Transverse (Betatron) Motion

Linear betatron motion

Dispersion function of off momentum particle Simple Lattice design considerations Nonlinearities

What we learned:

Floquet Theorem

$$X'' + K(s)X = 0$$

$$X'' + K(s)X = 0 K(s) = K(s+L)$$

$$X(s) = aw(s)e^{j\psi(s)},$$

$$X(s) = aw(s)e^{j\psi(s)}, \quad w(s) = w(s+L), \quad \psi(s+L) - \psi(s) = 2\pi\mu$$

$$\beta(s) = w^2, \quad \alpha = -\frac{1}{2}\beta', \quad \gamma = \frac{1+\alpha^2}{\beta}, \qquad w(s) = \sqrt{\beta(s)}, \quad \psi(s) = \int_s^s \frac{1}{\beta} ds$$

$$w(s) = \sqrt{\beta(s)}, \quad \psi(s) = \int_{s_0}^{s} \frac{1}{\beta} ds$$

$$\begin{pmatrix} X(s_2) \\ X'(s_2) \end{pmatrix} = M(s_2, s_1) \begin{pmatrix} X(s_1) \\ X'(s_1) \end{pmatrix}$$

$$\begin{pmatrix}
X(s_2) \\
X'(s_2)
\end{pmatrix} = M(s_2, s_1) \begin{pmatrix}
X(s_1) \\
X'(s_1)
\end{pmatrix}$$

$$M(s_2, s_1) = \begin{pmatrix}
\sqrt{\frac{\beta_2}{\beta_1}} (\cos \mu + \alpha_1 \sin \mu) & \sqrt{\beta_1 \beta_2} \sin \mu \\
-\frac{1 + \alpha_1 \alpha_2}{\sqrt{\beta_1 \beta_2}} \sin \mu - \frac{\alpha_1 - \alpha_2}{\sqrt{\beta_1 \beta_2}} \cos \mu & \sqrt{\frac{\beta_2}{\beta_1}} (\cos \mu - \alpha_1 \sin \mu)
\end{pmatrix}$$

$$= \begin{pmatrix} \sqrt{\beta_2} & 0 \\ -\frac{\alpha_2}{\sqrt{\beta_2}} & \frac{1}{\sqrt{\beta_2}} \end{pmatrix} \begin{pmatrix} \cos \mu & \sin \mu \\ -\sin \mu & \cos \mu \end{pmatrix} \begin{pmatrix} \frac{1}{\sqrt{\beta_1}} & 0 \\ -\frac{\alpha_1}{\sqrt{\beta_1}} & \sqrt{\beta_1} \end{pmatrix}$$

The values of the Courant–Snyder parameters α_2 , β_2 , γ_2 at s_2 are related to α_1 , β_1 , γ_1 at s_1 by

$$\begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{2} = \begin{pmatrix} M_{11}^{2} & -2M_{11}M_{12} & M_{12}^{2} \\ -M_{11}M_{21} & M_{11}M_{22} + M_{12}M_{21} & -M_{12}M_{22} \\ M_{21}^{2} & -2M_{21}M_{22} & M_{22}^{2} \end{pmatrix} \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}_{1}$$

The evolution of the betatron amplitude function in a drift space is

$$\beta_{2} = \frac{1}{\gamma_{1}} + \gamma_{1}(s - \frac{\alpha_{1}}{\gamma_{1}})^{2} = \beta^{*} + \frac{(s - s^{*})^{2}}{\beta^{*}},$$

$$\alpha_{2} = \alpha_{1} - \gamma_{1}s = -\frac{(s - s^{*})}{\beta^{*}}, \quad \gamma_{2} = \gamma_{1} = \frac{1}{\beta^{*}}$$

Passing through a thin-lens quadrupole, the evolution of betatron function is

$$\beta_2 = \beta_1, \quad \alpha_2 = \alpha_1 + \frac{\beta_1}{f}, \quad \gamma_2 = \gamma_1 + \frac{2\alpha_1}{f} + \frac{\beta_1}{f^2}$$

$$X = \sqrt{2\beta J} \cos \psi, \quad X' = -\sqrt{\frac{2J}{\beta}} (\sin \psi + \alpha \cos \psi)$$

$$P_X = \beta X' + \alpha X = -\sqrt{2\beta J} \sin \psi$$

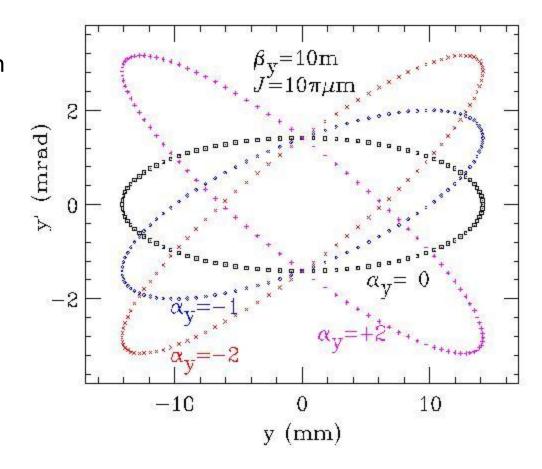
 (X,P_X) form a normalized phase space coordinates with $X^2+P_X^2=2\beta J$, here J is called **action**.

Courant-Snyder Invariant

$$\gamma X^{2} + 2\alpha X X' + \beta X'^{2} = \frac{1}{\beta} \left[X^{2} + (\alpha X + \beta X')^{2} \right] = 2J \equiv \varepsilon$$
Centroid

Centroid

Example: Ellipses (vertical) with different optical parameters



The betatron phase space ellipses of a particle with actions $J=10\pi$ mm-mrad. The btatron parameters are $\beta_y=10m$, and α_y shown by each curve. The scale for the ordinate y is mm, and y' in mrad. The betatron parameters for each ellipse are marked on the graph. All ellipses has the maximum y coordinate at $(2\beta_y J)^{1/2}$. The maximum anglular coordinate y' is $(2(1+\alpha_y^2)J/\beta_y)^{1/2}$. All ellipses have the same phase space area of 2J.

Courant-Snyder Invariant

$$\gamma X^{2} + 2\alpha X X' + \beta X'^{2} = \frac{1}{\beta} \left[X^{2} + (\alpha X + \beta X')^{2} \right] = 2J \equiv \varepsilon$$
Slope=-\alpha/\beta

Slope=-\alpha/\alpha

Slope=-\alpha/\beta

Slope=-\alpha/\beta

Slope=-\alpha/\beta

Slope=-\alpha/\beta

Slope=-\alpha/\beta

Emittance of a beam

Given a normalized distribution function $\rho(X, X')$ with $\int \rho(X, X') dX dX' = 1$, the moments of the beam distribution are

$$\begin{split} \left\langle X \right\rangle &= \int X \rho(X,X') dX dX', \quad \left\langle X' \right\rangle = \int X' \rho(X,X') dX dX', \\ \sigma_X^2 &= \int (X - \left\langle X \right\rangle)^2 \rho(X,X') dX dX', \quad \sigma_{X'}^2 = \int (X' - \left\langle X' \right\rangle)^2 \rho(X,X') dX dX', \\ \sigma_{XX'} &= \int (X - \left\langle X \right\rangle) (X' - \left\langle X' \right\rangle) \rho(X,X') dX dX' = r \sigma_X \sigma_{X'} \end{split}$$

Where σ_x and $\sigma_{x'}$ are the rms beam widths, $\sigma_{xx'}$ is the correlation, and r is the correlation coefficient. The rms beam emittance is then defined as

$$\varepsilon_{rms} = \sqrt{\sigma_X^2 \sigma_{X'}^2 - \sigma_{XX'}^2} = \sigma_X \sigma_{X'} \sqrt{1 - r^2}$$

The rms emittance is invariant in linear transport:

$$\varepsilon^{2} = \sigma_{X}^{2} \sigma_{X'}^{2} - \sigma_{XX'}^{2}$$

$$\sigma_{X}^{2} = \langle X^{2} \rangle - \langle X \rangle^{2}, \quad \sigma_{X'}^{2} = \langle X'^{2} \rangle - \langle X' \rangle^{2}, \quad \sigma_{XX'} = \langle XX' \rangle - \langle X \rangle \langle X' \rangle$$

we find

$$\frac{d\sigma_X^2}{ds} = 2\langle XX' \rangle - 2\langle X \rangle \langle X' \rangle$$

$$\frac{d\sigma_{X'}^2}{ds} = 2\langle X'X'' \rangle - 2\langle X' \rangle \langle X'' \rangle$$

$$\frac{d\sigma_{XX'}}{ds} = \langle X'^2 \rangle - \langle X' \rangle^2 - \langle X \rangle \langle X'' \rangle + \langle XX'' \rangle$$

$$X'' + KX = 0$$

$$\frac{d\varepsilon^2}{ds} = \sigma_X^2 \frac{d\sigma_{X'}^2}{ds} + \sigma_{X'}^2 \frac{d\sigma_X^2}{ds} - 2\sigma_{XX'} \frac{d\sigma_{XX'}}{ds} = 0$$

The σ -matrix is defined as

$$\sigma = \begin{pmatrix} \sigma_{11} & \sigma_{12} \\ \sigma_{12} & \sigma_{22} \end{pmatrix} = \begin{pmatrix} \sigma_y^2 & \sigma_{yy'} \\ \sigma_{yy'} & \sigma_{y'}^2 \end{pmatrix} = \langle (\mathbf{y} - \langle \mathbf{y} \rangle)(\mathbf{y} - \langle \mathbf{y} \rangle)^{\dagger} \rangle,$$

$$\sigma(s_2) = M(s_2|s_1)\sigma(s_1)M(s_2|s_1)^{\dagger}.$$

$$\epsilon_{rms} = \sqrt{\sigma_y^2 \sigma_{y'}^2 - \sigma_{yy'}^2} = \sigma_y \sigma_{y'} \sqrt{1 - r^2}.$$

If the beam distribution function is a function of the Courant-Snyder invariant, the σ -matrix is given by

$$\begin{pmatrix} \sigma_x^2 & \sigma_{xx'} \\ \sigma_{xx'} & \sigma_{x'}^2 \end{pmatrix} = \epsilon_{\rm rms} \begin{pmatrix} \beta & -\alpha \\ -\alpha & \gamma \end{pmatrix}.$$
 or
$$\mathbf{x}^\dagger \sigma^{-1} \mathbf{x} = \frac{1}{\epsilon_{\rm rms}} (\gamma x^2 + 2\alpha x x' + \beta x'^2).$$

Thus $\mathbf{y}^{\dagger} \boldsymbol{\sigma}^{-1} \mathbf{y}$ is invariant under linear transport systems. An invariant beam distribution is $\rho(y, y') = \rho(\mathbf{y}^{\dagger} \boldsymbol{\sigma}^{-1} \mathbf{y})$.

The Gaussian distribution function

The equilibrium beam distribution in the linearized betatron phase space may be any function of the invariant action. However, the Gaussian distribution function is commonly used to evaluate the beam properties. Expressing the normalized Gaussian distribution in the normalized phase space, we obtain

$$\rho(X, P_X) = \frac{1}{2\pi\sigma_X^2} e^{-(X^2 + P_X^2)/2\sigma_X^2}$$

where $\langle X^2 \rangle = \langle P_X^2 \rangle = \sigma_X^2 = \beta_X \epsilon_{rms}$ with an rms emittance ϵ_{rms} . Transforming (X, P_X) into the action-angle variables (J, ψ) with

$$X = \sqrt{2\beta J} \cos \psi$$
, $P_X = -\sqrt{2\beta J} \sin \psi$

The Jacobian of the transformation is β_x , and the distribution function becomes

$$\rho(J) = \frac{1}{\varepsilon_{rms}} e^{-J/\varepsilon_{rms}}, \quad \rho(\varepsilon) = \frac{1}{2\varepsilon_{rms}} e^{-\varepsilon/2\varepsilon_{rms}}$$

The percentage of particles contained within $\epsilon{=}n\epsilon_{rms}$ is $1-e^{-n/2}$

$\epsilon/\epsilon_{ m rms}$	2	4	6	8
Percentage in 1D [%]	63	86	95	98
Percentage in 2D [%]	40	74	90	96

The maximum phase-space area that particles can survive in an accelerator is called the *admittance*, or the *dynamic aperture*. The admittance is determined by the vacuum chamber size, the kicker aperture, and nonlinear magnetic fields.

Adiabatic damping and the normalized emittance: $\varepsilon_n = \varepsilon \beta \gamma$

The Courant–Snyder invariant, derived from the phase-space coordinate X, X', is not invariant when the energy is changed. To obtain the Liouville invariant phase-space area, we should use the conjugate phase-space coordinates (X, P_x) in Hamiltonian. Since $p_x = p_x' = mc\beta\gamma X'$, where m is the particle's mass, p is its momentum, and βγ is the Lorentz relativistic factor, the normalized emittance defined by $\varepsilon_n = \varepsilon \beta \gamma$ is invariant. The beam emittance decreases with increasing beam momentum, i.e. $\varepsilon = \varepsilon_n/\beta \gamma$. This is called *adiabatic damping*. Since the transverse velocity of a particle does not change during acceleration, the transverse angle $X' = p_x/p$ becomes smaller at a higher particle momentum. Thus the beam emittance $\varepsilon = \varepsilon_n/\beta \gamma$ decreases with energy. The adiabatic damping also applies to beam emittance in proton or electron linacs.

Because of the quantum fluctuation, The beam emittance in electron storage rings **increases** with energy ($\sim \gamma^2$). The corresponding normalized emittance is proportional to γ^3 .

Some simple examples:

- 1. Large colliders are normally made of arcs and insertion regions (IRs), where arcs are made of FODO cells for beam transport, and IRs are used for physics experiments. The IR matches all optical functions for special properties relevant to physics experiments.
- 2. Synchrotron radiation facilities are designed to minimize emittance and retain a straight section for IDs.
- 3. We examine the effect of edge angle in beam motion.

$$M_x = \begin{pmatrix} 1 & 0 \\ \frac{\tan \delta}{\rho} & 1 \end{pmatrix} \quad M_z = \begin{pmatrix} 1 & 0 \\ -\frac{\tan \delta}{\rho} & 1 \end{pmatrix}$$

The particle orbit enters and exits a *sector dipole* magnet perpendicular to the dipole edges. If the gradient function of the dipole is zero, i.e. $\partial Bz/\partial x = 0$, the transfer matrix is $(\cos \theta - \rho \sin \theta)$ (1)

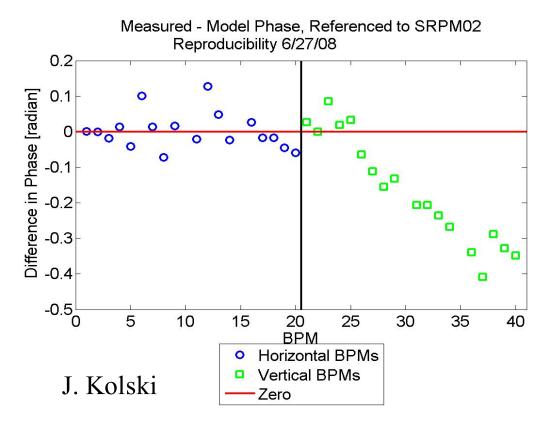
$$M_x = \begin{pmatrix} \cos \theta & \rho \sin \theta \\ -\frac{\sin \theta}{\rho} & \cos \theta \end{pmatrix}, \quad M_z = \begin{pmatrix} 1 & \ell \\ 0 & 1 \end{pmatrix}$$

where θ is the bending angle, ρ is the bending radius, and ℓ is the length of the dipole. A sector magnet gives rise to horizontal focusing. A rectangular dipole gives a transport matrix: $1 \rho \sin \theta$

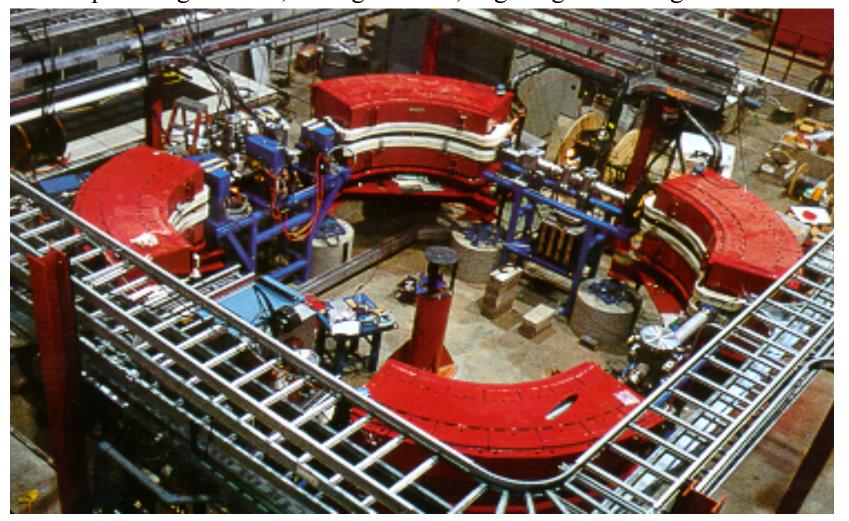
Three parameters that determine the edge focusing focal length: the edge angle (δ) , gap height (g), and the fringe field integral (FINT, κ).

$$-\frac{1}{f} = -\frac{1}{\rho} \tan(\delta - \psi) \qquad \psi = \frac{g\kappa}{\rho} \sec(\delta) (1 + \sin^2 \delta) \qquad \kappa = \int_{-\infty}^{\infty} \frac{B_y(s) (B_0 - B_y(s))}{gB_0^2} ds$$

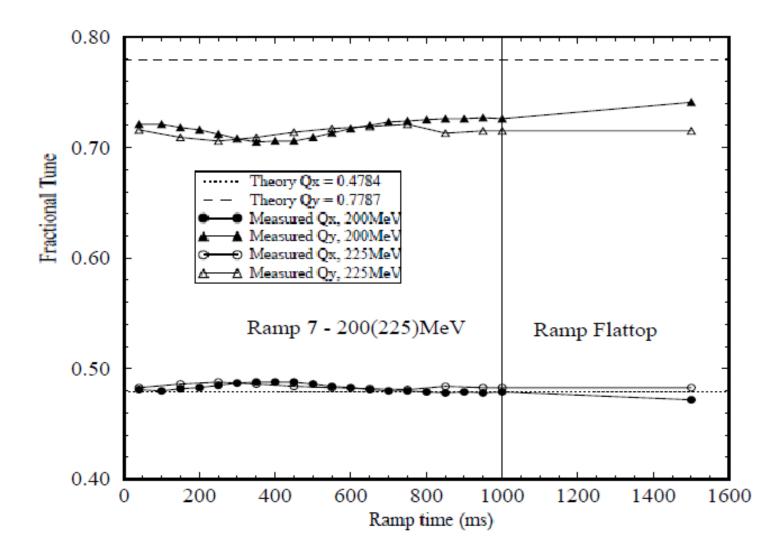
$$\psi = \kappa_1 \frac{g}{\rho} \frac{1 + \sin 2\delta}{\cos \delta} \left[1 - \kappa_2 \kappa_1 \frac{g}{\rho} \tan \delta \right]$$



CIS: Circumference = 17.364 m, Inj KE= 7 MeV, extraction: 240 MeV Dipole length = 2 m, 90 degree bend, edge angle = 12 deg.

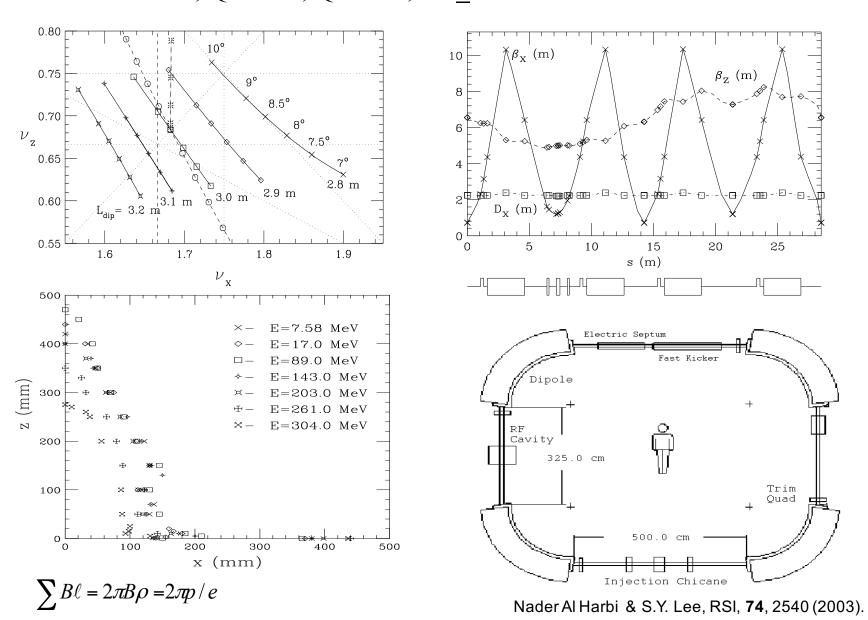


eCIS: No constraint on circumference (C=20m). Use CIS dipoles & cavity Need Damping wigglers, chicane, electrostatic kickers & septum



Xiaojian Kang (Ph.D. Thesis, 1998): Betatron tunes of CIS 200 & 225 MeV ramping

Ldip=3.0 m, ρ=1.91 m, Edge_angle=8.5° Circum=28.5 m, Qx=1.68, Qz=0.71, KE_tr=356 MeV



Low energy synchrotrons often rely on the bending radius $K_x=1/\rho^2$ for horizontal focusing and edge angles in dipoles for vertical focusing. Find the lattice property of the low energy synchrotron described by the following input data file (MAD). What is the effects of changing the edge angle and dipole length? Discuss the stability limit of the lattice.

```
TITLE,"CIS BOOSTER (1/5 Cooler), (90degDIP)"
! CIS = 1/5 of Cooler circumference = 86.82m / 5 = 17.364m
! It accelerates protons from 7 MeV to 200 MeV in 1-5 Hz.
LCELL:=4.341! cell length 17.364m/4
L1:=2.0! dipole length
L2:=LCELL-L1! straight section length
RHO:=1.27324
EANG:=12.*TWOPI/360! use rad. for edge angle
ANG := TWOPI/4
OO: DRIFT,L=L2
BD: SBEND, L=L1, ANGLE=ANG, E1=EANG, E2=EANG, K2=0.
SUP: LINE=(BD,OO)! a superperiod
USE, SUP, SUPER=4
PRINT,#S/E
TWISS, DELTAP=0.0, TAPE
STOP
```

Betatron motion: Effects of Linear Magnetic field Error

$$x'' + K_x(s)x = \frac{\Delta B_y}{B\rho}, \quad y'' + K_y(s)y = -\frac{\Delta B_x}{B\rho}$$

$$\Delta B_{y} + j\Delta B_{x} = B_{0} \sum_{n} (b_{n} + ja_{n})(x + jy)^{n},$$

$$B_{y} = B_{0}b_{0}, \quad B_{x} = B_{0}a_{0},$$

Dipole field error

$$B_{y} = B_{0}b_{1}x, \quad B_{x} = B_{0}b_{1}y,$$

$$B_{y} = -B_{0}a_{1}y, \quad B_{x} = B_{0}a_{1}x,$$

Quadrupole field error

Skew Quadrupole field error

$$B_y = B_0 b_2 (x^2 - y^2), \quad B_x = 2B_0 b_2 xy,$$

$$B_y = -2B_0 a_2 xy$$
, $B_x = B_0 a_2 (x^2 - y^2)$,

Sextupole field error

$$x'' + [K_x(s) + k(s)]x = \frac{b_0}{\rho}, \quad y'' + [K_y(s) - k(s)]y = -\frac{a_0}{\rho}$$

Effect of dipole field error:

We consider a single localized dipole error with the kick angle given by $\theta=\Delta B\ell/B\rho$. Because of the dipole field error, the reference orbit is perturbed! The idea is to find a new closed orbit that include the dipole field error.

$$X'' + K_X(s)X = \theta \delta(s - s_0)$$

The closed orbit is given by the following condition:

$$\begin{pmatrix} X_0 \\ X_0' - \theta \end{pmatrix} = M \begin{pmatrix} X_0 \\ X_0' \end{pmatrix} = \begin{pmatrix} \cos \Phi + \alpha_0 \sin \Phi & \beta_0 \sin \Phi \\ -\gamma_0 \sin \Phi & \cos \Phi - \alpha_0 \sin \Phi \end{pmatrix} \begin{pmatrix} X_0 \\ X_0' \end{pmatrix}$$

Where $\Phi=2\pi\nu$, ν is the betatron tune, the parameters α_0 , β_0 , and γ_0 are values of the Courant-Snyder parameters at the kicker location. The solution is

$$X_{0} = \frac{\beta_{0}\theta}{2\sin\pi\nu}\cos\pi\nu,$$

$$X_{0}' = \frac{\theta}{2\sin\pi\nu}(\sin\pi\nu - \alpha_{0}\cos\pi\nu)$$

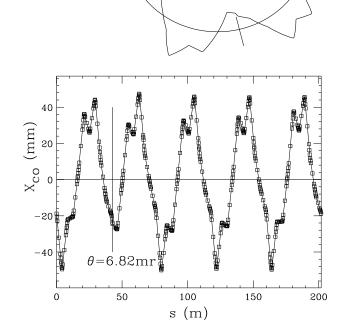
We have solved the closed orbit at one point s_0 . The closed orbit of the accelerator can be obtained by making mapping matrix:

$$\begin{pmatrix} X(s) \\ X'(s) \end{pmatrix}_{co} = M(s, s_0) \begin{pmatrix} X_0 \\ X'_0 \end{pmatrix} \qquad X_{co}(s) = G(s, s_0) \theta$$

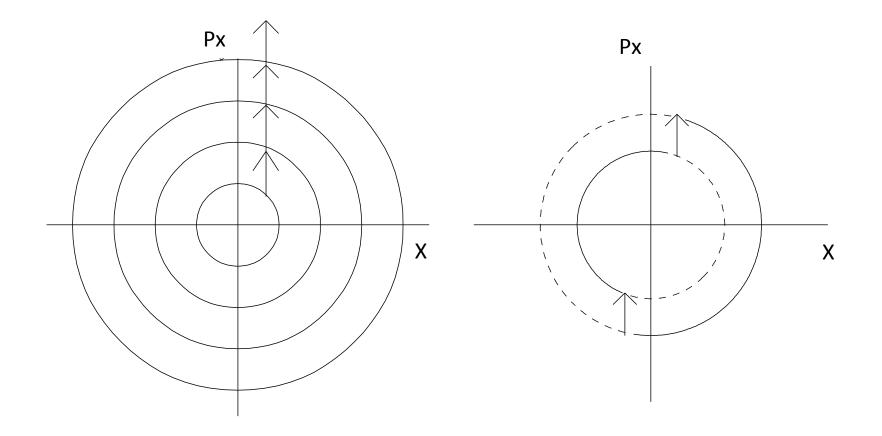
$$G(s, s_0) = \frac{\sqrt{\beta(s_0)\beta(s)}}{2\sin \pi v} \cos[\pi v - |\psi(s) - \psi(s_0)|]$$

Note that the closed orbit is described by Green's function. When the betatron tune is an integer, the closed orbit diverges. Each time, when the particle arrives the same location will receive a coherent kick and the particle becomes unstable.

How? And Why

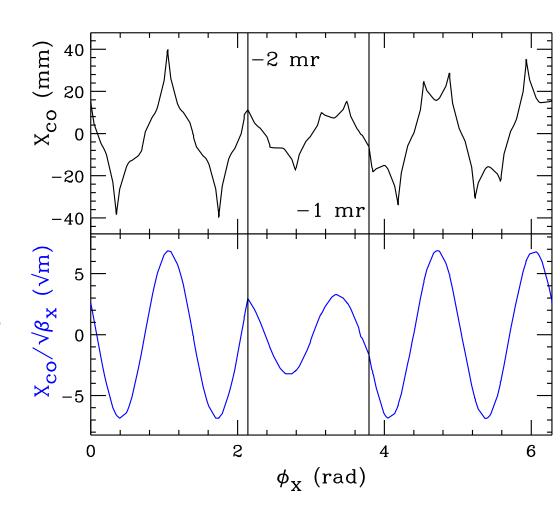


 $\theta = 6.82 \text{ mr}$



Left, a schematic plot of the closed-orbit perturbation due to an error dipole kick when the betatron tune is an integer. Here $p_X = \beta_X \Delta X' = \beta_X \theta$, where θ is the dipole kick angle and β_X is the betatron amplitude function value at the dipole. Right, a schematic plot of the particle trajectory resulting from a dipole kick when the betatron tune is a half-integer; here the angular kicks from two consecutive orbital revolutions cancel each other.

An accelerator with circumference 360 m is made of 18 FODO cells. The horizontal betatron tune of the synchrotron is v_x =4.8. If one of the 36 dipoles has an error of -2 mrad and another has error of -1 mrad.



TLS orbit vs dipole field error: Lecture note by C.C. Kuo (2002 OCPA Singapore)

