## Free Electron Lasers

# **Outline**

- Introduction
	- What is free electron laser (FEL)
	- Applications and some FEL facilities
	- Basic setup
	- Different types of FEL
- How FEL works
	- Electrons' trajectory and resonant condition
	- Analysis of FEL process at small gain regime (Oscillator)
	- Analysis of FEL process at high gain regime (Amplifier)

# Introduction I: What is free electron lasers

- A free-electron laser (FEL), is a type of laser whose lasing medium consists of very-high-speed electrons moving freely through a magnetic structure, hence the term free electron.
- The free-electron laser was invented by John Madey in 1971 at Stanford University.
- Advantages:
	- $\checkmark$  Wide frequency range
	- $\checkmark$  Tunable frequency
	- $\checkmark$  May work without a mirror (SASE)
- Disadvantages: large, expensive

#### Introduction II: Applications and FEL facilities

• Medical, Biology (small wavelength and short pulse are required for imaging proteins), Military (~Mwatts)…



• Operational FEL light sources worldwide (~20):

#### Free Electron Laser User Facilities Worldwide



#### Introduction III: FEL facilities







**PAL XFEL, South Korea** 





The Shanghai Soft X-ray Free-Electron Laser Facility Shanghai SXFEL, China



FEL User Facilities for Scientific Research

# Introduction IV: Basic Setup

![](_page_5_Figure_1.jpeg)

# Introduction V: different types of FEL

![](_page_6_Figure_1.jpeg)

Unperturbed Electron motion in helical wiggler  
\n(in the absence of radiation field)  
\n
$$
\vec{B}_{w}(x,y,z) = B_{w} \left[\cos(k_{w}z)\hat{x} - \sin(k_{w}z)\hat{y}\right]
$$
  
\n $\vec{F}(x,y,z) = -e\vec{v} \times \vec{B} = -e\nu_{z}\hat{z} \times \vec{B} = -e\nu_{z}B_{w} \left[\cos(k_{w}z)\hat{y} + \sin(k_{w}z)\hat{x}\right]$   
\n $\frac{d(mg\nu_{x})}{dt} = mg\frac{dv_{x}}{dt} = -e\nu_{z}B_{w}\sin(k_{w}z)$   
\n $\frac{d(mg\nu_{y})}{dt} = mg\frac{dv_{y}}{dt} = -e\nu_{z}B_{w}\sin(k_{w}z)$   
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\n $\frac{d(mg\nu_{y})}{dt} = -e\nu_{z}B_{w}\$ 

#### Energy change of electrons due to radiation field

$$
\vec{v}_{\perp}(z) = \frac{cK}{\gamma} \Big[ \cos(k_u z) \hat{x} - \sin(k_u z) \hat{y} \Big]
$$

Consider a circularly polarized electromagnetic wave (plane wave is an assumption for 1D analysis, which is usually valid for near axis analysis) propogating along z direction

**rgy change of electrons due to radiation field**  
\n
$$
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$$
\n\nacircularly polarized electromagnetic wave (plane wave is an assumption for 1D  
\nwhich is usually valid for near axis analysis) propagating along z direction  
\n
$$
\vec{E}_{\perp}(z,t) = E \left[ \cos(kz - \omega t)\hat{x} + \sin(kz - \omega t)\hat{y} \right] \qquad E_{z} = 0
$$
\n
$$
= E \left[ \cos(k(z - ct))\hat{x} + \sin(k(z - ct))\hat{y} \right] \qquad W = kc
$$
\n\nchange of an electron is given by  
\n
$$
\frac{dE}{dt} = \vec{F} \cdot \vec{v} = -e\vec{v}_{\perp} \cdot \vec{E}_{\perp}
$$
\n\nreading order, electrons move with constant velocity and hence  $z = v_{z}(t - t_{0})$   
\n
$$
\frac{dE}{dt} = \frac{dz}{dt} \frac{dE}{dz} = v_{z} \frac{dE}{dz} = \frac{1}{v_{z}} \frac{dE}{dz}
$$
\n\nPondermotive phase:  
\n
$$
\frac{dE}{dz} = -eE\theta_{s} \frac{c}{v_{z}} \cos(\psi) \approx -eE\theta_{s} \cos(\psi)
$$
\n
$$
\boxed{y = k_{u}z + k(z - ct)}
$$

Energy change of an electron is given by  $\frac{d\mathcal{E}}{dt} = \vec{F} \cdot \vec{v} = -e \vec{v}_{\perp} \cdot \vec{E}_{\perp}$ 

To the leading order, electrons move with constant velocity and hence  $|z - v_z(t - t_0)|$ 

$$
\frac{dE}{dt} = \frac{dz}{dt}\frac{dE}{dz} = v_z \frac{dE}{dz} \Rightarrow \frac{dE}{dz} = \frac{1}{v_z}\frac{dE}{dt}
$$

Pondermotive phase:

$$
V = k_u z + k(z - ct)
$$

# Resonant Radiation Wavelength

$$
\frac{d\mathcal{E}}{dz} = -eE\theta_s \cos\left[\left(k_w + k - k\frac{c}{v_z}\right)z + \psi_0\right]
$$

We define the resonant radiation wavelength such that

$$
k_w + k_0 - k_0 \frac{c}{v_z} = 0 \Rightarrow I_0 = I_w \left(\frac{c}{v_z} - 1\right) \approx \frac{I_w}{2g_z^2}
$$

$$
g_z^{-2} \circ 1 - v_z^2 / c^2 = 1 - \left(v_z^2 + v_\wedge^2\right) / c^2 + v_\wedge^2 / c^2 = g^{-2} + g_s^2 = g^{-2} \left(1 + K^2\right)
$$

FEL resonant frequency:

![](_page_9_Picture_5.jpeg)

At resonant frequency, the rotation of the electron and the radiation field is synchronized in the x-y plane and hence the energy exchange between them is most efficient.

#### Helicity of radiation at synchronization

The synchronization requires opposite helicity of radiation with respect to the electrons' trajectories.

![](_page_10_Figure_2.jpeg)

![](_page_10_Figure_3.jpeg)

# Longitudinal equation of motion

In the presence of the radiation field, the longitudinal equation of motion of an electron read

$$
\frac{dE}{dz} = -eE\theta_{s}\cos(\psi) \qquad y = k_{w}z + k(z - ct) \qquad \mathcal{E}_{0} \text{ is the average energy of the beam.}
$$
\n
$$
\frac{d}{dz}\psi = k_{w} + k - \frac{\omega}{v_{z}(\mathcal{E})}
$$
\n
$$
\approx k_{w} + k - \omega \left[ \frac{1}{v_{z}(\mathcal{E}_{0})} + (\mathcal{E} - \mathcal{E}_{0}) \frac{d}{d\mathcal{E}} \frac{1}{v_{z}} \right] \left\langle \frac{1}{\sqrt{1 - \frac{1}{\omega^{2}}} \right| \left\langle \frac{1}{\omega_{z}} \right| \left\langle \frac{1}{
$$

#### Low Gain Regime: Pendulum Equation

$$
\begin{aligned}\n\frac{dP}{dz} &= -eE\theta_s \cos(\psi) \\
\frac{d}{dz}\psi &= C + \frac{\omega}{\gamma_z^2 c \mathcal{E}_0} P\n\end{aligned}\n\right\} \Rightarrow \frac{d^2}{dz^2}\psi + \frac{eE\theta_s \omega}{\gamma_z^2 c \mathcal{E}_0} \cos(\psi) = 0
$$

We assume that the change of the amplitude of the radiation field, E, is negligible and treat it as a constant over the whole interaction.

$$
\frac{d^2}{dz^2}y + \hat{u}\cos(y) = 0 \qquad \hat{u} = \frac{l_w^2 e E \theta_s \omega}{\gamma_z^2 c \mathcal{E}_0} \qquad \hat{z} = \frac{z}{l_w}
$$

Pendulum equation:

$$
\frac{d^2}{dz^2}\left(\mathcal{Y}+\frac{\rho}{2}\right)+\hat{u}\sin\left(\mathcal{Y}+\frac{\rho}{2}\right)=0
$$

#### Low Gain Regime: Similarity to Synchrotron Oscillation

 $\mathcal Y$  is the angle between the transverse velocity vector and the radiation field vector and hence there is no energy kick for  ${\cal Y}$  =  $\rho$  /  $2$ 

#### FEL Synchrotron Oscillation

$$
\frac{d\tau}{ds} = \eta_{\tau}\pi_{\tau}; \ \ \frac{d\pi_{\tau}}{ds} = \frac{1}{C} \frac{eV_{RF}}{p_{o}c} \sin(k_{o}h_{\tau}\tau);
$$

![](_page_13_Figure_5.jpeg)

#### Low Gain Regime: Qualitative Observation

![](_page_14_Figure_1.jpeg)

The average energy of the electrons is right at resonant energy:

$$
\gamma_0 \gg \frac{\gamma_w \left(1 + K^2\right)}{2g^2} \implies \gamma = \gamma_0 = \sqrt{\frac{\lambda_w \left(1 + K^2\right)}{2\lambda_0}}
$$
With positive

\*Plots are taken from talk slides by Peter Schmuser.

The average energy of the electrons is slightly above the resonant energy:

$$
\gamma=\gamma_0+\Delta\gamma
$$

 $\lambda_0$  With positive detuning, there is net energy loss by electrons.

#### Low Gain Regime: Derivation of FEL Gain

Change in radiation power density (energy gain per seconds per unit area):

$$
\Delta \Pi_r = c \varepsilon_0 (E_{ext} + \Delta E)^2 - c \varepsilon_0 E_{ext}^2 \approx 2 c \varepsilon_0 E_{ext} \Delta E
$$

Average change rate in electrons' energy per unit beam area:

Energy deviation at entrance

![](_page_15_Figure_5.jpeg)

Assuming radiation has the same cross section area as the electron beam, we obtain the change in electric field amplitude:

$$
\Delta \Pi_r + \Delta \Pi_e = 0 \Longrightarrow \Delta E = -\frac{j_0 \langle P \rangle}{2 c \varepsilon_0 E_{ext} e}
$$
  

$$
\frac{dP}{dz} = -eE\theta_s \cos(\psi)
$$
  

$$
\frac{d}{dz}\psi = C + \frac{\omega}{\gamma_z^2 c \varepsilon_0} P
$$
  

$$
\Rightarrow \langle P \rangle = -eE\theta_s \langle \int_0^1 \cos[\psi(\hat{z})] d\hat{z} \rangle
$$

#### Low Gain Regime: Derivation of FEL Gain

$$
\frac{d^2}{d\hat{z}^2}\psi + \hat{u}\cos\psi = 0
$$
  

$$
\psi(\hat{z}) = \psi(0) + \psi'(0)\hat{z} - \hat{u}\int_0^{\hat{z}} d\hat{z}_1 \int_0^{\hat{z}_1} \cos\psi(\hat{z}_2) d\hat{z}_2
$$
 (1)

Assuming that all electrons have the same energy and uniformly distributed in the Pondermotive phase at the entrance of FEL:  $P_0 = 0$  and  $f(\psi_0) = \frac{1}{2}$  .  $\pi$  and  $\pi$  $(\psi_0) = \frac{1}{2\pi}$  . 1<sup>1</sup>  $f(\psi_0) = \frac{1}{2}$  .

The zeroth order solution for phase evolution is given by ignoring the effects from FEL interaction:

$$
\frac{dP}{dz} = -eE\theta_s \cos(\psi) \quad \bigg| \Rightarrow \quad \frac{d}{d\hat{z}}\psi = \hat{C} \Rightarrow \begin{cases} \quad \psi(\hat{z}) = \psi_0 + \hat{C}\hat{z} \\ \quad \psi'(\hat{z}) = \psi_0 + \hat{C}\hat{z} \end{cases} \qquad \hat{C} \equiv Cl_w
$$

Inserting the zeroth order solution back into eq.  $(1)$  yields the 1<sup>st</sup> order solution:

$$
\psi(\hat{z}) = \psi_0 + \hat{C}\hat{z} + \Delta \psi(\psi_0, \hat{z}) \qquad \Delta \psi(\psi_0, \hat{z}) = -\hat{u} \int_0^{\hat{z}} d\hat{z}_1 \int_0^{\hat{z}_1} \cos[\psi_0 + \hat{C}\hat{z}_2] d\hat{z}_2
$$

#### Low Energy Regime: Derivation of FEL Gain

$$
\Delta \psi(\psi_0, \hat{z}) = -\hat{u} \int_0^{\hat{z}} d\hat{z}_1 \int_0^{\hat{z}_1} \cos[\psi_0 + \hat{C}\hat{z}_2] d\hat{z}_2
$$
  
= 
$$
-\frac{\hat{u}}{\hat{C}^2} \left\{ \int_0^{\hat{c}z} \sin(\psi_0 + x_1) dx_1 - \hat{C}\hat{z} \sin \psi_0 \right\} = \frac{\hat{u}}{\hat{C}^2} \left[ \cos(\psi_0 + \hat{C}\hat{z}) - \cos \psi_0 + \hat{C}\hat{z} \sin \psi_0 \right]
$$

$$
\langle P \rangle = -eE I_w \theta_s \left\langle \int_0^1 \cos[\psi_0 + \hat{C}\hat{z} + \Delta \psi(\psi_0, \hat{z})] d\hat{z} \right\rangle
$$
 Average energy loss of electrons  
\n
$$
= eE \theta_s I_w \left\langle \int_0^1 \sin[\psi_0 + \hat{C}\hat{z}] \sin(\Delta \psi(\psi_0, \hat{z})) d\hat{z} \right\rangle - eE \theta_s I_w \left\langle \int_0^1 \cos[\psi_0 + \hat{C}\hat{z}] \cos(\Delta \psi(\psi_0, \hat{z})) d\hat{z} \right\rangle
$$
  
\n
$$
\approx eE \theta_s I_w \left\langle \int_0^1 \Delta \psi(\psi_0, \hat{z}) \sin[\psi_0 + \hat{C}\hat{z}] d\hat{z} \right\rangle - \frac{eE \theta_s I_w}{2\pi} \int_0^1 d\hat{z} \int_0^{2\pi} \cos[\psi_0 + \hat{C}\hat{z}] d\psi_0
$$
  
\n
$$
= \frac{eE \theta_s I_w}{2\pi} \frac{\hat{u}}{\hat{C}^2} \int_0^1 d\hat{z} \left\langle \hat{C}\hat{z} \cos(\hat{C}\hat{z}) \right\rangle_0^2 \sin^2 \psi_0 d\psi_0 - \sin(\hat{C}\hat{z}) \int_0^{2\pi} \cos^2 \psi_0 d\psi_0 \right\rangle
$$
  
\n
$$
= -eE \theta_s I_w \frac{\hat{u}}{\hat{C}^3} \left(1 - \frac{\hat{C}}{2} \sin \hat{C} - \cos \hat{C}\right)
$$

#### Low Energy Regime: Derivation of FEL Gain

Growth in the amplitude of radiation field:

$$
\Delta E = -\frac{j_0 \langle P \rangle}{2c \varepsilon_0 E_{ext}} = \frac{\pi j_0 \theta_s^2 \omega}{c \gamma_z^2 \gamma} \frac{l_w^3 E_{ext}}{I_A} \frac{2}{\hat{C}^3} \left( 1 - \frac{\hat{C}}{2} \sin \hat{C} - \cos \hat{C} \right)
$$

$$
\hat{u} = \frac{l_w^2 e E_{ext} \theta_s \omega}{\gamma_z^2 c \gamma mc^2}
$$

$$
I_A = \frac{4\pi\varepsilon_0 mc^3}{e}
$$

The gain is defined as the relative growth in radiation power:

$$
g_s = \frac{(E_{ext} + \Delta E)^2 - E_{ext}^2}{E_{ext}^2} \approx \frac{2\Delta E}{E_{ext}} = \tau \cdot f(\hat{C})
$$
As of

 $f(E_{ext}) = \tau \cdot f(\hat{C})$  as observed earlier, there is no gain if the electrons has resonant energy the electrons has resonant energy.

![](_page_18_Figure_8.jpeg)

# High Gain Regime: Concept

1. Energy kick from radiation field + dispersion/drift -> electron density bunching;

![](_page_19_Figure_2.jpeg)

\*The plots are for illustration only. The right plot actually shows somewhere close to saturation.

2. Electron density bunching makes more electrons radiates coherently -> higher radiation field;

3. Higher radiation fields leads to more density bunching through 1 and hence closes the positive feedback loop -> FEL instability.

![](_page_19_Figure_6.jpeg)

![](_page_19_Picture_7.jpeg)

![](_page_19_Figure_8.jpeg)

The positive feedback loop between radiation field and electron density bunching is the underlying mechanism of high gain FEL regime.

# 1-D Model for cold beam without detuning **1-D Model for cold<br>detuni**<br> $B(z) = \langle e^{-i\psi} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-i\psi_j}$ <br>*B D*<br>Assuming that *C* = 0 , it follows  $\frac{d}{dz} \frac{d}{dz}$ <br> $\frac{d}{dz} B(z) = -i \langle e^{-i\psi} \frac{d}{dz} \psi \rangle = -i \frac{\omega}{c \gamma_z^2 E_t}$ **D** Model for cold beam without<br>
detuning<br>  $=\langle e^{-i\psi}\rangle = \frac{1}{N}\sum_{j=1}^{N}e^{-i\psi_{j}}$   $D(z) = \langle Pe^{-i\psi}\rangle = \frac{1}{N}\sum_{j=1}^{N}P_{j}e^{-i\psi_{j}}$ <br>
ssuming that  $c = 0$ , it follows  $\frac{d}{dz}\psi = C + \frac{\omega}{\gamma_{z}^{2}cE_{0}}P = \frac{\omega}{\gamma_{z}^{2}cE_{0}}P$ <br>  $(z) = -i\langle e$ d beam without<br>
ing<br>  $D(z) = \langle Pe^{-i\psi} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\psi_j}$ <br>  $\frac{d}{dz} \psi = C + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$ <br>  $\frac{\partial}{\partial E_0} \langle e^{-i\psi} P \rangle = -i \frac{\omega}{c \gamma_z^2 E_0} D(z)$ eam without<br>
<br>  $\sum_{z} = \langle Pe^{-i\nu} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\nu_j}$ <br>  $\sum_{z} + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$ <br>  $\sum_{z} -i\nu P \rangle = -i \frac{\omega}{c \gamma_z^2 E_0} D(z)$ -D Model for cold beam without<br>
detuning<br>  $=\langle e^{-iw}\rangle = \frac{1}{N}\sum_{j=1}^{N}e^{-iw_{j}}$   $D(z) = \langle Pe^{-iw}\rangle = \frac{1}{N}\sum_{j=1}^{N}P_{j}e^{-iw_{j}}$ <br>
ssuming that  $C = 0$ , it follows  $\frac{d}{dz}\psi = C + \frac{\omega}{\gamma_{z}^{2}cE_{0}}P = \frac{\omega}{\gamma_{z}^{2}cE_{0}}P$ <br>  $(z) = -i\langle e^{-iw}\frac{d}{dz}\$ **beam without**<br> **ng**<br>  $(z) = \langle Pe^{-iw} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-iw_j}$ <br>  $w = C + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$ <br>  $\frac{1}{C \gamma_z^2 E_0} Q(z)$ <br>  $\frac{1}{C \gamma_z^2 E_0} Q(z)$ <br>  $\frac{1}{C \gamma_z^2 E_0} P = -\langle e^{-iw} e E \theta_s \cos(w) \rangle \approx -\frac{1}{2}$ detuning<br>  $\frac{1}{\sqrt{\frac{N}{y}}e^{-i\psi_{j}}}$   $D(z) = \langle Pe^{-i\psi_{j}}\rangle$ <br>  $D(z) = \langle Pe^{-i\psi_{j}}\rangle$ <br>  $D(z) = \langle Pe^{-i\psi_{j}}\rangle$ <br>  $\frac{1}{\sqrt{\frac{N}{dz}}\psi} \frac{d}{dz}\psi = -i\frac{\omega}{c\gamma_{z}^{2}E_{0}}\langle e^{-i\psi}P\rangle$ <br>  $\frac{dP}{dz} = -e\theta_{s}E(z)\cos(\psi)$ <br>  $\frac{i\langle e^{-i\psi}P\frac{d}{dz}\psi\rangle \approx \langle e^{-i\psi}\frac{d}{dz$ *z z* **1-D Model for cold beam without**<br> **detuning**<br>  $B(z) = \langle e^{-i\nu} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-i\nu_j}$ <br>  $D(z) = \langle Pe^{-i\nu} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\nu}$ <br>
Assuming that  $C = 0$ , it follows  $\frac{d}{dz} w = C + \frac{\omega}{\gamma_z^2 \epsilon E_0} P = \frac{\omega}{\gamma_z^2 \epsilon E_0} P$ <br>  $\frac{$ **1-D Model for cold beam without**<br> **detuning**<br>  $B(z) = \langle e^{i\psi} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-i\psi_{j}}$ <br>  $D(z) = \langle Pe^{i\psi} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_{j} e^{-i\psi_{j}}$ <br>
Assuming that  $C = 0$ , it follows  $\frac{d}{dz} \psi = C + \frac{\omega}{\gamma_{z}^2 c F_0} P = \frac{\omega}{\gamma_{z}^2 c F_0}$ detuning<br>  $\frac{1}{N}\sum_{j=1}^{N}e^{-iw_{j}}$   $D(z) = \langle Pe^{-iw}\rangle = \frac{1}{N}\sum_{j=1}^{N}P_{j}e^{-iw_{j}}$ <br>  $\sum_{j=0}^{N} = 0$ , it follows  $\frac{d}{dz}\psi = C + \frac{\omega}{r_{z}^{2}cE_{0}}P = \frac{\omega}{r_{z}^{2}cE_{1}}P$ <br>  $\frac{dw}{dz}\frac{d}{dz}\psi = -i\frac{\omega}{c\gamma_{z}^{2}E_{0}}\langle e^{-iw}P\rangle = -i\frac{\omega}{c\gamma_{z}^{2}E_{$ Model for cold beam without<br>
detuning<br>  $e^{-i\psi}\rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-i\psi_{j}}$   $D(z) = \langle Pe^{-i\psi}\rangle = \frac{1}{N} \sum_{j=1}^{N} P_{j} e^{-i\psi_{j}}$ <br>  $= -i \left\langle e^{-i\psi} \frac{d}{dz} \psi \right\rangle = -i \frac{\omega}{c \gamma_{z}^{2} E_{0}} \left\langle e^{-i\psi} P \right\rangle = -i \frac{\omega}{c \gamma_{z}^{2} E_{0}} P$ <br>  $= -i \left\langle e^{-i$ **Example 1**<br> **Example 10**<br> **EXAMPLE 10** 1-D Model for cold beam without<br>
detuning<br>  $\langle z \rangle = \langle e^{-iy} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-iy}$ ,  $D(z) = \langle Pe^{-w} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-iy}$ ,<br>
Assuming that  $c = 0$ , it follows  $\frac{d}{dz} w = C + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$ <br>  $\frac{d}{dz} \frac{d}{dz} \$ **Model for cold beam wir**<br> **detuning**<br>  $e^{-iw}$  =  $\frac{1}{N} \sum_{j=1}^{N} e^{-iw_j}$ <br>  $D(z) = \langle Pe^{-iw} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-iy}$ <br>  $= -i \langle e^{-iw} \frac{d}{dz} \psi \rangle = -i \frac{\omega}{cz^2 E_0} \langle e^{-iw} P \rangle = -i \frac{d}{cz}$ <br>  $= -e^{\int \frac{dP}{dz}} = -e^{\int \frac{d}{dz} \psi} \rangle = -i \frac{\omega}{cz^2 E_0} \langle e$ **1-D Model for cold beam without**<br> **detuning**<br>  $B(z) = \langle e^{-iw} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-iw_j}$ <br>  $D(z) = \langle Pe^{-w} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-iw_j}$ <br>
Assuming that  $C = 0$ , it follows  $\frac{d}{dz} w = C + \frac{\omega}{\gamma_1^2 \epsilon E_0} P = \frac{\omega}{\gamma_2^2 \epsilon E_0} P$ <br>  $\frac{d}{dz} B$ **1-D Model for cold beam v<br>
detuning**<br>  $B(z) = \langle e^{-iw} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-iw_j}$ <br>  $D(z) = \langle Pe^{-iw} \rangle = -\frac{1}{N} \frac{1}{2} \sum_{j=1}^{N} e^{-iw_j}$ <br>
Assuming that  $C = 0$ , it follows  $\frac{d}{dz} \psi = C + \frac{\omega}{V_z^2 E_0} P = -\frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2$ −D Model for cold beam without<br>
detuning<br>  $= \langle e^{-i\psi} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-i\psi}$ ,  $D(z) = \langle Pe^{-i\psi} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\psi}$ <br>
Assuming that  $C = 0$ , , it follows  $\frac{d}{dz} \psi = C + \frac{\omega}{r_1^2 c E_0} P = \frac{\omega}{r_1^2 c E_0} P$ <br>  $\frac{d}{dz} = -i$  $\langle e^{-i\psi} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\psi_j}$ <br>  $\langle \frac{\omega}{z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$ <br>  $\langle \frac{\omega}{c \gamma_z^2 E_0} D(z) \rangle$ d beam without<br>
ing<br>  $D(z) = \langle Pe^{-i\psi} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\psi_j}$ <br>  $\frac{d}{dz} \psi = C + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$ <br>  $\frac{\omega}{\gamma_z^2 c E_0} \langle e^{-i\psi} P \rangle = -i \frac{\omega}{c \gamma_z^2 E_0} D(z)$ <br>  $\cos(\psi)$ **d beam without**<br> **ning**<br>  $D(z) = \langle Pe^{-iw} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-iw_j}$ <br>  $\frac{d}{dz} \psi = C + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$ <br>  $\frac{\omega}{\gamma_z^2 E_0} \langle e^{-iw} P \rangle = -i \frac{\omega}{c \gamma_z^2 E_0} D(z)$ <br>  $\cos(\psi)$ m without<br>  $e^{-i\psi}\rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\psi_j}$ <br>  $\frac{\omega}{cE_0} P = \frac{\omega}{\gamma_z^2 cE_0} P$ <br>  $\Rightarrow$   $\frac{1}{C \gamma_z^2 E_0} D(z)$ am without<br>  $Pe^{-i\psi}$  =  $\frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\psi_j}$ <br>  $\frac{\omega}{r_z^2 c E_0} P = \frac{\omega}{r_z^2 c E_0} P$ <br>  $\langle P \rangle = -i \frac{\omega}{c \gamma_z^2 E_0} D(z)$ beam without<br>  $log(z) = \langle Pe^{-iw} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-iw_j}$ <br>  $= C + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$ <br>  $\langle e^{-iw} P \rangle = -i \frac{\omega}{c \gamma_z^2 E_0} D(z)$ m without<br>  $\langle \overline{E}_{\overline{E}_{0}} P = \frac{1}{N} \sum_{j=1}^{N} P_{j} e^{-i \psi_{j}}$ <br>  $\overline{E}_{\overline{E}_{0}} P = \frac{\omega}{r_{z}^{2} E_{0}} P$ <br>  $\overline{C} = -i \frac{\omega}{c r_{z}^{2} E_{0}} D(z)$

$$
B(z) = \left\langle e^{-i\psi} \right\rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-i\psi_j} \qquad D(z)
$$

$$
D(z) = \left\langle Pe^{-i\psi}\right\rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-i\psi_j}
$$

Assuming that  $C = 0$ , it follows  $\frac{C}{\sqrt{2\pi}}\psi =$ 

$$
\frac{d}{dz}\psi = C + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P
$$

$$
\left|\frac{d}{dz}B(z)=-i\left\langle e^{-i\psi}\frac{d}{dz}\psi\right\rangle =-i\frac{\omega}{c\gamma_{z}^{2}\mathbf{E_{0}}}\left\langle e^{-i\psi}P\right\rangle =-i\frac{\omega}{c\gamma_{z}^{2}\mathbf{E_{0}}}D\left(z\right)\right|
$$

$$
\frac{dP}{dz} = -e\theta_s E(z) \cos(\psi)
$$

1-D Model for cold beam without  
\ndetuning  
\n
$$
B(z) = \langle e^{-iw} \rangle = \frac{1}{N} \sum_{j=1}^{N} e^{-iw_j} \qquad D(z) = \langle Pe^{-iw} \rangle = \frac{1}{N} \sum_{j=1}^{N} P_j e^{-iw_j}
$$
\nAssuming that  $c = 0$ , it follows  $\frac{d}{dz} \psi = C + \frac{\omega}{\gamma_z^2 c E_0} P = \frac{\omega}{\gamma_z^2 c E_0} P$   
\n
$$
\frac{d}{dz} B(z) = -i \langle e^{-iw} \frac{d}{dz} \psi \rangle = -i \frac{\omega}{c \gamma_z^2 E_0} \langle e^{-iw} P \rangle = -i \frac{\omega}{c \gamma_z^2 E_0} D(z)
$$
\n
$$
\frac{dP}{dz} = -e \theta_z E(z) \cos(\psi)
$$
\n
$$
\frac{d}{dz} D(z) = \langle e^{-iw} \frac{d}{dz} P \rangle - i \langle e^{-iw} P \frac{d}{dz} \psi \rangle \approx \langle e^{-iw} \frac{d}{dz} P \rangle = -\langle e^{-iw} e E \theta_z \cos(\psi) \rangle \approx -\frac{1}{2} e \theta_z E
$$

# Wave Equation

1-D theory and hence  $\partial/\partial x = 0$  and  $\partial/\partial y = 0$ 

Wave equation for transverse vector potential:

 $\frac{1}{\mu} - \frac{1}{2} \frac{U}{\gamma^2} - \mu_0 \vec{j}_{\perp}$  (1)  $\partial t^2$  route the set of  $\partial t^2$  $-\frac{1}{2}\frac{\partial^2 A_{\perp}}{2} = -\mu_0 \vec{j}$  (1  $\partial z^2$   $c^2$   $\partial t^2$   $\qquad$  $\partial^2 A_1$  1  $\partial^2 A_1$ *j* (1)  $t^2$   $\sim$   $\sim$   $\sim$  $A_1 \t 1$  (1)  $z^2$  *c*<sup>2</sup>  $\partial t^2$  *r*-0*y*  $\perp$  $\vec{A}_1$  1  $\partial^2 \vec{A}_1$   $\rightarrow$  (1)  $\frac{1}{2}$  -  $\mu_0 J_{\perp}$  (-1) 2  $a^2$   $a^2$   $f$  ${}^2\vec{A}$ , 1  $\partial^2\vec{A}$ ,  $\therefore$  $\mu_0 J_{\perp}$  (1)  $1 \qquad \qquad$   $\qquad \qquad$   $\qquad \qquad$   $\qquad$   $\psi = k_w z + k (z - ct)$ <br>  $\vec{A}_{\perp} = - \mu_0 \vec{j}_{\perp}$  (1)<br>  $= \theta_e e^{-ik_w z} j_z$  (2)

 $\rightarrow$   $\rightarrow$   $\rightarrow$ 

 $2\vec{A}$ 

Transverse current perturbation:

$$
\dot{J}_x + \dot{U}_y = \frac{1}{v_z} \left( v_x + i v_y \right) \dot{J}_z = \theta_s e^{-ik_w z} \dot{J}_z \tag{2}
$$

We seek the solution for vector potential of the form:

$$
\vec{v}_{\perp}(z) = \frac{cK}{\gamma} \Big[ \cos(k_u z) \hat{x} - \sin(k_u z) \hat{y} \Big]
$$

$$
A_{x,y}(z,t) = \widetilde{A}_{x,y}(z)e^{i\omega(z/c-t)} + \widetilde{A}_{x,y}^*(z)e^{-i\omega(z/c-t)}
$$
(3)

Inserting eq. (2) and (3) into eq. (1) yields

$$
e^{i\omega(z/c-t)}\left\{\frac{2i\omega}{c}\frac{\partial}{\partial z}\left(\frac{\widetilde{A}}{\widetilde{A}_{y}}\right)+\frac{\partial^{2}}{\partial z^{2}}\left(\frac{\widetilde{A}_{x}}{\widetilde{A}_{y}}\right)\right\}+C.C.=-\mu_{0}\theta_{s}\left(\frac{\cos(k_{w}z)}{-\sin(k_{w}z)}\right)j_{z}
$$
Multiplying both  
\n
$$
\left\{\frac{2i\omega}{c}\frac{\partial}{\partial z}\left(\frac{\widetilde{A}_{tot,x}}{\widetilde{A}_{tot,y}}\right)+\frac{\partial^{2}}{\partial z^{2}}\left(\frac{\widetilde{A}_{tot,x}}{\widetilde{A}_{tot,y}}\right)\right\}=-\frac{\mu_{0}N\theta_{s}}{2}\left(e^{ik_{w}z}+e^{-ik_{w}z}\right)\left\langle j_{z}e^{-i\psi}\right\rangle e^{ik_{w}z}
$$
helicity argument  
\n
$$
\frac{\sin\omega z}{2}\left(\frac{\widetilde{A}_{tot,x}}{\widetilde{A}_{tot,y}}\right)+\frac{\partial^{2}}{\partial z^{2}}\left(\frac{\widetilde{A}_{tot,x}}{\widetilde{A}_{tot,y}}\right)\right\}=-\frac{\mu_{0}N\theta_{s}}{2}\left\{\frac{e^{ik_{w}z}+e^{-ik_{w}z}}{ie^{ik_{w}z}-ie^{-ik_{w}z}}\right\}\left\langle j_{z}e^{-i\psi}\right\rangle e^{ik_{w}z}
$$
helicity argument

Multiplying both sides by  $e^{ik_wz}$ terms proportional ce they will change  $L$  (same as the nt).

1. Ignoring fast oscillating term  $\sim e^{2ik_{w}z}$ 

2. Ignoring second derivative by assuming that the variation of  $\tilde{A}_x$ '  $\tilde{A}_x$ '  $\tilde{a}$ ,

#### Wave Equation

After neglecting the fast oscillation terms, we get the following relation between the current perturbation and the vector potential of the radiation field:

$$
\frac{\partial}{\partial z}\widetilde{A}_{\text{tot},x} = -\frac{c\mu_0 N\theta_s}{4i\omega}\left\langle j_z e^{-i\psi}\right\rangle \qquad \frac{\partial}{\partial z}\widetilde{A}_{\text{tot},y} = \frac{\mu_0 Nc\theta_s}{4\omega}\left\langle j_z e^{-i\psi}\right\rangle
$$

 $\rightarrow$  $\rightarrow$  (  $\overrightarrow{a}$ In order to relate the vector potential to the electric field, we use the Maxwell equation:

**EXECUTE: EXECUTE:** We get the following relation between the  
intertribution and the vector potential of the radiation field:  

$$
\frac{\partial}{\partial z} \tilde{A}_{tot,x} = -\frac{c\mu_0 N \theta_s}{4i\omega} \langle j_z e^{-i\psi} \rangle \qquad \frac{\partial}{\partial z} \tilde{A}_{tot,y} = \frac{\mu_0 N c \theta_s}{4\omega} \langle j_z e^{-i\psi} \rangle
$$
  
der to relate the vector potential to the electric field, we use the Maxwell  
tion:  

$$
\nabla \times \vec{E} + \frac{\partial \vec{B}}{\partial t} = 0 \Rightarrow \nabla \times (\vec{E} + \frac{\partial \vec{A}}{\partial t}) = 0 \Rightarrow (\vec{E} + \frac{\partial \vec{A}}{\partial t}) = \vec{\nabla} \varphi \Rightarrow E_{x,y} = -\frac{\partial A_{x,y}}{\partial t}
$$

$$
\Rightarrow E_x + iE_y = E e^{i\omega(z/c-t)} = -\frac{\partial}{\partial t} \left[ \left( \frac{\lambda_0}{N_{tot,x}} + i \frac{\lambda_0}{N_{tot,y}} \right) e^{i\omega(z/c-t)} \right] \qquad \text{1D:} \quad \frac{\partial}{\partial x} = 0, \quad \frac{\partial}{\partial y} = 0
$$

$$
\Rightarrow E = i\omega \left( \frac{\lambda_0}{N_{tot,x}} + i \frac{\lambda_0}{N_{tot,y}} \right) \qquad \frac{1}{E} (z,t) = E \left[ \cos(k(z-ct)) \hat{x} + \sin(k(z-ct)) \hat{y} \right]
$$
  
ly, the relation between the radiation field and the current modulation is obtained:  

$$
\frac{d}{dz} E = i\omega \left( \frac{\partial}{\partial z} \tilde{A}_{tot,x} + i \frac{\partial}{\partial z} \tilde{A}_{tot,y} \right) = -\frac{c\mu_0 N \theta_s}{2} \langle j_z e^{-i\psi} \rangle = \frac{ec^2 N \mu_0 \theta_s}{2V} B = \frac{ec^2 n \mu_0 \theta_s}{2B} B
$$

$$
\langle j_z e^{-i\psi} \rangle = -\frac{ec}{N V} \frac{\partial}{\partial z} e^{-i\psi_z} = -\frac{ecB}{V}
$$

Finally, the relation between the radiation field and the current modulation is obtained:

$$
\frac{d}{dz}E = i\omega \left(\frac{\partial}{\partial z}\tilde{A}_{tot,x} + i\frac{\partial}{\partial z}\tilde{A}_{tot,y}\right) = -\frac{c\mu_0 N\theta_s}{2}\left\langle j_z e^{-i\psi} \right\rangle = \frac{ec^2 N\mu_0 \theta_s}{2V}B = \frac{ec^2 n\mu_0 \theta_s}{2}B
$$
\n
$$
\left\langle j_z e^{-i\psi} \right\rangle = -\frac{ec}{NV}\bigg|_{k=1}^N e^{-i\psi_k} = -\frac{ecB}{V}
$$
\n
$$
n = N/V
$$

# 1-D High Gain FEL Equation for Cold Beam and Zero Detuning **1-D High Gain FEL Equ**<br> **Zero D**<br>  $\frac{d}{dz}B(z) = -i\frac{\omega}{c\gamma_z^2E_0}D(z)$ <br>  $\frac{d}{dz}D = -\frac{1}{2}e\theta_z E$ <br>  $\frac{d}{dz}E = \frac{ec^2n\mu_0\theta_z}{2}B$ <br>  $\Gamma = \left[\frac{\pi j_0\theta_z}{c\gamma_z^2}\right]$ D High Gain FEL Equation for Cold Beam and<br>
Zero Detuning<br>  $=-i\frac{\omega}{c\gamma_z^2E_0}D(z)$ <br>  $=-\frac{1}{2}e\theta_zE$ <br>  $=-\frac{e^2n\mu_0\theta_z}{2}B$ <br>  $\Gamma = \left[\frac{\pi_0\theta_z^2\omega}{c\gamma_z^2\gamma A}\right]^{1/3}$  is the 1-D Gain rate parameter **1-D High Gain FEL Equal <br>** *Zero D***<br>** *d***<sub>***dz</sub>*  $D = -\frac{1}{2}e\theta_s E$ *<br>
<i>d***<sub>***dz</sub>*  $E = \frac{ec^2n\mu_0\theta_s}{2}B$  *<br>
<i>d***<sub>dz</sub>**  $E = \frac{ec^2n\mu_0\theta_s}{2}B$  **<br>** *E* **=**  $\left[\frac{\pi j_0\theta_s^2}{c\gamma_z^2}\right)$ </sub></sub> 1 High Gain FEL Equation for Cold Beam and<br>
Zero Detuning<br>  $=-i\frac{\omega}{c\gamma_z^2E_0}D(z)$ <br>  $\frac{d^3}{dz^3}E=iE$ <br>  $=-\frac{1}{2}e\theta_zE$ <br>  $\frac{e^2n\mu_0\theta_z}{2}B$ <br>  $\Gamma = \left[\frac{\pi_0\theta_z^2\omega}{c\gamma_z^2\gamma I_A}\right]^{1/3}$  is the 1-D Gain rate parameter

1-D High Gain FEL Equat  
\nZero Det  
\n
$$
\frac{d}{dz}B(z) = -i\frac{\omega}{c\gamma_z^2E_0}D(z)
$$
\n
$$
\frac{d}{dz}D = -\frac{1}{2}e\theta_s E
$$
\n
$$
\frac{d}{dz}E = \frac{ec^2n\mu_0\theta_s}{2}B
$$
\n
$$
\Gamma = \left[\frac{\pi_0\theta_s^2\omega}{c\gamma_z^2\gamma I_A}\right]
$$

![](_page_23_Picture_2.jpeg)

![](_page_23_Figure_3.jpeg)

![](_page_23_Figure_4.jpeg)

$$
\frac{d^3}{d\hat{z}^3}E = iE
$$

 $\hat{z} = \Gamma z$  is normalized longitudinal location along wiggler,

$$
\Gamma \equiv \left[ \frac{\pi j_0 \theta_s^2 \omega}{c \gamma_z^2 \gamma I_A} \right]^{1/3}
$$
 is the 1-D Gain rate parameter

$$
I_{A} = \frac{4\pi\varepsilon_{0}mc^{3}}{e}
$$
 is called Alfven current  
\n
$$
\lambda_{1} = e^{i\frac{\pi}{6}} = \frac{\sqrt{3}}{2} + i\frac{1}{2}
$$
Groups and  
\n
$$
\lambda_{2} = e^{i\frac{5\pi}{6}} = -\frac{\sqrt{3}}{2} + i\frac{1}{2}
$$
Comparing mode  
\n
$$
\lambda_{3} = e^{-i\frac{\pi}{2}} = -i
$$

# 1D Gain Length

• At high gain limit, i.e.  $\hat{z} \gg 1$ , the radiation field is given by

$$
E(\hat{z}) \approx B_1 e^{\lambda_k \hat{z}} = B_1 \exp\left[\frac{\sqrt{3}}{2} \Gamma z\right] \exp\left[i\frac{1}{2} \Gamma z\right]
$$

and the radiation power is

$$
P(\hat{z}) = \varepsilon_0 c |E(\hat{z})^2| A = \varepsilon_0 c |B_1|^2 \exp(\sqrt{3}\Gamma z) = \varepsilon_0 c |B_1|^2 A \exp\left(\frac{z}{L_G}\right)
$$

and the 1-D power gain length is

**Pierce Parameter**

**1D Gain Length**  
\nn limit, i.e. 
$$
\hat{z} \gg 1
$$
, the radiation field is given by  
\n $E(\hat{z}) \approx B_1 e^{\lambda_k \hat{z}} = B_1 \exp\left[\frac{\sqrt{3}}{2} \Gamma_z\right] \exp\left[i\frac{1}{2} \Gamma_z\right]$   
\nadiation power is  
\n $\varepsilon_0 c |E(\hat{z})^2| A = \varepsilon_0 c |B_1|^2 \exp\left(\sqrt{3} \Gamma_z\right) = \varepsilon_0 c |B_1|^2 A \exp\left(\frac{z}{L_G}\right)$   
\n-D power gain length is  
\n
$$
L_G = \frac{1}{\sqrt{3}\Gamma} = \frac{\lambda_w}{4\pi\sqrt{3}\rho}
$$
\n $\rho = \frac{\gamma_z^2 \Gamma_c}{\omega} = \frac{\Gamma}{2k_w}$   
\n $\rho = \frac{\gamma_z^2 \Gamma_c}{\omega} = \frac{\Gamma}{2k_w}$   
\n $\rho = \frac{\gamma_z^2 \Gamma_c}{2\pi\sqrt{3}\rho} = \frac{\lambda_w}{2\pi\sqrt{3}\rho}$ 

1-D amplitude gain length is  $\pi \sqrt{3}\rho$  $\lambda$  $3\Gamma$   $2\pi\sqrt{3}\rho$ 2  $\lambda_w$  $L_{GA} = 2L_G \equiv \frac{2}{\sqrt{2E}} = \frac{2L_w}{2\sqrt{2}}$  $\Gamma$   $2\pi\sqrt{3}\rho$  $=2L_G\equiv\frac{2}{\sqrt{2}}=-\frac{N_w}{\sqrt{2}}$ 

#### Solution for Cold Beam with Nonzero Detuning

![](_page_25_Figure_1.jpeg)

$$
(\hat{z}) = E_{ext} \left[ \frac{\lambda_2 \lambda_3 e}{(\lambda_1 - \lambda_2)(\lambda_1 - \lambda_3)} + \frac{\lambda_1 \lambda_3 e}{(\lambda_2 - \lambda_3)(\lambda_2 - \lambda_1)} + \frac{\lambda_1 \lambda_2 e}{(\lambda_3 - \lambda_1)(\lambda_3 - \lambda_2)} \right]
$$

#### Low Gain Limit of High Gain Solution

3  $^{2}$   $^{13}$  $\frac{2\pi i_0 \theta_s^2 \omega}{2} \frac{l_w^3}{l_w^3} = 2\Gamma^3 l_w^3$  $l_w^3$   $2\sqrt{3}l^3$  $\equiv \frac{2\pi j_0 \theta_s^2 \omega l_w^3}{l_w^3} = 2\Gamma^3 l_w^3$  $\pi \partial^2 \omega l^3 = -32$ **Proper limit of<br>
Figure 1. The set of**  $\frac{\overline{g_0}\theta_s^2 \omega}{\overline{c}\gamma_z^2 \gamma} \frac{l_w^3}{I_A} = 2\Gamma^3 l_w^3$ **<br>**  $\hat{C}_l = C l_w$ **<br>
tion factor for** Can we reproduce the previously obtained low gain solution by taking the proper limit of the high gain solution?

Can we reproduce the previously obtained low gain solution by taking the proper limit of  
\nthe high gain solution?  
\n
$$
g_{l} = \frac{(E_{ext} + \Delta E)^{2} - E_{ext}^{2}}{E_{ext}} \approx \frac{2\Delta E}{E_{ext}} = \tau \cdot f(\hat{C}_{l}) = 2\Gamma^{3}l_{w}^{3}f_{l}(\hat{C}_{l})
$$
\n
$$
g_{l} = \frac{2\pi j_{0}\theta_{x}^{2}\omega}{\hat{C}_{l}^{3}}\frac{l_{w}^{3}}{l_{w}} = 2\Gamma^{3}l_{w}^{3}
$$
\n
$$
g_{h}(\hat{C}_{l}) = \frac{\tilde{E}^{2} - E_{ext}^{2}}{E_{ext}} = \frac{\lambda_{2}\lambda_{3}e^{\lambda_{4}l_{w}}}{|\lambda_{1}-\lambda_{2}|\lambda_{1}-\lambda_{3}|} + \frac{\lambda_{1}\lambda_{3}e^{\lambda_{2}l_{w}}}{(\lambda_{2}-\lambda_{3}|\lambda_{2}-\lambda_{1}|)} + \frac{\lambda_{1}\lambda_{2}e^{\lambda_{3}l_{w}}}{(\lambda_{3}-\lambda_{1}|\lambda_{3}-\lambda_{2}|)} = 1
$$
\nThe normalization factor for high gain is different from  
\nthat of low gain:  
\n
$$
i_{w} = l_{w}\Gamma
$$
\n
$$
\hat{C}_{h} = C/\Gamma = Cl_{w}/\hat{l}_{w} = \hat{C}_{l}/\hat{l}_{w}
$$
\n
$$
i_{w} = \frac{\lambda_{1}\lambda_{2}e^{\lambda_{2}l_{w}}}{\lambda_{1}\lambda_{2}e^{\lambda_{3}l_{w}}}
$$
\n
$$
i_{w} = l_{w}\Gamma
$$
\n
$$
\hat{C}_{h} = C/\Gamma = Cl_{w}/\hat{l}_{w} = \hat{C}_{l}/\hat{l}_{w}
$$
\n
$$
i_{w} = \hat{C}_{l}/\hat{l}_{w} = \hat{C}_{l}/\hat{l}_{w}
$$

Let 
$$
\theta
$$
 is the right,  $\theta$  is the right,  $\$ 

$$
f_h(\hat{C}_l) = \frac{1}{2\hat{l}_w^3} \left\{ \left| \frac{\lambda_2 \lambda_3 e^{\lambda_l \hat{l}_w}}{(\lambda_1 - \lambda_2)(\lambda_1 - \lambda_3)} + \frac{\lambda_1 \lambda_3 e^{\lambda_2 \hat{l}_w}}{(\lambda_2 - \lambda_3)(\lambda_2 - \lambda_1)} + \frac{\lambda_1 \lambda_2 e^{\lambda_3 \hat{l}_w}}{(\lambda_3 - \lambda_1)(\lambda_3 - \lambda_2)} \right|^2 - 1 \right\}
$$

2  $-1$  The Hormanization  $\lambda_{3}-\lambda_{1}$   $(\lambda_{3}-\lambda_{2})$  following high gain is different from The normalization factor for that of low gain: oper limit of<br>  $\frac{\omega}{I_A} \frac{l_w^3}{l_x} = 2\Gamma^3 l_w^3$ <br>
=  $Cl_w$ <br>
factor for<br>
nt from<br>  $\hat{l}_w = \hat{C}_l / \hat{l}_w$ <br>  $\hat{l}_w = \hat{C}_l / \hat{l}_w$ <br>  $\hat{l}_w = \hat{l}_l$ <br>  $\hat{C}_l$ 

2.  $I = 2I \nu_w$ 

 $z \sim A$ 

**Gain Solution**  
\nsolution by taking the proper limit of  
\n
$$
\tau = \frac{2\pi_0 \theta_s^2 \omega l_w^3}{c\gamma_z^2 \gamma} = 2\Gamma^3 l_w^3
$$
\n
$$
\hat{C}_l = C l_w
$$
\n
$$
\frac{1 - \cos \hat{C}_l - \frac{\hat{C}_l}{2} \sin \hat{C}_l}{2l} = \frac{1}{\hat{C}_l} \frac{\Gamma}{\Gamma} = 2\Gamma^3 l_w^3
$$
\n
$$
\frac{\hat{C}_l = C l_w}{\Gamma}
$$
\nThe normalization factor for high gain is different from that of low gain:  
\n
$$
\hat{C}_h = C/\Gamma = C l_w / l_w = \hat{C}_l / l_w
$$
\n
$$
\lambda^3 + 2i \frac{\hat{C}_l}{l_w} \lambda^2 - \left(\frac{\hat{C}_l}{l_w}\right)^2 \lambda = i
$$
\n
$$
\frac{1}{\hat{C}_l} \frac{\partial}{\partial t} \left(\frac{\hat{C}_l}{l_w}\right)^2
$$
\n
$$
\frac{1}{\hat{C}_l} \left(\frac{\hat{C}_l}{l_w}\right)^2
$$
\n
$$
\frac{1}{\hat{C}_l} \left(\frac{\hat{C}_l}{l_w}\right)^2
$$

$$
g_{i} = \frac{(\mathcal{L}_{ext} + \Delta E) - \mathcal{L}_{ext}}{E_{ext}} \approx \frac{2\Delta E}{E_{ext}} = \tau \cdot f(\hat{C}_{i}) = 2\Gamma^{3}i_{w}^{3}f_{i}(\hat{C}_{i}) \qquad \left| f_{i}(C_{i}) = \frac{2}{C_{i}^{3}} \left(1 - \cos C_{i} - \frac{C_{i}}{2} \sin C_{i}\right)\right|
$$
\n
$$
g_{\lambda}(\hat{C}_{i}) = \frac{\tilde{E}^{2} - E_{ext}}{E_{ext}} = \left| \frac{\lambda_{2}\lambda_{3}e^{\lambda_{w}^{j}}}{(\lambda_{1} - \lambda_{2})(\lambda_{1} - \lambda_{3})} + \frac{\lambda_{1}\lambda_{2}e^{\lambda_{w}^{j}}}{(\lambda_{2} - \lambda_{3})(\lambda_{2} - \lambda_{1})} + \frac{\lambda_{1}\lambda_{2}e^{\lambda_{w}^{j}}}{(\lambda_{3} - \lambda_{1})(\lambda_{3} - \lambda_{2})}\right| - 1
$$
\nThe normalization factor for high gain is different from that of low gain:  
\n
$$
f_{\lambda}(\hat{C}_{i}) = \frac{1}{2i_{w}^{3}} \left| \frac{\lambda_{2}\lambda_{3}e^{\lambda_{w}^{j}}}{(\lambda_{1} - \lambda_{2})(\lambda_{1} - \lambda_{3})} + \frac{\lambda_{1}\lambda_{3}e^{\lambda_{2}^{j}}}{(\lambda_{2} - \lambda_{3})(\lambda_{2} - \lambda_{1})} + \frac{\lambda_{1}\lambda_{2}e^{\lambda_{w}^{j}}}{(\lambda_{3} - \lambda_{1})(\lambda_{3} - \lambda_{2})}\right| - 1 \right|
$$
\n
$$
f_{\lambda}(\hat{C}_{i}) = \frac{1}{2i_{w}^{3}} \left| \frac{\lambda_{2}\lambda_{3}e^{\lambda_{3}^{j}}}{(\lambda_{1} - \lambda_{2})(\lambda_{1} - \lambda_{3})} + \frac{\lambda_{1}\lambda_{3}e^{\lambda_{2}^{j}}}{(\lambda_{2} - \lambda_{1})(\lambda_{2} - \lambda_{1})} + \frac{\lambda_{1}\lambda_{2}e^{\lambda_{w}^{j}}}{(\lambda_{3} - \lambda_{2})}\right| - 1 \right|
$$
\n
$$
f_{\lambda}(\hat{C}_{i}) = \frac{1}{2i_{w}^{3}} \left| \frac{\lambda_{2}\lambda_{3
$$

 $31^3$ 

*A*  $w = 2^{\Omega}l^3$ 

 $\frac{\partial u}{\partial u} \frac{\partial u}{\partial v} = 2\Gamma^3 l_w^3$  $I_A$ <sup> $\ldots$ </sup>

*w*

# Bandwidth at High Gain Limit I

at High Ga<br>
ights from the exact<br>
ial equation for the<br>
get the approximate<br>
accurate results for<br>  $\frac{0 + a_1 \hat{C} + a_2 \hat{C}^2}{(a_0 + a_1 \hat{C} + a_2 \hat{C})^2}$ **c**<br> **c d width at High Gain Lir**<br>
and to extract insights from the exact<br>
fore, it is useful to get the approximate<br>
simpler but gives accurate results for<br>  $\lambda = i$   $\lambda = a_0 + a_1 \hat{C} + a_2 \hat{C}^2$ <br>  $\lambda^2 = i$   $\lambda = a_0 + a_1 \hat$ **Bandwidth at High Gain L**<br>
between the same of the same time start insights from the exact<br>
on of the 3<sup>*d*</sup> order polynomial equation for the<br>
radius. Therefore, it is useful to get the approximate<br>
gion that we are int **Bandwidth at High Constant Start (1)**<br>
metimes hard to extract insights from the exact<br>
of the 3<sup>rd</sup> order polynomial equation for the<br>
which is simpler but gives accurate results for<br>
on that we are interested in.<br>  $\hat{$ **EXECUTE:**<br> *f* and the examply<br> *f* and the example of the approximation for the useful to get the approximation for the example of the approximation.<br>  $\lambda = a_0 + a_1 \hat{C} + a_2 \hat{C}^2$ <br>  $\frac{a_0 + a_1 \hat{C} + a_2 \hat{C}^2}{a_0 + a_1 \hat{$ Figure 1 **Contains and the exact**<br>
seful to get the approximate<br>
dut gives accurate results for<br>
seted in.<br>  $\lambda = a_0 + a_1 \hat{C} + a_2 \hat{C}^2$ <br>  $\lambda = a_0 + a_1 \hat{C} + a_2 \hat{C}^2$ <br>  $\lambda = a_0 + a_1 \hat{C} + a_2 \hat{C}^2$ <br>  $\lambda = a_0 + a_1 \hat{C} + a_2 \hat{$ It is sometimes hard to extract insights from the exact solution of the 3<sup>rd</sup> order polynomial equation for the eigenvalue. Therefore, it is useful to get the approximate solution which is simpler but gives accurate results for the region that we are interested in.

$$
\lambda^3 + 2i\hat{C}\lambda^2 - \hat{C}^2\lambda = i \qquad \boxed{\lambda = a_0 + a_1\hat{C} + a_2\hat{C}^2}
$$

It is sometimes hard to extract insights from the exact solution of the 3<sup>rd</sup> order polynomial equation for the eigenvalue. Therefore, it is useful to get the approximate solution which is simpler but gives accurate results for the region that we are interested in. 
$$
\lambda^3 + 2i\hat{C}\lambda^2 - \hat{C}^2\lambda = i \qquad \lambda = a_0 + a_1\hat{C} + a_2\hat{C}^2
$$

 $d \left| \left| \hat{c}(\hat{\alpha}) \right| \right| \leq \alpha$ 

 $\left| \frac{\partial}{\partial z} f\left(\hat{C}\right) \right|_{\hat{C}=0} = 0 \Rightarrow \left| a_1 = -i \frac{2}{3} \right|$ 

 $1-\frac{1}{2}$ 

Zeroth order equation:

First order equation:

2  $\qquad \qquad$  $2 J \left( \begin{array}{c} 2 \end{array} \right)$  $\left| \frac{1}{\hat{C}^2} f\left(\hat{C}\right) \right|_{\hat{C}=0} = 0 \Rightarrow \left| a_2 = -\frac{1}{9} \left( \frac{\sqrt{3}}{2} - i \frac{1}{2} \right) \right|$  $d^2$   $c(\hat{c})$  0  $\sqrt{ }$  $2^{\sim}$  0 0

![](_page_27_Figure_7.jpeg)

![](_page_27_Figure_8.jpeg)

#### Bandwidth at High Gain Limit II

After taking the approximate eigenvalue, the radiation field in frequency domain is

**Bandwidth at High Gain Limit II**

\n**traking the approximate eigenvalue, the radiation field in frequency domain is**

\n
$$
E(\hat{C}) : \exp\left[a_0 \hat{z} + a_1 \hat{C} \hat{z} + a_2 \hat{C}^2 \hat{z}\right] : \exp\left[-\frac{\hat{C}^2}{2\sigma_{\hat{C}}^2}\right] \Rightarrow \sigma_{\hat{C}} = \sqrt{-\frac{1}{2\text{Re}(a_2)\hat{z}}}
$$
\nRe(a<sub>2</sub>) =  $-\frac{\sqrt{3}}{18}$   $\sigma_{\hat{C}} = 3\sqrt{\frac{1}{\sqrt{3}\Gamma z}}$   $\hat{C} = \frac{1}{6}\left(k_v - \frac{w}{2\sigma_{\hat{C}}^2}\right)$   $\Gamma = \rho \frac{\omega}{\gamma_z^2 c}$ 

\n**1. bandwidth for radiation field:**

\n
$$
\sigma_{\omega} = \Gamma 2c\gamma_z^2 \sigma_{\hat{C}} = 6c\gamma_z^2 \sqrt{\frac{\Gamma}{\sqrt{3}z}} = 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z}}
$$
\n**1. bandwidth for radiation power:**

\n
$$
\sigma_A = \frac{\sigma_{\omega}}{\sqrt{2}} = \omega_0 \sqrt{\frac{3\sqrt{3}\rho}{k_w z}}
$$
\nThere Parameter

\n
$$
\rho = \frac{\gamma_z^2 \Gamma c}{\gamma_{\omega}^2}
$$

$$
\operatorname{Re}(a_2) = -\frac{\sqrt{3}}{18} \qquad \sigma_{\hat{C}} = 3\sqrt{\frac{1}{\sqrt{3}\Gamma z}} \qquad \hat{C} = \frac{1}{G} \left(k_w - \frac{w}{2cg_z^2}\right) \qquad \Gamma = \rho \frac{\omega}{\gamma_z^2 c}
$$

1D FEL bandwidth for radiation field:

$$
\begin{aligned}\n\text{High Gain Limit II} \\
\text{P, the radiation field in frequency domain is} \\
\frac{\left[ \frac{1}{2\sigma_c^2} \right] \Rightarrow \sigma_{\hat{c}} = \sqrt{-\frac{1}{2\text{Re}(a_2)\hat{z}}}}{\left[ \frac{1}{2\sigma_c^2} \right]} \\
\hat{c} = \frac{1}{6} \left( k_w - \frac{w}{2cg_z^2} \right) \\
\frac{\sigma_w}{\sigma} = \Gamma 2c\gamma_z^2 \sigma_{\hat{c}} = 6c\gamma_z^2 \sqrt{\frac{\Gamma}{\sqrt{3}z}} = 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z}} \\
\frac{\sigma_A}{\sqrt{3}z} = \frac{\sigma_w}{\sqrt{2}} = \omega_0 \sqrt{\frac{3\sqrt{3}\rho}{k_w z}} \\
\frac{\sigma_A}{\sqrt{3}z} = \frac{\sigma_w}{\sqrt{2}} = \omega_0 \sqrt{\frac{3\sqrt{3}\rho}{k_w z}} \\
\rho = \frac{\gamma_z^2 \Gamma c}{\gamma} \n\end{aligned}
$$

1D FEL bandwidth for radiation power:

$$
\sigma_A = \frac{\sigma_{\omega}}{\sqrt{2}} = \omega_0 \sqrt{\frac{3\sqrt{3}\rho}{k_{w}z}}
$$

**Pierce Parameter**

$$
\begin{array}{c}\n\text{min is} \\
\hline\n\overline{a_2}\overline{\smash{\big)}\, \hat{z}} \\
\hline\n\sqrt{\frac{2\rho}{\sqrt{3}k_w z}} \\
\hline\n\text{Piece Parameter} \\
\hline\n\overline{p} = \frac{\gamma_z^2 \Gamma c}{\frac{\rho}{2}} \\
\hline\n\overline{p} = \frac{\gamma_z^2 \Gamma c}{\frac{\rho}{2}}\n\end{array}
$$

![](_page_29_Figure_0.jpeg)

Coherent length is the width of the radiation wave-packet generated by a delta-like excitation.

$$
E(\omega): \exp\left[-\frac{\omega^2}{2\sigma_{\omega}^2}\right] \Rightarrow E(t): \exp\left[-\frac{t^2}{2\sigma_t^2}\right] \implies \boxed{\sigma_t = \frac{|a_2|}{k_0 c}\sqrt{\frac{-k_w z}{\rho \operatorname{Re}(a_2)}} = \frac{1}{3k_0 c}\sqrt{\frac{2k_w z}{\rho\sqrt{3}}} = \frac{2}{3\sqrt{3}\sigma_{\omega}}}
$$

# FEL Gain for warm Beam with Lorentzian Energy

![](_page_30_Figure_1.jpeg)

FEL gain reduced substantially when the relative energy spread become comparable or larger than the Pierce parameter.

# FEL Saturation I

Like any other amplification mechanism, the exponential growth of FEL radiation can not continue forever. One of the criteria to determine the onset of saturation is when there is no electrons to be bunched further, i.e.  $\delta n / n_0 \sim 1$ , which happens to be the point where nonlinear effects starts to take over. **aturation I**<br>a, the exponential growth of I<br>determine the onset of satu<br> $\delta n / n_0 \sim 1$ , which happens to **i** all growth of FEL radiation can<br>onset of saturation is when the<br>ch happens to be the point wh<br>For FEL process starts from sl<br>noise, i.e. SASE, the maximal<br>can be derived as<br> $\delta n / n_0 \sim 1$   $\mathcal{B}_{\text{max}} \leq \sqrt{\frac{N_c}{n_0}} = L_c$ **FEL Saturation |**<br> *n* (*n*) wy other amplification mechanism, the exponential growth of FEL radiation can not<br>
ue forever. One of the criteria to determine the onset of saturation is when there is<br>
trons to be bunched f

![](_page_31_Figure_2.jpeg)

For FEL process starts from shot noise, i.e. SASE, the maximal gain can be derived as

$$
\delta n / n_0 \sim 1 \qquad \qquad \mathcal{S}_{\text{max}} \le \sqrt{\frac{M_e}{N_c}}
$$

 $=L_c$  /  $\lambda_{opt}$  is the ratio between coherent length and the radiation wavelength.

 $M_{_e}$  is the number of electrons in a radiation wavelength.

#### FEL Saturation II

There are other criteria which give similar results for the maximal Gain in SASE:

![](_page_32_Figure_2.jpeg)

![](_page_32_Figure_5.jpeg)

**Hence the Pierce parameter is also** called efficiency parameter.

# FEL Saturation III

• If we use the result that FEL typically saturates at 20 power gain length, the FEL bandwidth at saturation is given by FEL Satu<br>
f we use the result that F<br>
iven by<br>  $\lim_{s\alpha t} = 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z_{sat}}} \approx 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w 20}}$ <br>
L bandwidth for radiation amplitude a<br>  $\frac{\sigma_{\omega, sat}}{\omega_0} = 3\omega_0 \sqrt{\frac{2}{\sqrt{3}}\frac{1}{\sqrt{3}}}$ EL Saturation<br>
2 use the result that FEL typicall<br>
er gain length, the FEL bandwid<br>
n by<br>  $3\omega_{0}\sqrt{\frac{2\rho}{\sqrt{3}k_{w}z_{sat}}} \approx 3\omega_{0}\sqrt{\frac{2\rho}{\sqrt{3}k_{w}20L_{G}}}$ <br>  $L_{G}$ <br>
dwidth for radiation amplitude at saturation:<br>  $\frac{\sigma_{\omega, sat}}{\omega$ FEL Saturation II<br>
i we use the result that FEL typically :<br>
ower gain length, the FEL bandwidth<br>
iven by<br>
sate = 3 $\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_{w}z_{sut}}} \approx 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_{w}20L_G}}$   $L_G =$ <br>
Landwidth for radiation amplitude at s **FEL Saturation III**<br>
If we use the result that FEL typically sat<br>
power gain length, the FEL bandwidth a<br>
given by<br>  $w_{\text{total}} = 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z_{\text{stat}}}} \approx 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w 20L_{\text{G}}}}$   $L_G = \frac{1}{\sqrt{3}}$ <br>
EL bandwidt FEL Saturation III<br>
If we use the result that FEL typically saturates at 20<br>
power gain length, the FEL bandwidth at saturation is<br>
given by<br>  $\sigma_{m,w} = 3\omega_0 \sqrt{\frac{2\rho}{3k_w z_{wav}}} \approx 3\omega_0 \sqrt{\frac{2\rho}{3k_w 20L_c}}$   $L_c = \frac{1}{\sqrt{3}\Gamma} = \frac{\$ **Saturation III**<br>that FEL typically saturates as<br>the FEL bandwidth at satura<br> $\sqrt{\frac{2\rho}{\sqrt{3}k_w 20L_G}}$   $L_G = \frac{1}{\sqrt{3}\Gamma} = \frac{\lambda_w}{4\pi\sqrt{3}}$ <br>nplitude at saturation:<br> $3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z_{sat}}} \approx \rho \sqrt{1.8}$ <br>wer at saturation:<br> $\frac{$ **Fation |**<br> **FEL typically**<br> **WE SECUTE 15 16**<br> **WE SECUTE 16**<br> **Example 16**<br> **Example 2**<br> EL Saturation III<br>
result that FEL typically saturates at 20<br>
result that FEL bandwidth at saturation is<br>  $L_G = \frac{1}{\sqrt{3\Gamma}} = \frac{\lambda_w}{4\pi\sqrt{3}\rho}$ <br>
iation amplitude at saturation:<br>  $\frac{\sigma_{o, \text{sat}}}{\omega_0} = 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z_{\text$ **Saturation III**<br>
It that FEL typically saturates at 20<br>
, the FEL bandwidth at saturation is<br>  $L_G = \frac{1}{\sqrt{3}\Gamma} = \frac{\lambda_w}{4\pi\sqrt{3}\rho}$ <br>
amplitude at saturation:<br>  $= 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z_{sat}}} \approx \rho \sqrt{1.8}$ <br>
sower at saturation:<br> **Saturaller**<br>
t that FEL typic<br>
, the FEL bandy<br>  $\sqrt{\frac{2\rho}{\sqrt{3}k_w 20L_G}}$ <br>
amplitude at saturation<br>
=  $3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z_{sat}}} \approx \rho$ <br>
power at saturation:<br>  $\frac{S, sat}{S} = \frac{\sigma_{\omega, sat}}{\sqrt{2}\omega_0} = \sqrt{0.9}\rho$ **L Saturation III**<br> **A** suit that FEL typically saturates at 20<br>
th, the FEL bandwidth at saturation is<br>  $\frac{3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w 20L_c}}}$   $L_G = \frac{1}{\sqrt{3}\Gamma} = \frac{\lambda_w}{4\pi\sqrt{3}\rho}$ <br>  $\frac{3\omega_0}{\sqrt{\frac{2\rho}{\sqrt{3}k_w z_{var}}} \approx \rho\sqrt{1.8}}$ <br>
A **aturation III**<br>
hat FEL typically saturates at 20<br>
he FEL bandwidth at saturation is<br>  $\frac{2\rho}{\sqrt{3}k_{w}20L_{c}}$   $L_{G} = \frac{1}{\sqrt{3}\Gamma} = \frac{\lambda_{w}}{4\pi\sqrt{3}\rho}$ <br>
blitude at saturation:<br>  $\omega_{0}\sqrt{\frac{2\rho}{\sqrt{3}k_{w}z_{sat}}} \approx \rho\sqrt{1.8}$ <br>
er a

$$
\sigma_{\omega, sat} = 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w z_{sat}}} \approx 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_w 20L_G}} \qquad L_G \equiv \frac{1}{\sqrt{3}\Gamma} = \frac{\lambda_w}{4\pi\sqrt{3}\rho}
$$

FEL bandwidth for radiation amplitude at saturation:

$$
\frac{\sigma_{\omega,sat}}{\omega_0} = 3\omega_0 \sqrt{\frac{2\rho}{\sqrt{3}k_{w}z_{sat}}} \approx \rho\sqrt{1.8}
$$

FEL bandwidth for radiation power at saturation:

$$
\frac{\sigma_{A,sat}}{\omega_0} = \frac{\sigma_{\omega,sat}}{\sqrt{2}\omega_0} = \sqrt{0.9} \rho \approx \rho
$$
\nPiece parameter is re-  
equal to the bandwidth  
the FEL at saturation.

 $[0.9 \rho \approx \rho]$  equal to the bandwidth of Pierce parameter is roughly 34

# 3D Effects: Diffraction

![](_page_34_Figure_1.jpeg)

 $(z) = w_{01} |1 + \frac{z}{z}$ 2 *R z*  $\left\lceil \frac{1}{2} \right\rceil$  $z_R$ ) The radius of the radiation at a given distance is given by

The Rayleigh length or Rayleigh range is the distance along the propagation direction of a beam from the waist to the place where the area of the cross section is doubled.  $\sqrt{\frac{z}{z_R}}$ <br>
n direction of a<br>
bubled.

For a Gaussian radiation beam:

$$
z_R = \frac{\pi w_0^2}{\lambda_{opt}}
$$

The size of the electron beam and the seeding radiation field optics have to be properly chosen so that the interaction efficiency between radiation fields and electrons can be optimized.

## Three Dimensional Effects: 3D Gain

- In reality, the gain length will be longer than the 1D gain length due to diffraction, electron emittance, and electron beam energy spread. It is difficult to obtain a general analytical expression for the gain length with all these effects taken into account.
- The analytical approach typically involves expansion over a series of transverse modes.
- For the dominant transverse mode, there is a fitting formula derived by Ming Xie, which is typically of the accuracy of 10% compared with simulation results.

Ming Xie's fitting formula for 3D gain length

$$
L_{\rm 3D}=L_{\rm 1D}\left(1+\Lambda\right)
$$

$$
\Lambda = 0.45\eta_d^{0.57} + 0.55\eta_{\varepsilon}^{1.6} + 3\eta_{\gamma}^2 + 0.35\eta_{\varepsilon}^{2.9}\eta_{\gamma}^{2.4} + 51\eta_d^{0.95}\eta_{\gamma}^3 + 0.62\eta_d^{0.99}\eta_{\varepsilon}^{1.1}
$$
  
+5.3 $\eta_d^{0.76}\eta_{\varepsilon}^{2.3}\eta_{\gamma}^{2.7} + 120\eta_d^{2.1}\eta_{\varepsilon}^{2.9}\eta_{\gamma}^{2.8} + 3.7\eta_d^{0.43}\eta_{\varepsilon}\eta_{\gamma}$ 

Energy spread effects  
\n
$$
\eta_{\gamma} = \left(\frac{L_{1D} 4\pi}{\lambda_{w}}\right) \frac{\delta \gamma}{\gamma}
$$
\n
$$
\eta_{\varepsilon} = \left(\frac{L_{1D} 4\pi}{\beta_{b} \gamma \lambda}\right) \varepsilon_{n}
$$
\n
$$
\eta_{d} = \frac{L_{1D}}{Z_{R}}
$$

#### Three-Dimensional Effects: transverse modes

Cylindrical coordinates, Laguerre-Gaussian modes Cartesian coordinates, Hermite-Gaussian modes

![](_page_36_Picture_2.jpeg)

![](_page_36_Figure_4.jpeg)

![](_page_36_Figure_5.jpeg)

FIG. 9. (Color) Evolution of the LCLS transverse profiles at different  $\zeta$  locations (courtesy of Sven Reiche, UCLA).