

## 1894 **Relativistic Cyclotron**

1895 **Abstract** This chapter introduces the AVF (azimuthally varying field), isochronous,  
1896 relativistic cyclotron, and to the theoretical material needed for the simulation exer-  
1897 cises. A brief reminder of the historical context is followed by further basic theoretical  
1898 considerations leaning on the cyclotron concepts introduced in Chapter 3 and in-  
1899 cluding

- 1900 - Thomas focusing and the AVF cyclotron,
- 1901 - positive focusing index,
- 1902 - isochronous optics,
- 1903 - separated sector cyclotrons,
- 1904 - spin dynamics in an AVF cyclotron.

1905 Simulation exercises use optical elements and keywords met earlier: the analytical  
1906 field modeling DIPOLE, TOSCA in case using a field map is preferred, CAVITE to  
1907 accelerate, SPNTRK to solve spin motion, FAISCEAU, FAISTORE, FIT, etc. The  
1908 exercises further develop on radial and spiral sector magnets, edge focusing and  
1909 flutter, isochronous optics, separated sector ring cyclotrons, and their modeling in  
1910 DIPOLE, DIPOLES and other CYCLOTRON keyword capabilities.

1911 **Notations used in the Text**

$B; B_0$	magnetic field; at a reference radius $R_0$
$\mathbf{B}; B_R; B_\theta; B_y$	field vector; radial, azimuthal and axial components
$BR = p/q; BR_0$	magnetic rigidity; reference rigidity
$C; C_0$	closed orbit length, $C = 2\pi R$ ; reference, $C_0 = 2\pi R_0$
$E$	ion energy, $E = \gamma m_0 c^2$
EFB	effective Field Boundary
$\mathcal{F}; F$	azimuthal field form factor; flutter, $F = \left( \frac{\langle (\mathcal{F} - \langle \mathcal{F} \rangle)^2 \rangle}{\langle \mathcal{F} \rangle^2} \right)^{1/2}$
$f_{\text{rev}}, f_{\text{rf}}$	revolution and RF voltage frequencies
$h$	harmonic number, an integer, $h = f_{\text{rf}} / f_{\text{rev}}$
$k = \frac{R}{B} \frac{dB}{dR}$	geometric index, a global quantity
$m; m_0; M$	ion mass; rest mass; in units of $\text{MeV}/c^2$
$n = \frac{\rho}{B} \frac{dB}{d\rho}$	focusing index, a local quantity
$\mathbf{p}; p_0$	ion momentum vector; reference momentum
$q$	ion charge
$R; R_0; R_E$	average radius of equilibrium orbit; $R = C/2\pi$ ; $R(p = p_0)$ ; $R(E)$
$\mathcal{R}$	radial field form factor
1912 $RF$	Radio-Frequency
$s$	path variable
$T_{\text{rev}}, T_{\text{rf}}$	revolution and accelerating voltage periods
$v$	ion velocity
$V(t); \hat{V}$	oscillating voltage; its peak value
$x, x', y, y'$	radial and axial coordinates $\left[ (*)' = \frac{d(*)}{ds} \right]$
$\alpha$	trajectory deviation, or momentum compaction
$\beta = v/c; \beta_0; \beta_s$	normalized ion velocity; reference; synchronous
$\gamma = E/m_0 c^2$	Lorentz relativistic factor
$\Delta p, \delta p$	momentum offset
$\varepsilon$	wedge angle
$\varepsilon_R$	strength of a depolarizing resonance
$\varepsilon_u$	Courant-Snyder invariant ( $u : x, y, l, \dots$ )
$\zeta$	spiral angle of a spiral sector dipole EFB
$\theta$	azimuthal angle
$\phi; \phi_s$	phase of oscillating voltage; synchronous phase

1913 **3.1 Introduction**

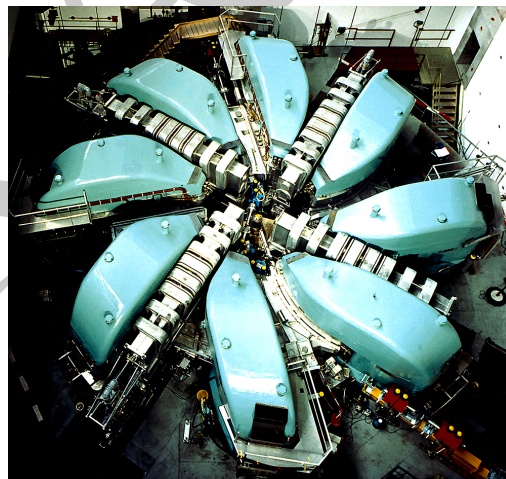
1914 Isochronous cyclotrons are in operation today by the thousands, tens are produced  
 1915 each year. Applications include production of radio-isotopes mostly, proton therapy  
 1916 (Fig. 3.1), high power beams for accelerator-driven systems, secondary particle beam

1917 production (Fig. 3.2), and more [1]. The technology and its applications are fostered  
1918 by cryogeny and high fields which further allow compactness (Fig. 3.1) as well as  
1919 highest beam rigidities (Fig. 3.3).

**Fig. 3.1** COMET proton-therapy cyclotron at PSI. A 250 MeV, 500 nA, 4-sector isochronous AVF cyclotron. The spiral poles enhance axial focusing. A 3 m diameter superconducting coil provides the dipole field [2]

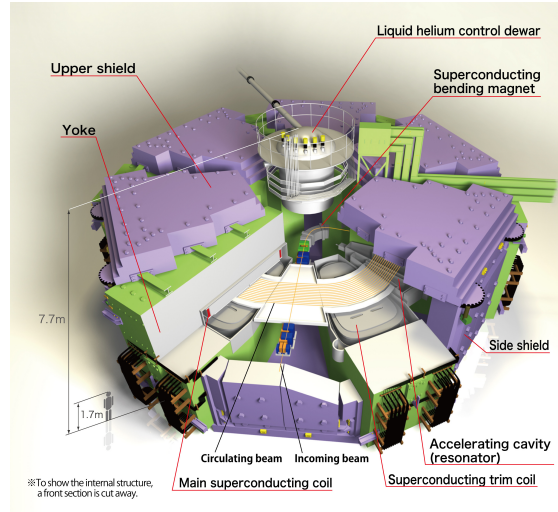


**Fig. 3.2** PSI 590 MeV ring cyclotron delivers a 1.4 MW proton beam. Acceleration takes ~180 turns; extraction efficiency is > 99.99%; overall diameter is 15 m. Beam is used for the production of secondary neutron and muon beams [3]

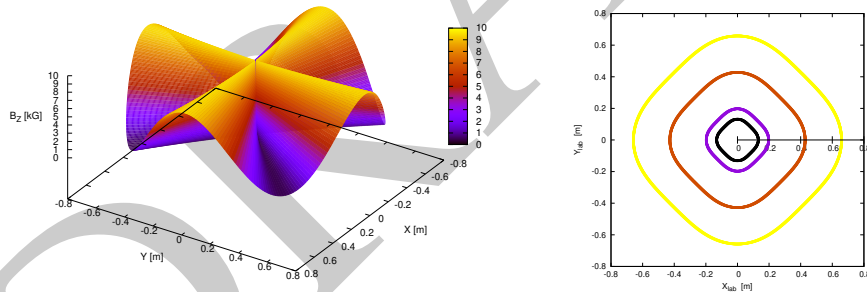


1920 At the origin of the evolution of the cyclotron technology, which led to the AVF  
1921 innovation in the late 1930s, is the energy limitation of the classical cyclotron, at a  
1922 few 10s of MeV/nucleon (Chap. 3). Axial focusing in the latter results from the slow  
1923 decrease of the guiding field with radius in the wide gap between the electromagnet

**Fig. 3.3** RIKEN K2500, superconducting coil, separated-sector, 8,300-ton ring cyclotron [4]. The dipole field is 3.8 T, rigidity 8 T m, diameter 18.4 m. Beam injection radius is 3.56 m, extraction radius is 5.36 m. The cyclotron is part of a radioactive ion beam accelerator complex [4]



1924 poles. That negative field index  $-1 < k < 0$  (Eqs. 3.11, 3.12) results in both radial and  
 1925 axial periodic stability (Eq. 3.18). Isochronism requires instead the field to increase  
 1926 with radius, *i.e.* a field index  $k > 0$ , a consequence of  $B(R) \propto \gamma(R)$  (Sect. 3.2).  
 The AVF concept by L.H. Thomas in 1938<sup>1</sup> [5] (Fig. 3.4), solved the problem:



**Fig. 3.4** A 4-periodic AVF cyclotron design (after Ref. [5]). Left: mid-plane azimuthally modulated field. Right: closed orbits around the cyclotron feature azimuthally varying curvature, greater on the hills, weaker in the field valleys

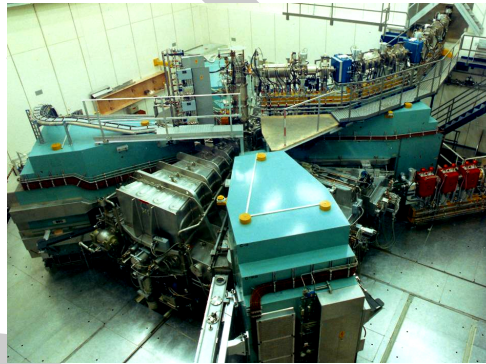
1927 AVF entails axial periodic stability as long as the field modulation parameter  $F >$   
 1928  $\beta\gamma$  (Sect. 3.2.1). The vertical defocusing effect which the radially increasing field  
 1929 causes is compensated by the focusing effect of the AVF. Spiral pole geometry was  
 1930

<sup>1</sup> The very L.H. Thomas of the Thomas-BMT spin motion differential equation, author of the eight years earlier Nature article [7].

1931 further introduced in 1954 [8] to increase axial focusing, so allowing greater  $k$  and  
 1932 isochronous acceleration to higher energy (Sect. 3.2.2). It took some time, until the  
 1933 late 1950s (see Stammach's Fig. 3.4), for Thomas' concept to make its way and lead  
 1934 up to practical realisations<sup>2</sup>. AVF cyclotrons were constructed to accelerate all sorts  
 1935 of ions whereas classical cyclotrons tended to leave the scene (Fig. 3.4). Applications  
 1936 included material science, radiobiology, production of secondary beams, and more.  
 1937 Polarized ion beams became part of the landscape as well from the moment polarized  
 1938 ion sources were made available [10].

1939 The separated sector method was developed in the early 1960s, instances are  
 1940 today's high power PSI 590 MeV spiral sector cyclotron (Fig. 3.2), brought into oper-  
 1941 ation in 1974, and its injector-II, a radial-sector design (Fig. 3.5). Iron-free regions  
 1942 between separated sector dipoles allows room for multiple high-Q RF resonators thus  
 1943 greater turn separation at extraction, for higher efficiency extraction systems and thus  
 1944 higher beam current, and for the insertion of beam instrumentation. Cyclotron en-  
 1945 ergy subsequently increased, up to the present days near-GeV range. Cryogeny was  
 1946 introduced in the early 1960s at the Michigan State University superconducting coil  
 1947 K500 cyclotron<sup>3</sup> [11]. Superconducting technology allows higher field and reduction  
 1948 of size, culminating today with RIKEN's K2500 SRC (Fig. 3.3).

**Fig. 3.5** PSI injector II, four separated radial sectors, 0.87 MeV injection energy, accelerates protons to 72 MeV in about 100 turns [6]. The drifts include the 50.7 MHz accelerating RF system and a flattop cavity. Injection is from the top, in the central region



## 1949 3.2 Basic Concepts and Formulae

1950 Mass increase with energy causes loss of synchronism in the classical cyclotron,  
 1951 and the required negative field index (decreasing guiding field with radius) for

<sup>2</sup> One can read for instance, in 1959's Ref.[9], Cyclotrons and Synchrocyclotrons, regarding engineering aspects, "Also, no consideration is given to the AVF cyclotron, since none of this type has reached the advanced design stage".

<sup>3</sup>  $K = E A / Z^2$ , with  $A$  the number of mass,  $Z$  the number of charge, is a measure of the equivalent proton energy, 500 MeV in this case.

**Table 3.1** A comparison between an AVF and a separated sector cyclotron of same energy, 72 MeV, namely, the former AVF injector and the present Injector II of PSI high power cyclotron, after Ref. [10, p. 126])

		AVF	separated sector
Injection energy	keV	14	870
Extraction energy	MeV	72	72
Beam current	mA	0.2	1.6
Magnet		single dipole	4 sectors
Weight	ton	470	4 × 180
Dipole gap height	mm	240 to 450	35
$\langle B \rangle$ ; $B_{\max}$	T	1.6; 2	0.36; 1.1
RF system		180° dees	2 resonators
Accelerating voltage	kV	2 × 70	4 × 250
RF	MHz	50	50
Normalized beam emittance, hor.; vert.	$\pi\mu\text{m}$	2.4; 1.2	1.2; 1.2
Beam phase width	deg	16 - 40	12
Energy spread	%	0.3	0.2
Turn separation at extraction	mm	3	18

1952 axial periodic motion stability adds to the effect. Isochronism instead, *i.e.*, constant  
 1953  $\omega_{\text{rev}} = qB/\gamma m_0$ , given orbit radius  $R = \beta c/\omega_{\text{rev}}$ , leads to positive index

$$k = \frac{R}{B} \frac{\partial B}{\partial R} = \frac{\beta}{\gamma} \frac{\partial \gamma}{\partial \beta} = \beta^2 \gamma^2 \quad (3.34)$$

1954 requiring  $k$  to follow the energy increase: the weak focusing condition  $-1 < k < 0$   
 1955 can not be satisfied, transverse periodic stability is lost.

1956 Isochronism requires the revolution period  $T_{\text{rev}} = 2\pi\gamma m_0/qB$  to be momentum  
 1957 independent; under this condition, differentiating this expression yields the radial  
 1958 field dependence

$$B(R) = \frac{B_0}{\gamma_0} \gamma(R) \quad (3.35)$$

1959 with  $B_0$  and  $\gamma_0$  some reference conditions,

1960 This led H.A. Bethe and M.E. Rose to conclude, in 1938, “... *it seems useless*  
 1961 *to build cyclotrons of larger proportions than the existing ones... an accelerating*  
 1962 *chamber of 37 cm radius will suffice to produce deuterons of 11 MeV energy which*  
 1963 *is the highest possible...*” [12]. And F.T. Cole to comment, “*If you went to graduate*  
 1964 *school in the 1940’s, this inequality  $[-1 < r(dB/dr)/B < 0]$  was the end of the*  
 1965 *discussion of accelerator theory.*” [13, Sect. 1.4].

### 1966 3.2.1 Thomas Focusing

1967 Whereas the classical cyclotron approach assumed revolution symmetry of the field,  
 1968 a 1938 publication stated: “[...] *a variation of the magnetic field with angle, [...] of*

1969 order of magnitude  $v/c$ ; together with nearly the radial increase of relative amount  
 1970  $\frac{1}{2}v^2/c^2$  of Bethe and Rose; gives stable orbits that are in resonance and not defo-  
 1971 cused.” [5]. In other words, AVF in proper amount (Fig. 3.4) compensates the axial  
 1972 defocusing resulting from the increase of the field with radius (Eq. 3.35). Azimuthal  
 1973 field modulation and radial increase may be obtained by shaping the magnet poles,  
 as illustrated in Fig. 3.6.

**Fig. 3.6** Pole shaping in an AVF cyclotron, an electron model, here [14]. The focusing pattern is FfFfFf, an alternation of strong (hill regions) and weak (valleys) radial focusing [15]



1974

1975 *Azimuthal field modulation, flutter*

1976 A simple approach to the  $2\pi/N$ -periodic axial symmetry and field modulation may  
 1977 assume a sinusoidal azimuthal form factor

$$\mathcal{F}(\theta) = 1 + f \sin(N\theta) \quad (3.36)$$

1978 This is the case in Fig. 3.4, for instance. The mid-plane field can thus be expressed  
 1979 under the form

$$B(R, \theta) = B_0 \mathcal{R}(R) \mathcal{F}(\theta) \quad (3.37)$$

1980 with  $\mathcal{R}(R)$  the radial dependence. The orbit curvature varies along the  $\frac{2\pi}{N}$ -periodic  
 1981 orbit, this requires distinguishing between the local focusing index  $n = \frac{\rho(s)}{B(s)} \frac{dB}{d\rho}$  and  
 1982 the geometrical index  $k$  (Eq. 3.34), a global quantity which determines the wave  
 1983 numbers (Eq. 3.39). A “flutter” factor can be introduced to quantify the effect of the  
 1984 azimuthal modulation of the field on the focusing,

$$F = \left( \frac{\langle (\mathcal{F} - \langle \mathcal{F} \rangle)^2 \rangle}{\langle \mathcal{F} \rangle^2} \right)^{1/2} \xrightarrow{\text{hard edge}} \left( \frac{R}{\rho} - 1 \right)^{1/2} \quad (3.38)$$

1985 where  $\langle * \rangle = \oint (*) d\theta / 2\pi$ . If the scalloping of the orbit (*i.e.*, its excursion in the  
 1986 vicinity of  $R$ ) is of small amplitude, then  $R \approx \rho$  and, accounting for the isochronism  
 1987 condition (Eq. 3.34), approximate values of the wave numbers write

$$v_R \approx \sqrt{1+k} \stackrel{\text{isochr.}}{=} \gamma, \quad v_y \approx \sqrt{-k+F^2} \stackrel{\text{isochr.}}{=} \sqrt{-\beta^2\gamma^2+F^2} \quad (3.39)$$

1988 Thus the horizontal wave number increases during acceleration, linearly with energy,  
 1989 whereas in the absence of countermeasure the axial wave number would decrease  
 1990 - see Sect. 3.2.2. An additional property is

$$v_R^2 + v_y^2 = 1 + F^2 \xrightarrow{\text{hard edge}} \frac{R}{\rho} \quad (3.40)$$

1991 The flutter allows designing  $-k + F^2 > 0$  (whereas  $k > 0$ ), so ensuring peri-  
 1992 odic stability of the axial motion. In the hypothesis of a sinusoidal azimuthal field  
 1993 modulation (Eq. 3.36) one has  $F = f/\sqrt{2}$  and

$$v_y \approx \sqrt{-k + f^2/2}, \quad v_R^2 + v_y^2 = 1 + f^2/2 \quad (3.41)$$

#### 1994 *Off-Momentum Orbit*

1995 The dispersion function  $D = \delta x / \delta p / p$  in the revolution symmetry field is (Eq. 3.20)  
 1996 has the form  $D = \frac{R_0}{1+k}$ . Given the isochronous condition  $k = \beta^2\gamma^2$  it can be written

$$D = \frac{R}{\gamma^2} \quad (3.42)$$

1997 An alternate approach consists in considering that, with the isochronism condition  
 1998  $2\pi R/\beta c = T_{\text{rev}}$ , a constant, one gets  $\frac{dR}{R} = \frac{d\beta}{\beta} = \frac{1}{\gamma^2}$ .

#### 1999 *AVF Modeling*

2000 A numerical approach to the azimuthal modulation beyond the simple sine modula-  
 2001 tion of Eq. 3.36, is discussed in Sect. 13.3.3 (Eqs. 13.12, 13.16). It provides a model-  
 2002 ing of  $\mathcal{F}(\theta)$  over the whole beam excursion area, possibly including an R-dependence,  
 2003  $\mathcal{F}(R, \theta)$ . The method ensures the continuity of  $\mathcal{F}(R, \theta)$  and its derivatives, between  
 2004 neighboring magnetic sectors. It is resorted to in the simulation exercises.

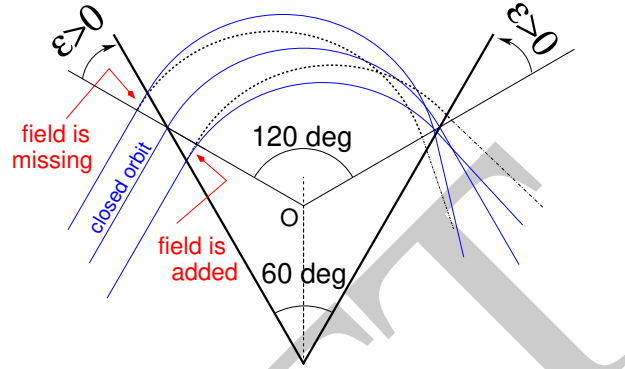
#### 2005 *Wedge Focusing*

2006 In the entrance and exit regions of a bending sector, closed orbits are at an angle  
 2007 to the iso-field lines, this causes “wedge focusing”, an effect sketched in Fig. 3.7:  
 2008 with positive wedge angle  $\varepsilon$ , case of the AVF configuration, radial focusing de-



2009 creases whereas the angle of off mid-plane particle velocity vector to the azimuthal  
2010 component of the field in the wedge region causes axial focusing.

**Fig. 3.7** A 120 deg bending of the closed orbit (curvature center at O) is ensured by a 60 deg bending sector. This results in a wedge angle ( $\varepsilon > 0$  by convention in this configuration) in the transition regions between valleys and hills, which causes a decrease of the radial focusing (solid incoming trajectories, compared to dotted ones), and axial focusing under the effect of the trajectory angle to the azimuthal field component



### 2011 3.2.2 Spiral Sector

2012 Spiral sector geometry was introduced in 1954 in the context of fixed field alternating  
2013 gradient accelerator (FFAG) studies [8], and found application in cyclotrons (as in  
2014 PSI's COMET cyclotron, Fig. 3.1). Spiraling the edges (Fig. 3.8) results in stronger  
2015 axial focusing (Eq. 3.45) compared to a radial sector (Eq. 3.39), it also permits an  
2016 increase of the wedge angle with radius, so maintaining proper compensation of an  
2017 increase of  $k(R)$  (Eq. 3.34). In a spiral sector bend the wedge angle is positive on one  
2018 side of the sector, negative on the other side (Fig. 3.8), with a global axial focusing  
2019 resultant. In a similar approach to the periodic field modulation in a radial sector  
2020 (Eq. 3.36), a convenient approach to the spiral sector AVF uses azimuthal form factor

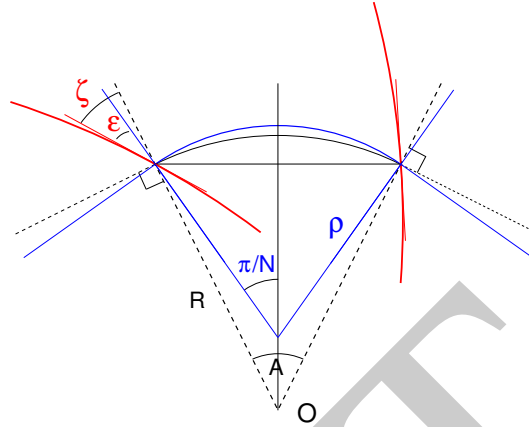
$$\mathcal{F}(R, \theta) = 1 + f \sin \left[ N \left( \theta - \tan(\zeta(R)) \ln \frac{R}{R_0} \right) \right] \quad (3.43)$$

2021 with the spiral angle  $\zeta(R)$  an increasing function of radius  $R$ , whereas the mid-plane  
2022 field now writes under the form

$$B(R, \theta) = B_0 \mathcal{R}(R) \mathcal{F}(R, \theta) \quad (3.44)$$

2023 The local magnet edge geometry at  $R$  satisfies  $r = r_0 \exp(\theta/\tan(\zeta))$ , a logarithmic  
2024 spiral centered at the center of the ring, with  $\zeta$  the angle between the tangent to the  
2025 spiral edge and the ring radius (Fig. 3.8). This results in a larger contribution of the  
2026 flutter term in the axial wave number,

**Fig. 3.8** Geometrical parameters of a spiral sector dipole. The center of the ring is at  $O$ ,  $\zeta$  is the spiral angle (increasing with radius),  $\varepsilon$  is the wedge angle. In the hard edge field model, a line of constant field inside the sector is an arc of radius  $R$ ; thus the curvature radius  $\rho$  varies along the closed orbit in the dipole



$$v_y \approx \sqrt{-k + F^2(1 + 2 \tan^2 \zeta)} \quad (3.45)$$

2027 As the field index  $k$  increases with  $R$  to ensure isochronism (Eq. 3.34), the spiral  
2028 angle follows so to maintain  $-k + F^2(1 + 2 \tan^2 \zeta) > 0$ . A limitation here is the  
2029 maximum spiral angle achievable, obviously  $\zeta \rightarrow 90$  deg.

2030 As an illustration, in TRIUMF cyclotron  $\zeta$  reaches 72 deg in the 500 MeV region  
2031 (from zero in the 100 MeV region) whereas  $1 + 2 \tan^2 \zeta$  increases to 20 (from 1 in  
2032 the 100 MeV region) and compensates a low  $F < 0.07$  (down from  $F = 0.3$ ). In PSI  
2033 590 MeV cyclotron  $\zeta$  reaches  $35^\circ$  on the outer radius. Most isochronous cyclotrons  
2034 of a few tens of MeV use spiral sectors to benefit from the more efficient axial  
2035 focusing [15].

2036 More can be found in the scaling FFAG chapter (Sect. 9.2.2) regarding the spiral  
2037 sector, and regarding its numerical simulation.

### 2038 3.2.3 Isochronism

2039 In the hypothesis of isochronism, the revolution angular frequency satisfies  $\omega_{\text{rev}} =$   
2040  $c\beta(\gamma)/R(\gamma) = \text{constant}$ . An orbital radius  $R_\infty = c/\omega_{\text{rev}}$  is reached asymptotically as  
2041  $\beta = v/c = R/R_\infty \rightarrow 1$ . In terms of the RF and harmonic number,

$$R_\infty = h \frac{c}{\omega_{\text{rf}}} \quad (3.46)$$

2042 Given  $BR_\infty = \gamma m_0 c/q$  and using  $\gamma = (1 - (R/R_\infty)^2)^{-1/2}$ , the radial dependence of  
2043 the field can be expressed in terms of  $R_\infty$ , namely,

$$B_0 \mathcal{R}(R) = \gamma B_0 = \frac{B_0}{\sqrt{1 - (R/R_\infty)^2}} \quad \text{with } B_0 = \frac{m_0 \omega_{\text{rev}}}{q} = \frac{m_0}{q} \frac{\omega_{\text{rf}}}{h} \quad (3.47)$$

2044 and goes to infinity with  $R \rightarrow R_\infty$ . For protons for instance, with  $m_0/q = 1.6726 \times$   
 2045  $10^{-27}[\text{kg}] / 1.6021 \times 10^{-19}[\text{C}] \approx 10^{-8}$ ,  $BR_\infty[\text{T m}] = \gamma m_0 c / q \approx 3\gamma$ . A typical value  
 2046 for  $R_\infty$  can be obtained assuming for instance an upper  $\gamma = 1.64$  (600 MeV) in a  
 2047 region of upper field value  $B = 1.64$  T, yielding  $R_\infty \approx 3$  m.

### 2048 *Radial field*

2049 From Eq. 3.47 it results that the radial field form factor of Eqs. 3.37, 3.44 can be  
 2050 written

$$\mathcal{R}(R) = \left( 1 - \left( \frac{R}{R_\infty} \right)^2 \right)^{-1/2} \quad (3.48)$$

2051 A possible approach consists in using the Taylor expansion of  $\mathcal{R}(R)$  (within the limits  
 2052 of radius of convergence of that series), namely

$$\mathcal{R}(R) = 1 + \frac{1}{2} \left( \frac{R}{R_\infty} \right)^2 + \frac{3}{8} \left( \frac{R}{R_\infty} \right)^4 + \frac{5}{16} \left( \frac{R}{R_\infty} \right)^6 + \dots \quad (3.49)$$

2053 The coefficients in this polynomial in  $R/R_\infty$  are the field index and its derivatives,  
 2054 they can be a starting point for further refinement of the isochronism, including for  
 2055 instance side effects of the azimuthal field form factor  $\mathcal{F}(R, \theta)$  (Eqs. 3.36, 3.43).

2056 The radial field index  $k(R)$  in the AVF cyclotron is designed to satisfy the condition  
 2057 of isochronism (Eq. 3.34). However, reducing the RF phase slip over the acceleration  
 2058 cycle substantially below  $\pm\pi/2$  requires a tolerance below  $10^{-5}$  on field value over  
 2059 the orbit excursion area. This tight constraint requires pole machining, shimming,  
 2060 and other correction coil strategies in order to satisfy Eq. 3.34.

### 2061 *Fast Acceleration*

2062 Fixed field and fixed RF allow fast acceleration, the main limitation is in the amount  
 2063 of voltage which can be implemented around the ring. The voltage per turn reaches  
 2064 4 MV for instance at the PSI 590 MeV ring cyclotron, where bunches are accelerated  
 2065 from 72 MeV to 590 MeV in less than 200 turns.

2066 Harmful resonances may have to be crossed as wave numbers vary during accel-  
 2067 eration, including the ‘‘Walkinshaw resonance’’  $\nu_R = 2\nu_y$ , as  $\nu_R \approx \gamma$  whereas the  
 2068 axial wave number spans  $\nu_y \approx 1^- \sim 1.5$ . This coupling resonance may result in an  
 2069 increase of vertical beam size and subsequent particle losses, fast crossing mitigates  
 2070 the effect.

2071 Fast acceleration improves extraction efficiency, as the turn separation  $dR/dn$  is  
 2072 proportional to the energy gain per turn (Sect. 3.2.4).

## 2073 **3.2.4 Cyclotron Extraction**

2074 The minimum radial distance between the last two turns, where the extraction septum  
 2075 is located, is imposed by beam loss tolerances, which in some cases (high power  
 2076 beams for instance) may be tight, in the  $10^{-4}$  range or less. Space charge in particular  
 2077 matters, as it increases the energy spread, and thus the radial extent of a bunch. In  
 2078 the relativistic cyclotron the separation between two consecutive turns satisfies

$$\Delta R \approx \frac{\gamma}{\gamma + 1} \frac{\Delta E}{E} \frac{R}{v_R^2} \quad (3.50)$$

2079 with  $\Delta E$  the effective acceleration rate per turn. This indicates that greater turn  
 2080 separation at extraction results from increased ring size. As a matter of fact, size is a  
 2081 limitation to intensity in small cyclotrons. It also indicates that extraction efficiency  
 2082 may be increased by moving the radial wave number closer to  $\nu_R = 1$ .

### 2083 3.2.5 Resonant Spin Motion

2084 In the quasi-uniform, quasi vertical field  $\mathbf{B} \approx \mathbf{B}_y$  of a classical cyclotron dipole, spins  
 2085 quietly perform  $G\gamma$  precessions around a vector  $\omega_{\text{sp}} \parallel \mathbf{B}$  (Eq. 3.30) as the particle  
 2086 velocity completes a  $2\pi$  precession around the ring (Sect. 3.2.5) [16].

2087 More is liable to happen in the AVF cyclotron, due to the strong radial field index  
 2088 (Eq. 3.34) and to the azimuthal field modulation (Eqs. 3.36, 3.43): the azimuthal and  
 2089 radial field components  $B_\theta$  and  $B_R$  are non-zero out of the median plane,  $\mathbf{B}(R, \theta, y)$   
 2090 may locally depart from vertical in a substantial manner, and so will the local pre-  
 2091 cession vector  $\omega_{\text{sp}}(R, \theta, y)$ . The latter varies periodically in addition, as the particle  
 2092 undergoes periodic vertical motion about the median plane. Resonance between spin  
 2093 precession (characterized by spin tune  $\nu_{\text{sp}} = G\gamma$ , Eq. 3.33) and periodic perturbing  
 2094 field components (characterized by the axial wave number  $\nu_y$ , Eqs. 3.39, 3.45) occurs  
 2095 if the two motions feature coinciding frequencies. This condition can be expressed  
 2096 under the form

$$\nu_{\text{sp}} \pm \nu_y = \text{integer} \quad \text{or, equivalently} \quad G\gamma = \text{integer} \pm \nu_y \quad (3.51)$$

2097 The spin precession axis  $\omega_{\text{sp}}$  moves away from the vertical as the spin motion gets  
 2098 closer to resonance (during acceleration as  $G\gamma$  varies for instance), to end up in the  
 2099 median plane on the resonance [17, Sect. 3.6].

2100 Consider now an ion bunch, away from any depolarizing resonance. Its polariza-  
 2101 tion is  $\langle S_y \rangle$ , the average of the projection of the spins on the vertical. If a depolarizing  
 2102 resonance is crossed during acceleration, the initial polarization (far upstream of the  
 2103 resonance; index i) and final polarization (far downstream of the resonance; index f)  
 2104 satisfy the Froissart-Stora law [18],

$$\frac{\langle S_y \rangle_f}{\langle S_y \rangle_i} = 2e^{-\frac{\pi}{2} \frac{|\epsilon_R|^2}{a}} - 1 \quad (3.52)$$

2105 where  $|\epsilon_R|$  is the strength of the resonance: a measure of the strength of the depolar-  
 2106 izing fields, its calculation is addressed in a next chapter;  $a$  is the resonance crossing  
 2107 speed,

$$a = G \frac{d\gamma}{d\theta} \pm \frac{dv_y}{d\theta} \quad (3.53)$$

2108 The Froissart-Stora formula indicates that, if the resonance is crossed slowly ( $a \rightarrow 0$ ),  
 2109  $\langle S_y \rangle_f / \langle S_y \rangle_i \rightarrow -1$ : spins quietly follow the flipping motion of the precession axis,  
 2110 polarization is flipped and preserved. If the crossing is fast ( $a \rightarrow \infty$ ),  $\langle S_y \rangle_f / \langle S_y \rangle_i \rightarrow$   
 2111 0, polarization is unaffected. Intermediate crossing speeds cause polarization loss:  
 2112  $|\langle S_y \rangle|$  ends up smaller after the resonance.

### 2113 3.3 Exercises

2114 Exercises 3.14 to 3.16 use a field map, designed in exercise 3.13, to simulate an AVF  
 2115 cyclotron dipole. Note that they can be performed using DIPOLE[S] analytical field  
 2116 model instead, as in exercise 3.17 (a similar simulation which can be referred to  
 2117 is exercise 3.2, Classical Cyclotron Chapter). As a reminder, regarding the interest  
 2118 of one or the other of the two methods: field maps allow close to real field models  
 2119 (a measured field map for instance, or from a magnet computer code); using an  
 2120 analytical field model allows more flexibility regarding magnet parameters, which  
 2121 can for instance be optimized using a matching procedure.

2122 Note: some of the input data files for these simulations are available in zgoubi  
 2123 sourceforge repository at

2124 `[pathTo]/branches/exemples/book/zgoubiMaterial/cyclotron_relativistic/`

#### 2125 3.13 Modeling Thomas AVF Cyclotron

2126 Solution: page 367.

2127 In this exercise a 2D mid-plane field map is built, inspired from Thomas's 1938 ar-  
 2128 ticle [5]. The method to build the map is that of Exercise 3.1, TOSCA[MOD.MOD1=22.1]  
 2129 keyword is used to raytrace through and derive the optical parameters of the 4-period  
 2130 AVF cyclotron.

2131 (a) Construct a  $360^\circ$  2D map of the median plane field  $B_Z(R, \theta)$ , simulating the  
 2132 field in the 4-period Thomas cyclotron of Fig. 3.4, assuming the following:

2133 -  $B_Z(R, \theta) = B_0[1 + f \sin(4(\theta - \theta_i))]$  (Eq. 3.36), with  $\theta_i$  some arbitrary ori-  
 2134 gin of the azimuthal angle, to be determined. Hint: depending on  $\theta_i$  value, the  
 2135 closed orbit may be at an angle to the polar radius, as seen in Fig. 3.4; in that case  
 2136 TOSCA[MOD.MOD1=22.1] would require non-zero in and out positioning angles  
 2137 TE and TS, to be determined and stated using KPOS option [19]; instead, a proper  
 2138 choice of  $\theta_i$  value allows a simpler TE=TS=0;

2139 - an average axial field  $B_0 = 0.5$  T on the 200 keV radius (the latter,  $R_0(B_0)$ , is to  
 2140 be determined),  $B_Z > 0$  and  $0 < f < 1$  modulation.

2141 - an arbitrary field index  $k$  - a good idea is to start building and testing the AVF  
2142 in the case  $k = 0$ ;

2143 - a uniform map mesh in a polar coordinate system  $(R, \theta)$  as sketched in Fig. 3.17,  
2144 covering  $R=1$  to 100 cm; take a radial increment of the mesh  $\Delta R = 0.5$  cm, azimuthal  
2145 increment  $\Delta\theta = 0.5$  cm/ $R_M$ , with  $R_M$  some reference radius, say  $R_M = 50$  cm, half  
2146 way between map boundaries;

2147 - an appropriate 6-column formatting of the field map data for TOSCA to read,  
2148 as follows:

2149  $R \cos \theta, Z, R \sin \theta, BY, BZ, BX$

2150 with  $\theta$  varying first,  $R$  varying second in that list.  $Z$  is the vertical direction (normal  
2151 to the map mesh), so  $Z \equiv 0$  in this 2D mesh.

2152 Provide a graph of  $B_Z(R, \theta)$  over the extent of the field map.

2153 (b) Raytrace a few concentric closed trajectories centered on the center of the  
2154 dipole, ranging in  $10 \leq R \leq 80$  cm. Provide a graph of these concentric trajectories  
2155 in the  $(O; X, Y)$  laboratory frame, and a graph of the field along trajectories. Initial  
2156 coordinates can be defined using OBJET, particle coordinates along trajectories  
2157 during the stepwise raytracing can be logged in zgoubi.plt by setting IL=2 under  
2158 TOSCA.

2159 (c) Check the effect of the integration step size on the accuracy of the trajectory  
2160 and time-of-flight computation, by considering some  $\Delta s$  values in  $[0.1, 10]$  cm, and  
2161 energies in a range from 200 keV to a few tens of MeV (considering protons).

2162 (d) Produce a graph of the energy or radius dependence of wave numbers.

2163 (e) Calculate the numerical value of the axial wave number,  $\nu_y$ , from the flutter  
2164 (Eqs. 3.38, 3.39). Comparing with the numerical values, discrepancy is found: repeat  
2165 (d) for  $f=0.1, 0.2, 0.3, 0.6$ , check the evolution of this discrepancy.

### 2166 3.14 Designing an Isochronous AVF Cyclotron

2167 Solution: page 375.

2168 (a) Introduce a radius dependent field index  $k(R)$  in the AVF cyclotron designed  
2169 in exercise 3.13, proper to ensure  $R$ -independent revolution period, in three different  
2170 cases of modulation:  $f=0$  (no modulation),  $f=0.2$  and  $f=0.9$ .

2171 Check this property by computing the revolution period  $T_{\text{rev}}$  as a function of  
2172 kinetic energy  $E_k$ , or radius  $R$ . On a common graph, display both  $T_{\text{rev}}$  and  $dT_{\text{rev}}/T_{\text{rev}}$   
2173 as a function of radius, including for comparison a fourth case:  $B=\text{constant}=5$  kG.

2174 (b) Provide a graph of the energy dependence of wave numbers.

### 2175 3.15 Acceleration to 200 MeV in an AVF Cyclotron

2176 Solution: page 380.

2177 In this exercise protons are accelerated to over 100 MeV in an AVF cyclotron:  
2178 well beyond the about 20 MeV energy reached in the classical cyclotron (see exer-  
2179 cise 3.10).

2180 (a) Produce an acceleration cycle of a proton, from 0.2 to 100 MeV, in the AVF  
2181 cyclotron designed in exercise 3.14. Note that a dedicated field map has to be created  
2182 in order to allow for the higher maximum energy - a 3 meter field map outer radius  
2183 works. Assume proper modulation coefficient  $f$  for axial focusing all the way to

2184 300 MeV. Assume a double-dee design, and 400 keV peak voltage in the gap, use  
 2185 CAVITE[IOPT=7] for acceleration to account for RF phase.

2186 (b) Give a graph of the energy dependence of wave numbers over the acceleration  
 2187 range.

### 2188 3.16 Thomas-BMT Spin Precession in Thomas Cyclotron

2189 Solution: page 384.

2190 This exercise uses the field maps and input data file of exercise 3.15. Dependence  
 2191 of energy boost on RF phase is removed by using CAVITE[IOPT=3] [19]. Consider  
 2192 helion ions: use PARTICUL[Name=HELION] to define mass, charge and G fac-  
 2193 tor, all quantities needed for the integration of Thomas-BMT differential equation  
 2194 (Eq. 3.30).

2195 (a) By scanning the axial wave number, find the  $G\gamma$  value for which the spin  
 2196 motion resonance condition (Eq. 3.51) is satisfied.

2197 (b) Consider a particle with non-zero axial motion, so that it experiences hori-  
 2198 zontal magnetic field components as it circles around. Track its spin through the  
 2199 resonance, take initial spin vertical  $\mathbf{S} \equiv \mathbf{S}_Z$ . Provide a graph of  $S_Z$  as a function of  
 2200  $G\gamma$  or energy.

2201 (c) Simulate resonance crossing for a series of different vertical motion amplitudes  
 2202  $Z_0$ ; produce a graph of these resonance crossings  $S_Z(\text{turn})$ .

2203 Plot the ratio  $S_{y,f}/S_{y,i}(Z_0)$ . From a match of this  $S_{y,f}/S_{y,i}$  series with Eq. 3.52,  
 2204 show that the resonance strength changes in proportion to the vertical excursion.

2205 (d) Repeat (c) for a series of different resonance crossing speeds instead (Eq. 3.53),  
 2206 leaving  $Z_0$  unchanged.

2207 Show that this  $S_{y,f}/S_{y,i}$  series can be matched with Eq. 3.52.

### 2208 3.17 Isochronism and Edge Focusing in a Separated Sector Cyclotron

2209 Solution: page 387.

2210 This exercise uses DIPOLE to simulate a 30 deg sector dipole of a 4-period cy-  
 2211 clotron, and allow playing with field fall-off extent at dipole EFBs. The configuration  
 2212 of the cyclotron is typically that of PSI 72 MeV injector (Fig. 3.5). DIPOLE allows  
 2213 radial field indices up to the third order ( $\partial^3 B_Z / \partial R^3$ ) [19, Eq. 6.3.18]. In question (b)  
 2214 however, higher order indices are needed to improve the isochronism, requiring the  
 2215 use of DIPOLES [19, Eqs. 6.3.20, 21].

2216 Take fringe fields into account (see Sect. 13.3.3), with

2217 -  $\lambda = 7$  cm the fringe extent (changing  $\lambda$  changes the flutter, Eq. 3.38),

2218 -  $C_0 = 0.1455$ ,  $C_1 = 2.2670$ ,  $C_2 = -0.6395$ ,  $C_3 = 1.1558$  and  $C_4 = C_5 = 0$ , for a  
 2219 realistic field fall-off model.

2220 (a) Assume  $k = 0$ , here. Produce a model of a period using DIPOLE.

2221 Produce a graph of closed orbits across a period for a few different rigidities (FIT  
 2222 can be used to find them), and a graph of the field along these orbits.

2223 (b) In this question, R-dependence of the mid-plane magnetic field proper to  
 2224 ensuring energy independent revolution period is introduced. Use DIPOLES here,  
 2225 as it allows  $b_i$  field indices to higher order, as necessary to reach tight isochronism  
 2226 over the full energy range.

2227 Assume a peak field value  $B_0 = 1.1$  T at a radius of 3.5 m in the dipoles. Find the  
 2228 average orbit radius  $R$ , and average field  $B$  (such that  $BR = p/q$ ), at an energy of  
 2229 72 MeV.

2230 Determine a series of index values,  $b_{i=1,n}$ , in the model [19, Eq. 6.3.19]

$$B_Z(R, \theta) = B_0 \mathcal{F}(R, \theta) \left( 1 + b_1 \frac{R - R_0}{R_0} + b_2 \left( \frac{R - R_0}{R_0} \right)^2 + \dots \right) \quad (3.54)$$

2231 proper to bring the revolution period closest to  $R$ -independent, in the energy range  
 2232 0.9 to 72 MeV (hint: use a Taylor development of Eq. 3.48 and identify with the  
 2233  $R$ -dependent factors in Eq. 3.54).

2234 (c) Play with the value of  $\lambda$ , concurrently to maintaining isochronism with  
 2235 appropriate  $b_i$  values. Check the evolution of radial and axial focusing - OB-  
 2236 JET[KOBJ=5] and MATRIX[IORD=1,IFOC=11] or TWISS, or OBJET[KOBJ=6]  
 2237 and MATRIX[IORD=2,IFOC=11], can be used to get the wave numbers.

2238 From raytracing trials, observe that (i) the effect of  $\lambda$  on radial focusing is weak  
 2239 (a second order effect in the particle coordinates); (ii) greater (smaller)  $\lambda$  value  
 2240 results in smaller (greater) flutter and weaker (stronger) axial focusing (a first order  
 2241 effect). Note: the integration step size in DIPOLE[S] has to be consistent with the  
 2242 field fall-off extent ( $\lambda$  value), in order to ensure that the numerical integration is  
 2243 converged.

2244 (d) For some reasonable value of  $\lambda$  (normally, about the height of a magnet  
 2245 gap, say, a few centimeters), compute  $F^2 = \frac{\langle (B(\theta) - \langle B \rangle)^2 \rangle}{\langle B \rangle^2}$ . Check the validity of  
 2246  $v_y = \sqrt{-\beta^2 \gamma^2 + F^2}$  (Eq. 3.39). OBJET[KOBJ=5] and MATRIX[IORD=1,IFOC=11]  
 2247 can be used to compute  $v_y$ , or multturn raytracing and a Fourier analysis.

2248 (e) Check the rule  $F^2 \xrightarrow{\text{hard edge}} \frac{R}{\rho} - 1$  (Eq. 3.38), from the field  $B(\theta)$  delivered by  
 2249 DIPOLES. Give a theoretical demonstration of that rule.

### 2250 3.18 A Model of PSI Ring Cyclotron Using CYCLOTRON

2251 Solution: page 390.

2252 The simulation input data file in Tab. 3.2 is based on the use of CYCLOTRON, to  
 2253 simulate a period of the eight-sector PSI ring cyclotron and work on the isochronism.  
 2254 That file is the starting point of the present exercise.

2255 (a) With zgoubi users' guide at hand, explain the signification of the data in that  
 2256 simulation input data file.

2257 (b) Compute and plot a few trajectories and field along, across the sector. Provide  
 2258 a graph of field density over the sector.

2259 (c) Compute and plot the radius dependence of the revolution period.

2260 (d) The field indices  $b_1, b_2, \dots$  are aimed at realizing the isochronism; four,  $b_1 - b_4$   
 2261 are accounted for in (a) and (b), they were drawn from the PSI cyclotron spiral sector  
 2262 magnet field map data. Question (c) proves this small set of indices to result in a  
 2263 poor isochronism of the orbits.



**Table 3.2** Simulation input data file: a period of an eight-sector PSI-style cyclotron. The data file is set up for a scan of the periodic orbits, from radius  $R=204.1171097$  cm to  $R=383.7131468$  cm, in 15 steps

```

PSI CYCLOTRON

'OBJET'
1249.382414
2
1 1
204.1171097 8.915858372 0. 0. 0. 1. 'o'
1
'PARTICUL'
PROTON

'CYCLOTRON'
2
1 45.0 276. 1.0
0. 0. 0.99212277 51.4590015 0.5 800. -0.476376328 2.27602517e-03 -4.8195589e-06 3.94715806e-09
18.3000E+00 1. 28. -2.0
8 1.1024358 3.1291507 -3.14287154 3.0858059 -1.43545 0.24047436 0. 0. 0.
11.0 3.5 35.E-3 0.E-4 3.E-8 0. 0. 0.
18.3000E+00 1. 28. -2.0
8 0.70490173 4.1601305 -4.3309575 3.540416 -1.3472703 0.18261076 0. 0. 0.
-8.5 2. 12.E-3 75.E-6 0. 0. 0. 0.
0. -1
0 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0.
2 10.
0.4
2 0. 0. 0.

'FIT2'
2
1 31 0 [-300.,100]
1 35 0 [.1,3.]
2
3.1 1 2 #End 0. 1. 0
3.1 1 3 #End 0. 1. 0
'FAISCEAU'

'FAISTORE'
orbits.fai
1

'REBELOTE'
14 0.2 0 1
OBJET 30 221.065356:383.7131468

'SYSTEM'
1
gnuplot <./gnuplot_orbits.gnu
'END'

```

2264 Add higher order indices, until a sufficient number, with proper values, is found  
 2265 that allows FIT to reach a final isochronism improved by an order of magnitude.  
 2266 Provide a revised input data file with updated index series and their values.

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2283 Figure 3.3: the picture, and the permission to use it in this publication, have been granted by  
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