Options for Coherent electron Cooling

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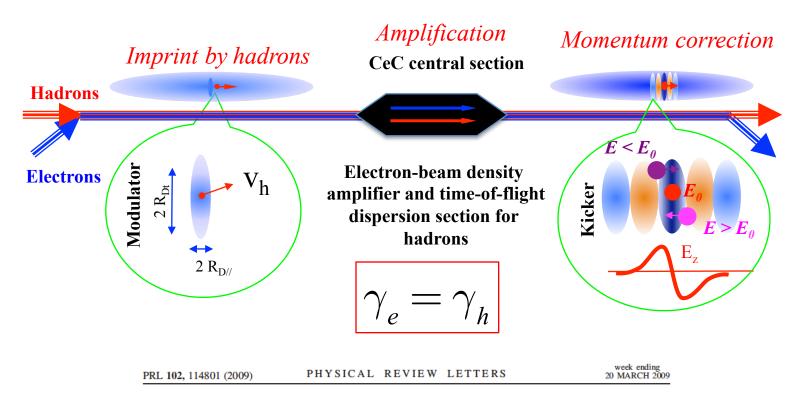
Outline

- ☐ Options for Coherent electron Cooling
- ☐ What are advantages of various schemes
- ☐ What can be tested?
- ☐ How to evaluate cooling
- Conclusions

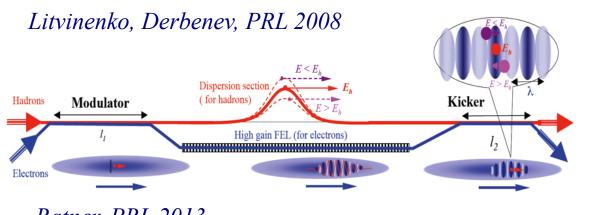
What is Coherent electron Cooling



- Short answer stochastic cooling of hadron beams with bandwidth at optical wave frequencies: 1 1000 THz
- Longer answer



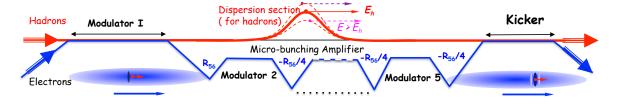
Coherent Electron Cooling





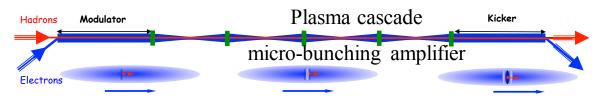
High gain FEL amplifier

Ratner, PRL 2013



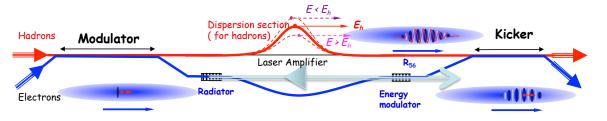
Multi- Chicane Microbunching amplifier

Litvinenko, Wang, Kayran, Jing, Ma, 2017



Plasma-Cascade Microbunching amplifier

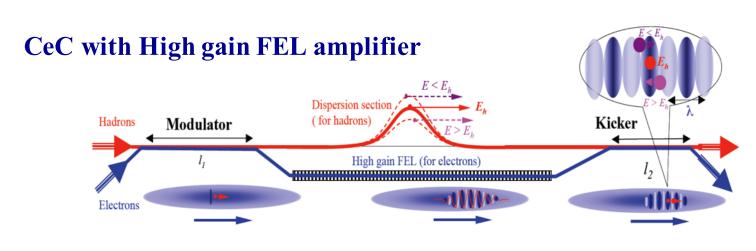
Litvinenko, Cool 13



Hybrid laserbeam amplifier

- The best studied and fully explored scheme
- Experimentally demonstrated both as instability and amplifier
- 3D FEL theory and simulation are very advanced
- Can operate at relatively low electron beam peak currents
- Allows in principle economic option without separating electron and hadron beams

- When compared with microbunching amplifier, it has relatively lower bandwidth ~ few % of the FEL frequency
- FEL saturates at lower gain than micro-bunching amplifier
- Semi-periodic structure of the modulation limits the range where cooling occurs

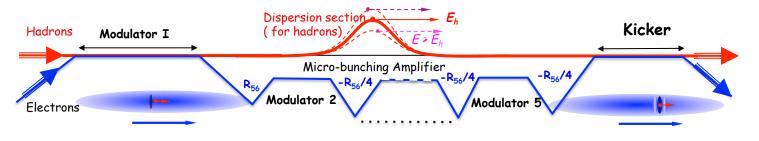




- Very broad band amplifier
- Micro-bunching instability was experimentally demonstrated
- Can operate at significant gain without saturation and can be extended to LHC energies
- Ratner's original scheme is in principle insensitive to longitudinal space charge effects in the electron beam

- Micro-bunching amplifier was not demonstrated
- Less studied especially numerically in 3D than other CeC schemes
- Requires electron beam with low energy spread
- Definitely require separation of electron and hadron beams

Multi-Chicane Microbunching amplifier

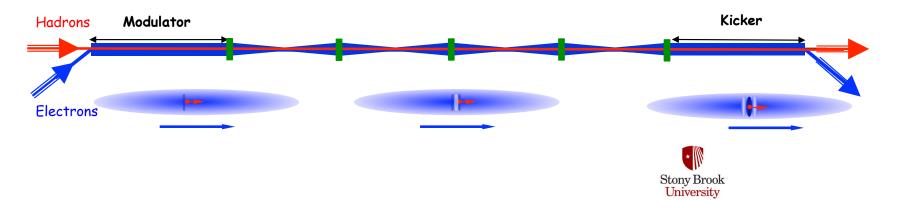




- Very broad band amplifier, can operate at significant gain without saturation
- Plasma-cascade micro-bunching instability was experimentally demonstrated
- Has good theoretical model and is extensively studied in 3D numerical simulations
- Cool hadrons with all energy deviation (no anti-cooling)
- Does not require (full) separation of electron and hadron beams

- Micro-bunching amplifier was not demonstrated
- Requires better quality electron beam than FEL amplifier
- Can operate for medium hadron energies (up to hundreds of GeV, such as US EIC), but can not be extended to LHC energies
- Less studied than FEL-based CeC

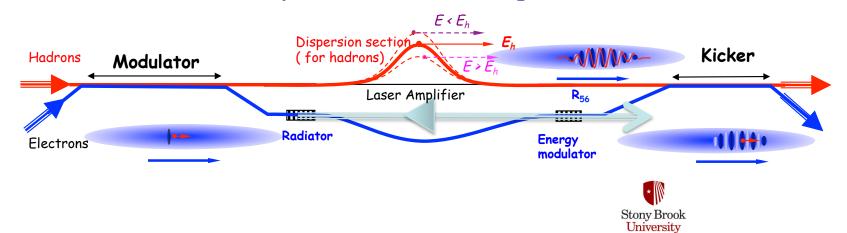
Plasma-Cascade Microbunching amplifier



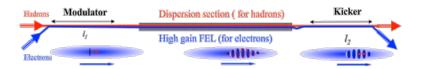
- Relatively broad-band amplifier
- Take advantage of laser technology
- Does not require high peak current electron beam
- Take advantage of flexibility provided by high K-wigglers to adjust wavelength of radiation to that of the laser-amplifier
- Has some synergy with opticalstochastic cooling

- Not studied in details
- Definitely require separation of electron and hadron beams
- Would require rather significant delay of the hadron beam – may require R₅₆ reduction scheme for hadrons
- Semi-periodic structure of the modulation limits the energy range where cooling occurs

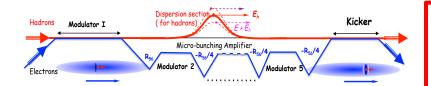
Hybrid laser-beam amplifier



What can be tested experimentally?

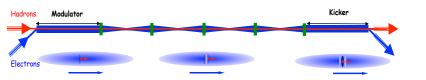




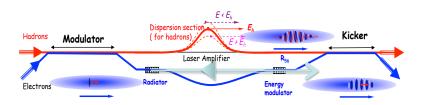


Cooling test requires serious modification of the RHIC lattice & superconducting magnets +\$20-\$30M OR

Building new CeC system at another hadron storage ring







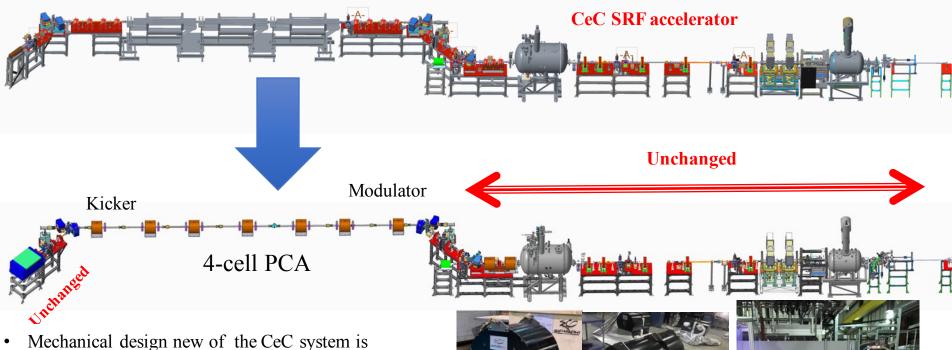
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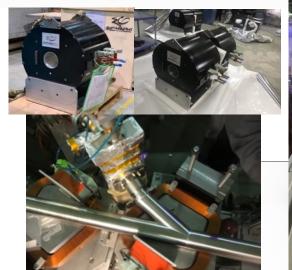
Changing CeC amplifier from FEL to PCA

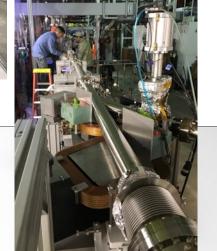


Small gap in FEL wigglers is not compatible with low energy RHIC operations of the Beam Energy Scan (BES-II) program



- Mechanical design new of the CeC system is completed. We used SBU NSF "Center for Accelerator Science and Education" grant to procure new hardware
- We procured and commissioned new laser system with controllable pulse structure
- All new vacuum chambers with beam diagnostics are built and installed
- All supports are built and installed
- All solenoids are designed, manufactured, delivered and undergo magnetic measurements
- Assembly of the plasma-cascade based CeC can be completed during this year's RHIC shut-down





How to evaluate CeC: the original recipe University

Free Electron Lasers and High-energy Electron Cooling, Vladimir N. Litvinenko, Yaroslav S. Derbenev, Proceedings of 29th International Free Electron Laser Conference, Novosibirsk, Russia, August 27-31, 2007

• Linear response of electron beam on perturbations – no saturation, superposition principle

$$\begin{split} \delta\vec{\mathbf{E}}_{h} &= Ze \cdot \vec{\mathbf{G}}_{Eh} (\vec{r}, \vec{r}_{h}, \gamma_{h}, t, t_{h}); \delta\vec{\mathbf{B}}_{h} = Ze \cdot \vec{\mathbf{G}}_{Bh} (\vec{r}, \vec{r}_{h}, \gamma_{h}, t, t_{h}); \\ \delta\vec{\mathbf{E}}_{e} &= -e \cdot \vec{\mathbf{G}}_{Ee} (\vec{r}, \vec{r}_{e}, \gamma_{e}, t, t_{e}); \delta\vec{\mathbf{B}}_{e} = -e \cdot \vec{\mathbf{G}}_{Be} (\vec{r}, \vec{r}_{e}, \gamma_{e}, t, t_{e}); \\ \vec{\mathbf{E}} &= Ze \cdot \sum_{h} \vec{\mathbf{G}}_{Eh} (\vec{r}, \vec{r}_{h}, \gamma_{h}, t, t_{h}) - e \cdot \sum_{e} \vec{\mathbf{G}}_{Ee} (\vec{r}, \vec{r}_{e}, \gamma_{e}, t, t_{e}); \\ \vec{\mathbf{B}} &= Ze \cdot \sum_{h} \vec{\mathbf{G}}_{Bh} (\vec{r}, \vec{r}_{h}, \gamma_{h}, t, t_{h}) - e \cdot \sum_{e} \vec{\mathbf{G}}_{Be} (\vec{r}, \vec{r}_{e}, \gamma_{e}, t, t_{e}) \end{split}$$

- Evaluation of hadron distribution function using Fokker-Plank equation with both damping and diffusion terms
- Cooling transversely using coupling with longitudinal degrees of freedom

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• Linear response of electron beam on perturbations – no saturation, superposition principle

$$\delta E_{i} = eZ \int \vec{\mathbf{E}} \cdot d\vec{r}_{i}; \quad \delta \vec{p}_{i} = eZ \int \left(\vec{\mathbf{E}} + \frac{\left[\vec{p}_{i} \times \vec{\mathbf{B}} \right]}{\gamma_{i}m} \right) \cdot dt; \quad X^{T} = (x, P_{x}, y, P_{y}, z, P_{z});$$

$$\delta E_{i} = (eZ)^{2} \cdot g_{Eh}(X_{i}, t_{i}) - Ze^{2} \cdot g_{Ee}(X_{i}, t_{i});$$

$$g_{Eh}(X_{i}, t_{i}) = \sum_{h} \int \vec{\mathbf{G}}_{Eh}(\vec{r}_{i}, \vec{r}_{h}, \gamma_{h}, t_{i}, t_{h}) \cdot d\vec{r}_{i}; \quad g_{Ee} = \int \sum_{e} \vec{\mathbf{G}}_{Ee}(\vec{r}_{i}, \vec{r}_{e}, \gamma_{e}, t_{i}, t_{e}) \cdot d\vec{r}_{i};$$

$$\delta \vec{p}_{i} = (eZ)^{2} \cdot \vec{g}_{ph}(X_{i}, t_{i}) - Ze^{2} \cdot \vec{g}_{pe}(X_{i}, t_{i});$$

$$\vec{g}_{ph}(X_{i}, t_{i}) = \sum_{h} \int \left(\vec{\mathbf{G}}_{Eh} + \frac{\left[\vec{p}_{i} \times \vec{\mathbf{G}}_{Bh} \right]}{\gamma_{i}m} \right) \cdot dt_{i}; \quad \vec{g}_{pe} = \sum_{e} \int \left(\vec{\mathbf{G}}_{Ee} + \frac{\left[\vec{p}_{i} \times \vec{\mathbf{G}}_{Be} \right]}{\gamma_{i}m} \right) \cdot dt_{i}$$

- Evaluation of hadron distribution function using Fokker-Plank equation with both damping and diffusion terms
- Cooling transversely using coupling with longitudinal degrees of freedom

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- Linear response of electron beam on perturbations no saturation, superposition principle
- Evaluation of hadron distribution function using Fokker-Plank equation with both damping and diffusion terms

$$\overline{f} = \left\langle \widetilde{f} \right\rangle; \widetilde{f} = \sum_{h} \delta \left(X - X_{i}(t) \right)$$

$$\frac{\partial \overline{f}(X,s)}{\partial t} + \frac{\partial}{\partial X_{i}} \left[\frac{dX_{i}(X,t)}{dt} \overline{f}(X,s) \right] - \frac{1}{2} \frac{\partial^{2}}{\partial X_{i} \partial X_{k}} \left[D_{ik}(X,t) \overline{f}(X,t) \right] = 0$$

$$\left\langle \frac{dX_{i}(X,t)}{dt} \right\rangle = \frac{1}{\tau} \int (X_{i} - Z_{i}) \cdot W(Z,X|\tau,t) dZ = \frac{1}{T_{o}} \left\langle \delta X_{i} \right\rangle$$

$$2D_{ik}(X,t) = \frac{1}{2\tau} \int (X_{i} - Z_{i}) (X_{k} - Z_{k}) W(Z,X|\tau,t) dZ = \frac{1}{T_{o}} \left\langle \delta X_{i} \cdot \delta X_{i} \right\rangle$$

Cooling transversely using coupling with longitudinal degrees of freedom



Transverse cooling: the original recipe

• Cooling transversely using coupling with longitudinal degrees of freedom by making energy kick depending on transverse motion (via R_{51} , R_{52} , R_{53} , R_{54} or by displacing beam center in the kicker section)

$$X^{T} = [x, x', y, y', \tau, \delta]; \tau = -c(t - t_{o}); \delta = \frac{E - E_{o}}{\beta_{o} E_{o}};$$

$$\Delta E = F(X); \Delta \delta \equiv \Delta x_{6} = \frac{F(X)}{\beta_{o} E_{o}} \approx const - \sum_{i=1}^{6} \zeta_{i} \cdot x_{i};$$

$$\Delta X^{T} = \begin{bmatrix} 0 & 0 & 0 & 0 & \Delta x_{6} \end{bmatrix}; S = \begin{bmatrix} \sigma & 0 & 0 & 0 \\ 0 & \sigma & 0 & 0 \\ 0 & 0 & \sigma & 0 \end{bmatrix}; \sigma = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -1 & 0 & 0 & 0 \end{bmatrix};$$

$$X = \sum_{k=1}^{3} (a_{k} Y_{k} e^{i\psi_{k}} + a_{k}^{*} Y_{k}^{*} e^{-i\psi_{k}}); \quad Y_{j} S Y_{k}^{*T} = -2i\delta_{kj}; Y_{k}^{T} = \begin{bmatrix} y_{1k} & y_{2k} & y_{3k} & y_{4k} & y_{5k} & y_{6k} \end{bmatrix};$$

$$\Delta a_{k} = \frac{i}{2} \Delta X^{T} S Y_{k}^{*T} = \frac{iy_{5k}^{*}}{2} \Delta x_{6} e^{-i\psi_{k}} = -\frac{iy_{5k}^{*}}{2} e^{-i\psi_{k}} \sum_{i=1}^{6} \zeta_{i} \cdot x_{i}; \quad x_{i} = \sum_{j=1}^{3} (a_{j} y_{ij} e^{i\psi_{j}} + a_{k}^{*} Y_{k}^{*} e^{-i\psi_{k}});$$

$$\Delta a_{k} = -\frac{iy_{5k}^{*}}{2} \sum_{i=1}^{6} \zeta_{i} \sum_{j=1}^{3} a_{j} y_{ij} e^{i(\psi_{j} - \psi_{k})} \rightarrow \langle \Delta a_{k} \rangle = -\xi_{k} a_{k} \rightarrow a_{k} = a_{k0} e^{-n\xi_{k}}; \quad \sum_{k} \operatorname{Re} \xi_{k} = \operatorname{Tr} D = \zeta_{6} \equiv \zeta_{\delta}$$

$$\left\langle e^{i(\psi_{j} - \psi_{k})} \right\rangle = \delta_{kj}; \left\langle e^{-i(\psi_{j} + \psi_{k})} \right\rangle = 0; \quad \xi_{k} = \frac{i}{2} \sum_{i=1}^{6} \zeta_{i} y_{5k}^{*} y_{ik}; \quad \operatorname{Re} \xi_{k} = \operatorname{Im} \sum_{i=1}^{6} \zeta_{i} y_{5k}^{*} y_{ik}$$



Transverse cooling: the original recipe

• Cooling transversely using coupling with longitudinal degrees of freedom by making energy kick depending on transverse motion (via R₅₁, R₅₂, R₅₃, R₅₄ or by displacing beam center in the kicker section) – we can only redistribute cooling decrements between three eigen modes

$$\langle \Delta a_k \rangle = -\xi_k a_k \rightarrow a_k = a_{k0} e^{-n\xi_k}; \quad \xi_k = \frac{i}{2} \sum_{i=1}^6 \zeta_i y^*_{5k} y_{ik}; \quad \sum_k \xi_k = TrD = \zeta_6 \equiv \zeta_\delta$$

For slow synchrotron oscillations ($Q_s << 1$)

$$Q_{s} << Q_{1,2}$$

$$Y_{1k}$$

$$Y_{2k}$$

$$Y_{3k}$$

$$Y_{4k}$$

$$Y_{5k}$$

$$Y_{5k}$$

$$Q_{s} << Q_{1,2}$$

$$Y_{k\beta}$$

Hence, introduction dependencies on the components of transverse motion and non-zero dispersion in the kicker section allows to re-distribute cooling decrements

Instead of conclusion

- ✓ There is a variety of amplifiers suitable for CeC
 - ✓ In addition to what we discussed now, Yaroslav Derbenev is proposing using coherent synchrotron radiation instability as CeC amplifier one need a specific schematic to understand how it fit into the CeC family
- ✓ Theoretical evaluation is typically limited to 1D, but 3D simulation are performed for two CeC schemes
- ✓ Two CeC options can be tested experimentally at RHIC we currently pursuing CeC with plasma-cascade amplifier
- ✓ The evaluation scheme that I presented only looking simple evil is always in details
- ✓ Following presentations will give a much deeper view into physics and realities of CeC





Sum of decrements theorem



Let's consider an arbitrary linear s-dependent equation:

$$\frac{dX}{ds} = \mathbf{D}(s) \cdot X; \tag{SD-1}$$

e.g. the overall motion is not necessary symplectic

$$X(s) = \mathbf{R}(s)X_o \to \frac{d\mathbf{R}}{ds} = \mathbf{D}\mathbf{R} \to \frac{d}{ds} \det[\mathbf{R}(s)] = Trace[\mathbf{D}(s)] \cdot \det[\mathbf{R}(s)]$$

$$\det[\mathbf{R}(s)] = \int_{0}^{s} Trace[\mathbf{D}(\xi)] d\xi.$$
(SD-2)

Prove of the later is rather trivial

$$\mathbf{R}(s+ds) = (\mathbf{I} + ds\mathbf{D}(s^*) + ds^2\mathbf{O}) \cdot \mathbf{R}(s); \ s^* \in \{s, s + ds\} \rightarrow \det \mathbf{R}(s+ds) = \det (\mathbf{I} + ds\mathbf{D}(s^*) + ds^2\mathbf{O}) \cdot \det \mathbf{R}(s);$$

$$\det A = \sum_{i,j,k} \varepsilon_{ijk-} a_{1i} a_{2j} a_{3k} \cdots ; \det (\mathbf{I} + ds\mathbf{D}(s^*) + \varepsilon^2\mathbf{O}) = \sum_{i,j,k} \varepsilon_{ijk-} (\delta_{1i} + dsd_{1i}) (\delta_{2j} + dsd_{2j}) (\delta_{3k} + dsd_{3k}) \dots + O(\varepsilon^2)$$

$$\sum_{i,j,k} \varepsilon_{ijk-} (\delta_{1i} + dsd_{1i}) (\delta_{2j} + dsd_{2j}) (\delta_{3k} + dsd_{3k}) \dots = \prod_{i=1}^{2n} (\delta_{ii} + dsd_{ii}) + ds^2 \sum_{i,j,k} \varepsilon_{ijk-1} d_{1i} \sum_{i,j,k} \varepsilon_{ijk-1} (\delta_{2j} + dsd_{2j}) (\delta_{3k} + dsd_{3k}) \dots d_{j1} \dots +$$

$$+ ds^2 \sum_{i,j\neq2,k} \varepsilon_{ijk-} \sum_{i,j,k} \varepsilon_{ijk-1} (\delta_{1i} + dsd_{1i}) d_{2j} (\delta_{3k} + dsd_{3k}) \dots d_{j2} + \dots = \prod_{i=1}^{2n} (\delta_{ii} + dsd_{ii}) + O(ds^2);$$

$$\prod_{i=1}^{2n} (\delta_{ii} + dsd_{ii}) = 1 + ds \sum_{i=1}^{2n} d_{ii} + O(ds^2) = 1 + ds \cdot Tr[\mathbf{D}(s^*)];$$

$$\det \mathbf{R}(s + ds) \equiv \det \mathbf{R}(s) + d(\det \mathbf{R}(s)) + O(ds^2) = (1 + ds \cdot Tr[\mathbf{D}(s^*)] + O(ds^2)) \cdot \det \mathbf{R}(s);$$

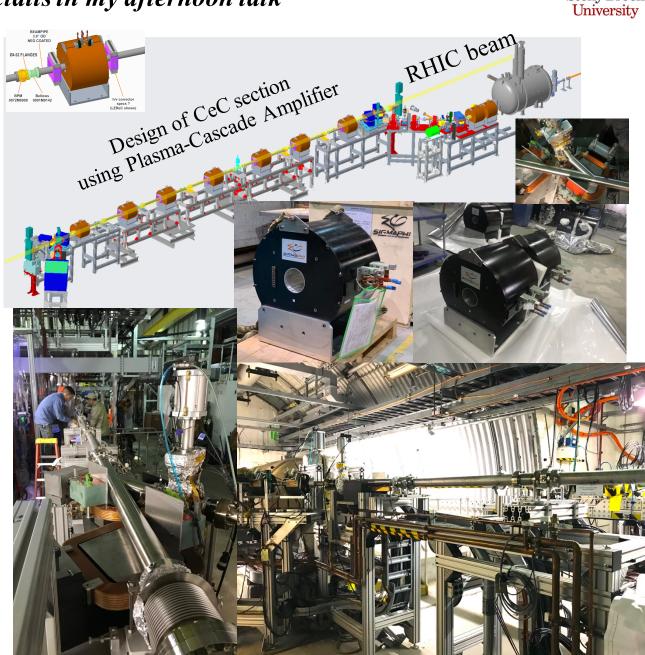
$$ds \rightarrow 0 \Rightarrow d(\det \mathbf{R}(s)) = ds \cdot Tr[\mathbf{D}(s)] \cdot \det \mathbf{R}(s).$$

$$(SD 2)$$

Status: more details in my afternoon talk



- Mechanical design new CeC system is completed
- We procured and commissioned new laser system with controllable pulse structure
- All new vacuum with beam diagnostics are built chambers are installed
- All supports are built and installed
- All solenoids are designed, manufactured, delivered and undergo magnetic measurements
- Assembly of the plasmacascade based CeC can be completed during this year's RHIC shut-down period



Distribution of the decrements

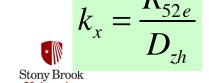
$$X = \frac{1}{2} \sum_{k=1}^{3} (a_k Y_k(s) e^{i\psi_k} + c.c.); \quad Y_j^{*T} S Y_k = 2i\delta_{jk}; Y_j^T S Y_k = 0; \quad S = \begin{bmatrix} \sigma & 0 & 0 \\ 0 & \sigma & 0 \\ 0 & 0 & \sigma \end{bmatrix}; \sigma = \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix}$$

$$\delta a_{k} = -\xi \frac{e^{-i\psi_{k}}}{2i} Y_{k}^{*T} SK \cdot \sum_{j=1}^{3} (a_{j} Y_{j}(s) e^{i\psi_{j}} + c.c.);$$

$$\xi_{k} = \frac{\langle \delta a_{k} \rangle}{a_{k}} = -\xi \frac{Y_{k}^{*T} SKY_{k}}{2i}; \qquad 2 \cdot \sum_{k=1}^{3} \xi_{k} = \xi \cdot Tr(K) = \xi;$$

$$\xi_{k} = \frac{\xi}{2i} \cdot Y_{k}^{5*} (k_{x} Y_{k}^{1} + Y_{k}^{6})$$

$$X^{T} = \{x, x', y, y', -c\tau, \delta\}$$



Distribution of the decrements

$$Y_{k=1,2} \cong \begin{pmatrix} Y_{k1} \\ Y_{k2} \\ Y_{k3} \\ Y_{k5} \\ 0 \end{pmatrix} = \begin{pmatrix} Z_{k} \\ -Z_{k}^{T}SD \\ 0 \end{pmatrix}; Y_{3} \cong \frac{1}{\sqrt{\Omega}} \begin{pmatrix} D_{x} \\ D_{x}^{T} \\ D_{y} \\ D_{y}^{T} \\ i\Omega \\ 1 \end{pmatrix};$$

$$\xi_{k} = \frac{\xi}{2i} \cdot Y_{k}^{*5} \left(k_{x}Y_{k}^{1} + Y_{k}^{6}\right)$$

$$\xi_{s} = \frac{\xi}{2} \left(k_{x}D_{x} + 1\right);$$

$$\xi_{s=1,2} = -\frac{\xi}{2i} \cdot \left(Z_{k}^{*T}SD\right) \cdot k_{x}Z_{k}^{1}$$

$$\xi_{k=1,2} = -k_{x}D_{x}\frac{\xi}{2}$$

Uncoupled case

$$\xi_{y} = 0; \quad \text{Re}\,\xi_{x} = -\frac{\xi}{2} \cdot R_{52e} \frac{D_{xh}}{D_{zh}}; \quad \text{Re}\,\xi_{s} = \frac{\xi}{2} \cdot \left(1 - R_{52e} \frac{D_{xh}}{D_{zh}}\right)$$

