookhaven National Laboratory





Outline

- Introduction
 - Collective effects, collective instabilities
- Wakefields and Impedances (Ultra-relativistic model)
 - Wake functions
 - Panofsky-Wenzel theorem
 - Cylindrical symmetric structure
 - Wake potentials, loss factor and kick factor
 - Impedances

What are collective effects?

- In the single particle dynamics, the E&M fields due to the charged particle themselves are neglected when considering their motions.
- As the number of the particles increases, the particles' own fields (and fields induced by them) can start to affect their behavior, which is generally called the collective effects.



Collective instabilities

- The particle beam interacts with its surroundings to generate an electromagnetic field, known as wakefield. This field then acts back on the beam, perturbing its motion.
- Under unfavorable conditions, the perturbation on the beam are continuously enhanced by the wakefield, leading to the collective



• For the rest of the lecture, we will focus on a wakefield model developed for an ultrarelativistic beam, $\gamma >> 1$ PHY 564 Fall 2020 Lecture 20

Ultra-relativistic beam and cylindrical perfect conducting beam pipe





At the limit of $\gamma \rightarrow \infty$





(It is also assumed that particles go straight, i.e. no radiations from particles)

Wake Functions

- Rigid bunch approximation: the motion of particles is not affected while passing through the structure
- Impulse approximation:

instead of the detailed E&M field in the structure, we care more about the total momentum change to the particles due to the wake field:

$$\Delta \vec{p}(x,y,s) = e \int_{-\infty}^{\infty} dt \Big[\vec{E}(x,y,z,t) + c\hat{z} \times \vec{B}(x,y,z,t) \Big]_{z=ct-s}$$



$$w_l(x, y, s) = -\frac{c}{qe} \Delta p_z = -\frac{c}{q} \int_{-\infty}^{\infty} E_z(x, y, ct - s, t) dt \quad [V/C]$$

Х

q

 $\left[\sqrt{/C} \right]$

S

Transverse wake function*:

$$\vec{w}_t(x,y,s) = \frac{c}{qe} \Delta \vec{p}_\perp = \frac{c}{q} \int_{-\infty}^{\infty} \left[\vec{E}_\perp(x,y,z,t) + c\hat{z} \times \vec{B}(x,y,z,t) \right]_{z=ct-s} dt$$

* These definition follow from 'Impedances and Wakes in High-Energy Particle Accelerators by B. Zotter, which is different from those in 'Physics of Collective Beam Instabilities in High Energy Accelerators' by A. Chao.
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Panofsky-Wenzel Theorem

We want to find relation between longitudinal wake function and transverse wake function due to a structure (a piece of beam pipe, bpm, bellow, cavity....)

$$\nabla_{s} \times \Delta \vec{p}(x,y,s) = \nabla_{s} \times \int_{a}^{b} \vec{F}(x,y,z,t) \Big|_{z=vt-s} dt = \int_{a}^{b} \left[\nabla \times \vec{F}(x,y,z,t) \right]_{z=vt-s} dt$$

$$\nabla_{s} = \hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} - \hat{z} \frac{\partial}{\partial s}$$

$$\nabla = \hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} + \hat{z} \frac{\partial}{\partial z}$$

$$\nabla = \hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} + \hat{z} \frac{\partial}{\partial z}$$

$$\nabla = \hat{x} \frac{\partial}{\partial x} + \hat{y} \frac{\partial}{\partial y} + \hat{z} \frac{\partial}{\partial z}$$

$$\nabla \times \vec{F} = q \nabla \times \vec{E} + q \nabla \times (\vec{v} \times \vec{B})$$

$$= -q \frac{\partial \vec{B}}{\partial t} + q \vec{v} (\nabla \cdot \vec{B}) - q (\vec{v} \cdot \nabla) \vec{B}$$

$$= -q \frac{\partial \vec{B}}{\partial t} - q v \frac{\partial}{\partial z} \vec{B}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\nabla_{s} \times \Delta \vec{p}(x,y,s) = -q \int_{-\infty}^{\infty} \left[\left(\frac{\partial}{\partial t} + v \frac{\partial}{\partial z} \right) \vec{B}(x,y,z,t) \right]_{z=vt-s} dt = -q \int_{-\infty}^{\infty} \frac{d}{dt} \vec{B}(x,y,vt-s,t) dt = 0$$

$$\frac{\partial}{\partial s} \Delta \vec{p}_{\perp} = -\vec{\nabla}_{\perp} \Delta p_{z}$$

$$\sum \frac{\partial}{\partial s} \vec{w}_{t}(x,y,s) = \vec{\nabla}_{\perp} w_{t}(x,y,s)$$

$$\left[\nabla_{\perp} \times \Delta \vec{p}_{\perp}(x,y,s) \right] \cdot \hat{z} = 0$$
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$$\sum \nabla_{s} \nabla \vec{x} = 0$$

$$\nabla_{s} \nabla \vec{x} = 0$$

$$\sum \nabla_{s} \nabla \vec{x} = 0$$

$$\nabla_{s} \nabla \vec{x$$

Another Relation at $\beta \rightarrow 1$

$$\nabla_{s} \cdot \Delta \vec{p}(x, y, s) = \nabla_{s} \cdot \int_{-\infty}^{\infty} \vec{F}(x, y, z, t) \Big|_{z=vt-s} dt = \int_{-\infty}^{\infty} \left[\nabla \cdot \vec{F}(x, y, z, t) \right]_{z=vt-s} dt$$

$$\nabla_{s} \cdot \Delta \vec{p}(x, y, s) = -\frac{q}{c} \int_{-\infty}^{\infty} \left[\frac{\partial}{\partial t} E_{z}(x, y, z, t) \right]_{z=vt-s} dt$$

$$\nabla_{s} \cdot \Delta \vec{p}(x, y, s) = -\frac{q}{c} \int_{-\infty}^{\infty} \left[\frac{\partial}{\partial t} E_{z}(x, y, z, t) \right]_{z=vt-s} dt$$

$$= -\frac{q}{c} \int_{-\infty}^{\infty} \left\{ \frac{d}{dt} E_{z}(x, y, vt - s, t) - \left[v \frac{\partial}{\partial z} E_{z}(x, y, z, t) \right] \right\}_{z=vt-s} dt$$

$$\nabla \cdot \vec{F} = q \nabla \cdot \vec{E} + q \nabla \cdot (\vec{v} \times \vec{B}) = \frac{q v}{c} \int_{-\infty}^{\infty} \left[\frac{\partial}{\partial z} E_{z}(x, y, z, t) \right]_{z=vt-s} dt$$

$$= -\frac{q v}{c} \int_{-\infty}^{\infty} \left[\frac{\partial}{\partial z} E_{z}(x, y, vt - s, t) - \left[v \frac{\partial}{\partial z} E_{z}(x, y, z, t) \right] \right]_{z=vt-s} dt$$

$$= -\frac{q v}{c} \frac{\partial}{\partial s} \int_{-\infty}^{\infty} E_{z}(x, y, vt - s, t) dt$$

$$= q \frac{\rho}{\varepsilon_{0}} - q \mu_{0} \vec{v} \cdot \left(\rho v \hat{z} + \varepsilon_{0} \frac{\partial}{\partial t} \vec{E} \right) \qquad \approx -\frac{\partial}{\partial s} \Delta p_{z}(x, y, s)$$

$$= q \frac{\rho}{\varepsilon_{0} \gamma^{2}} - \frac{q}{c} \beta \frac{\partial}{\partial t} E_{z}$$

$$\approx -\frac{q}{c} \frac{\partial}{\partial t} E_{z}$$
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Cylindrical symmetric structure I



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Cylindrical symmetric structure II

$$\frac{\partial}{\partial s}\Delta\vec{p}_{\perp} = -\vec{\nabla}_{\perp}\Delta p_{z} \implies \begin{cases} \frac{\partial}{\partial s}\Delta p_{\theta} = -\frac{1}{r}\frac{\partial}{\partial\theta}\Delta p_{z} & \Delta p_{r}(r',r,\theta,s) = \sum_{m=0}^{\infty}\Delta\tilde{p}_{m,r}(r',r,s)\cos(m\theta) \\ \frac{\partial}{\partial s}\Delta p_{r} = -\frac{\partial}{\partial r}\Delta p_{z} \implies \Delta p_{z}(r',r,\theta,s) = \sum_{m=0}^{\infty}\Delta\tilde{p}_{m,z}(r',r,s)\cos(m\theta) \end{cases}$$

$$\begin{bmatrix} \nabla_{\perp} \times \Delta \vec{p}_{\perp}(r',r,\theta,s) \end{bmatrix} \cdot \hat{z} = 0 \implies \frac{\partial}{\partial r} (r\Delta p_{\theta}) = \frac{\partial}{\partial \theta} \Delta p_{r} \implies \Delta p_{\theta}(r',r,\theta,s) = \sum_{m=0}^{\infty} \Delta \tilde{p}_{m,\theta}(r',r,s) \sin(m\theta)$$
$$\vec{\nabla}_{\perp} \cdot \Delta \vec{p} (r',r,\theta,s) = 0 \implies \frac{\partial}{\partial r} (r\Delta p_{r}) = -\frac{\partial}{\partial \theta} \Delta p_{\theta}$$
$$\left(\frac{\partial}{\partial r} \Delta \tilde{p}_{r,\theta} = \frac{m}{\Delta} \Delta \tilde{p}_{r,\theta} = \frac{\partial}{\partial \Delta} \Delta \tilde{p}_{r,\theta} = -\frac{\partial}{\partial \theta} \Delta \tilde{p}_{\theta} \right)$$

$$\Rightarrow \begin{cases} \frac{\partial s}{\partial s} \Delta p_{m,\theta} = \frac{-}{r} \Delta p_{m,z} & \frac{\partial s}{\partial s} \Delta \tilde{p}_{m,r} = -\frac{-}{\partial r} \Delta \tilde{p}_{m,z} \\ \frac{\partial s}{\partial r} (r \Delta \tilde{p}_{m,\theta}) = -m \Delta \tilde{p}_{m,r} & \frac{\partial s}{\partial r} (r \Delta \tilde{p}_{m,r}) = -m \Delta \tilde{p}_{m,\theta} \end{cases} \Rightarrow \frac{\partial s}{\partial r} \left[r \frac{\partial s}{\partial r} (r \Delta \tilde{p}_{m,r}(r',r,s)) \right] - m^2 \Delta \tilde{p}_{m,r}(r',r,s) = 0 \\ \frac{\partial s}{\partial r} (r \Delta \tilde{p}_{m,r}(r,s)) = -m \Delta \tilde{p}_{m,\theta} & \Rightarrow \frac{\partial s}{\partial r} \left[r \frac{\partial s}{\partial r} (r \Delta \tilde{p}_{m,r}(r',r,s)) \right] - m^2 \Delta \tilde{p}_{m,r}(r',r,s) = 0 \\ \Delta \tilde{p}_{m,r}(r,s) = A_m(r',s) mr^{m-1} + B_m(r',s)r^{-m-1} \end{cases}$$

Cylindrical symmetric structure III

By analyzing the source term in the Maxwell equations, it can be shown that the driving term has an explicit dependence on r'

$$\rho = \sum_{m=0}^{\infty} \rho_m \quad \vec{j} = \sum_{m=0}^{\infty} \vec{j}_m, \quad \vec{j}_m = c\rho_m \hat{s}, \qquad \vec{E}, \vec{B} \sim I_m = qa^m \qquad A_m(r', s) = \frac{qe}{v} r'^m W_m(s)$$

$$\rho_m = \frac{I_m}{\pi a^{m+1}(1+\delta_{m0})} \delta(s-ct) \delta(r-a) \cos m\theta,$$

*Reference: A. Chao 'Physics of Collective Beam Instabilities in High Energy Accelerators', eq. (2.35)

$$\Delta \tilde{p}_{m,r}(r,s) = A_m(r',s)mr^{m-1}$$

$$\Delta \tilde{p}_{m,\theta}(r',r,s) = -A_m(r',s)mr^{m-1}$$

$$\Delta \tilde{p}_{m,z} = -A'_m(r',s)r^m$$

$$\Delta \tilde{p}_{m,z}(r',r,s) = -\frac{qe}{v}r^{m}W_m(s)mr^{m-1}$$

$$\Delta \tilde{p}_{m,z}(r',r,s) = -\frac{qe}{v}r^{m}W_m(s)r^m$$

Cylindrical Symmetric Structure IV

$$w_{l}(r',r,\theta,s) = -\frac{c}{qe} \Delta p_{z}(r',r,\theta,s) = \sum_{m=0}^{\infty} W'_{m}(s)r'^{m}r^{m}\cos(m\theta)$$
$$\vec{w}_{t}(r',r,\theta,s) = \frac{c}{qe} \Delta \vec{p}_{\perp}(r',r,\theta,s) = \sum_{m=0}^{\infty} W_{m}(s)mr'^{m}r^{m-1} \Big[\cos(m\theta)\hat{r} - \sin(m\theta)\hat{\theta}\Big]$$

* In many references (by A. Chao, K.Y. Ng ...), $W_m(s)$ and $W'_m(s)$ are called wake functions.



Wake Potential

• In practice, usually only monopole mode (m=0) wake is considered for longitudinal wake field and only dipole mode (m=1) is considered for transverse mode.

monopole longitudinal wake:
$$w_{//}(s) = W'_0(s)$$
V/Cdipole transverse wake: $w_{\perp}(s) = W_1(s)$ V/(C*m)

• Wake potentials are defined to describe the momentum change induced by all particles in a bunch to a test unit charge:

$$V_{I/}(z_0) = \frac{-c\Delta p_z(z_0)}{eQ_e} = \int_{z_0}^{\infty} \lambda(z_1) w_{I/}(z_1 - z_0) dz_1 \quad [V/C]$$

$$V_{\perp}(z_0) = \frac{c\Delta \vec{p}_{\perp}(z_0)}{eQ_e} = \int_{z_0}^{\infty} \langle \vec{x}_{\perp}(z_1) \rangle \lambda(z_1) w_{\perp}(z_1 - z_0) dz_1 \quad [V/C]$$

$$\lambda(z) \text{ is line number density of a bunch}$$

* If we observe at $z = z^*$ and use arriving time, $t = \frac{1}{c} (z^* - z)$ as longitudinal variables, above definition become $V_{//}(t_0) = \int_{-\infty}^{t_0} \lambda(t_1) w_{//}(t_0 - t_1) dt_1 \qquad \vec{V}_{\perp}(t_0) = \int_{-\infty}^{t_0} \langle \vec{x}_{\perp}(t_1) \rangle \lambda(t_1) w_{\perp}(t_0 - t_1) dt_1$

Loss Factor and Kick Factor

• Once the longitudinal wake potential is known, the total energy change of a bunch to the wakefields is given by

$$\Delta U = -\int_{-\infty}^{\infty} \left[Q_e V_{//}(z) \right] \left[Q_e \lambda(z) \right] dz$$
(z z+dz) Charge in slice (z,z+dz)

Potential at slice (z,z+dz)

Definition of Loss Factor:

$$\kappa_{\prime\prime} \equiv \frac{-\Delta U}{Q_e^2} = \int_{-\infty}^{\infty} V_{\prime\prime}(z) \lambda(z) dz \quad [V/C]$$

 Similarly, the total transverse momentum change of a bunch to the wakefields is given by

$$\Delta \vec{P}_{\perp} = \int_{-\infty}^{\infty} \left[eQ_e \frac{\vec{V}_{\perp}(z)}{c} \right] \left[\frac{Q_e}{e} \lambda(z) \right] dz \quad \vec{K}_{\perp} = \frac{c\Delta \vec{P}_{\perp}}{Q_e^2} = \int_{-\infty}^{\infty} V_x(z)\lambda(z) dz \quad [V/C]$$
werse momentum change
Particle number in slice (z z+dz)

Trans Particle number in Silce (2,2+u2) of a particle at slice (z,z+dz).

Impedances

• Although the time domain description of particle-enviroment interaction, the wake fields, contains all informations, it is often more convinient to describe the interaction in frequency domain (convolution vs multiplication, calculate wakes in frequency domain can be easier some times, solving beam instability problems...), i.e. the impedances

$$Z_{\prime\prime}(\omega) = \frac{1}{c} \int_{0}^{\infty} w_{\prime\prime}(s) e^{i\omega s/c} ds \qquad [s*V/C]=[Ohm]$$
$$Z_{\perp}(\omega) = -\frac{i}{c} \int_{0}^{\infty} w_{\perp}(s) e^{i\omega s/c} ds \qquad [s*V/(C*m)]=[Ohm/m]$$

• The inverse transformations are

$$w_{\prime\prime}(s) = \frac{1}{2\pi} \int_{-\infty}^{\infty} Z_{\prime\prime}(\omega) e^{-i\omega s/c} d\omega$$
$$w_{\perp}(s) = \frac{i}{2\pi} \int_{-\infty}^{\infty} Z_{\perp}(\omega) e^{-i\omega s/c} d\omega$$

* In complex \mathcal{W} plane, $Z_{II}(\omega)$ and $Z_{\perp}(\omega)$ should not have singularities in the upper half plane, i.e. $Im(\omega) \ge 0$, in order to satisfy the causality condition:

$$w_{\prime\prime}(s < 0) = 0$$
 $w_{\perp}(s < 0) = 0$

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*The frequency ω is frequently allowed to have an imaginary part, in that case the transformation is actually Laplace transform, which is only defined for $\operatorname{Im}(\omega) \ge 0$



Properties of Impedances

 Symmetry properties about positive and negative frequency (Homework)

$$Z_{\perp}^{\prime} * (\omega) = Z_{\perp}(-\omega) \implies \begin{cases} \operatorname{Re}[Z_{\perp}(\omega)] = \operatorname{Re}[Z_{\perp}(-\omega)] \\ \operatorname{Im}[Z_{\perp}(\omega)] = -\operatorname{Im}[Z_{\perp}(-\omega)] \\ \operatorname{Im}[Z_{\perp}(\omega)] = -\operatorname{Re}[Z_{\perp}(-\omega)] \\ \operatorname{Im}[Z_{\perp}(\omega)] = \operatorname{Im}[Z_{\perp}(-\omega)] \end{cases}$$

• Relations between real part and imaginary part of impedances

$$w_{II}(s) = \frac{1}{2\pi} \int_{-\infty}^{\infty} Z_{II}(\omega) e^{-i\omega s/c} d\omega \implies w_{II}(s) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \left\{ \operatorname{Re} \left[Z_{II}(\omega) \right] \cos\left(\frac{\omega s}{c}\right) - \operatorname{Im} \left[Z_{II}(\omega) \right] \sin\left(\frac{\omega s}{c}\right) \right\} d\omega$$
$$(s < 0) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \left\{ \operatorname{Re} \left[Z_{I}(\omega) \right] \cos\left(\frac{\omega s}{c}\right) + \operatorname{Im} \left[Z_{I}(\omega) \right] \sin\left(\frac{\omega |s|}{c}\right) \right\} d\omega = 0 \implies \int_{-\infty}^{\infty} \operatorname{Im} \left[Z_{I}(\omega) \right] \sin\left(\frac{\omega |s|}{c}\right) d\omega = -\int_{-\infty}^{\infty} \operatorname{Re} \left[Z_{I}(\omega) \right] \cos\left(\frac{\omega |s|}{c}\right) d\omega$$

Hence, it is possible to express wake function solely in terms of real part of impedance, which implies that the real part and imaginary part is related.

 W_l

$$\implies w_{l}(s>0) = \frac{2}{\pi} \int_{0}^{\infty} \operatorname{Re}\left[Z_{l}(\omega)\right] \cos\left(\frac{\omega s}{c}\right) d\omega \qquad w_{\perp}(s>0) = \frac{2}{\pi} \int_{0}^{\infty} \operatorname{Re}\left[Z_{\perp}(\omega)\right] \sin\left(\frac{\omega s}{c}\right) d\omega$$

Kramers-Kronig relations:

$$Z_{II}(\omega) = -\frac{i}{\pi} P.V. \int_{-\infty}^{\infty} \frac{Z_{II}(\omega')}{\omega' - \omega} d\omega' \implies \operatorname{Re}\left[Z_{II}(\omega)\right] = \frac{1}{\pi} P.V. \int_{-\infty}^{\infty} \frac{\operatorname{Im}\left[Z_{II}(\omega')\right]}{\omega' - \omega} d\omega' \qquad \operatorname{Im}\left[Z_{II}(\omega)\right] = -\frac{1}{\pi} P.V. \int_{-\infty}^{\infty} \frac{\operatorname{Re}\left[Z_{II}(\omega')\right]}{\omega' - \omega} d\omega'$$

Many pictures and derivations used in the slides are taken from the following references:

[1] 'Wake and Impedance' by G.V. Stupakov, SLAC-PUB-8683;

- [2] 'Physics of Intensity Dependent Instabilities' by K.Y. Ng, Lecture Notes in USPAS 2002;
- [3] 'Accelerator Physics' by S.Y. Lee;
- [4] 'Physics of Collective Beam Instabilities in High Energy Accelerators' by A. Chao;
- [5] 'Impedances and Wakes in High-Energy Particle Accelerators' by B. Zotter and S. Kheifets.

What we learned today

- Apart from external fields (generated by magnets, cavities...), the motions of particles can be affected by fields induced by their own charge, either through direct Coulomb interactions (beam-beam, IBS...) or through their environment (wakefield). These effects are called collective effects, which can limit the performance of an accelerator.
- One of these adverse effects is called collective instabilities, which make particles significantly deviate from their designed trajectories (To be continued in the next class).
- For ultra relativistic particles, the collective instabilities are well described by a formalism using the quantities: **wakefields and impedances**. One of the advantages of using the formalism is that the effects are explicitly factorized into two parts: the beam (charge, distribution, bunch length...) and the environment (wakefields or impedances).