

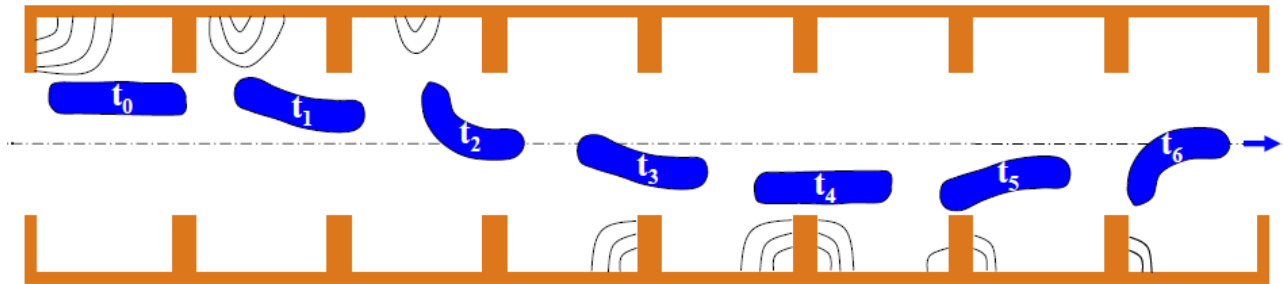
Collective Effects II: Examples of Collective Instabilities

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Outline

- Transverse beam breakup instability (BBU) in linear accelerator
 - Two particle model
 - BNS damping
- Longitudinal Robinson Instability ($m=0$)
 - Macro particle model
 - Resonator model for cavity impedance
 - Stability condition and growth rate

Single pass BBU (Two particle model)

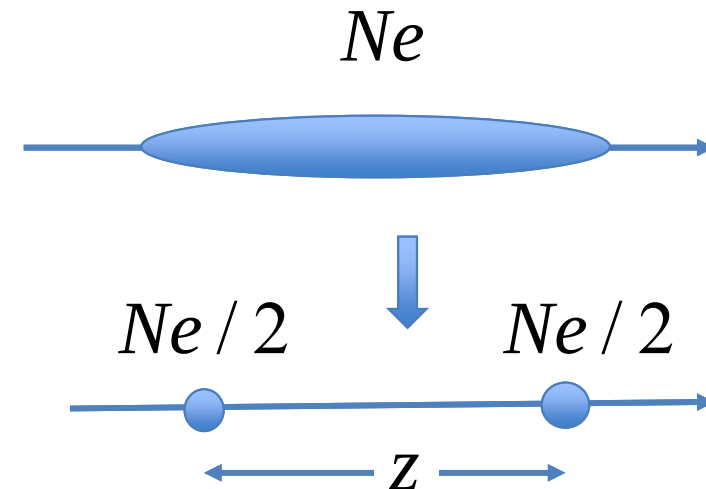


Leading particles $y_1(s) = \hat{y} \cos(k_\beta s)$

Trailing particles $y_2(s)'' + k_\beta^2 y_2(s) = \frac{Ne^2 W_1(z)}{2EL} y_1(s)$

$$= 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{2\gamma L} \hat{y} \cos(k_\beta s)$$

$$r_0 = \frac{1}{4\pi\epsilon_0} \frac{e^2}{mc^2}$$



*Note: our definition of the transverse wake function follow G. Stupakov's note and has a sign difference from that defined in A. Chao's book, i.e. W_1 here is $-W_1$ in Chao's book.

Driving term for particle 2

$$\vec{w}_i(x, y, s) = \frac{c}{qe} \Delta \vec{p}_\perp \quad q = \frac{Ne}{2}$$

$$m=1 \quad \vec{w}_i(r', r, \theta, s) = W_1(s) r' [\cos(\theta) \hat{r} - \sin(\theta) \hat{\theta}]$$

$$\Delta p_y = \frac{W_1(s) y_1 e}{c} \frac{Ne}{2} \quad \leftarrow \text{Transverse momentum change of particle 2 due to wakefield while it goes through the structure}$$

$$\Delta y' = \frac{\Delta p_y}{p_z} \approx \frac{c \Delta p_y}{E} = \frac{W_1(s) y_1 Ne^2}{2E} \quad \leftarrow \text{Transverse angle change of particle 2 due to wakefield}$$

$$\frac{\Delta y'}{L} = \frac{W_1(s) y_1 Ne^2}{2EL} \quad \leftarrow \text{Transverse angle changing rate of particle 2 due to wakefield, driving term}$$

Single pass BBU (Two particle model)

For a linear inhomogenous 2nd order differential equation

$$\frac{d^2 x}{dt^2} + a(t) \frac{dx}{dt} + b(t) x = f(t)$$

its solution is given by

$$W(t) = \begin{vmatrix} \phi_1(t) & \phi_2(t) \\ \phi_1'(t) & \phi_2'(t) \end{vmatrix}$$

$$x(t) = c_1 \phi_1(t) + c_2 \phi_2(t) + \int_{t_0}^t \frac{\phi_1(\xi) \phi_2(t) - \phi_2(\xi) \phi_1(t)}{W(\xi)} f(\xi) d\xi$$

$$y_{2,inh}(s) = 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{2\gamma L k_\beta} \hat{y} \int_0^s \sin(k_\beta s - k_\beta \xi) \cos(k_\beta \xi) d\xi$$

$$\phi_2 = \sin(k_\beta s) \quad \phi_1 = \cos(k_\beta s)$$

$$= 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{2\gamma L k_\beta} \hat{y} \frac{1}{2} \left[s \sin(k_\beta s) - \int_{-s/2}^{s/2} \sin(2k_\beta \tilde{\xi}) d\tilde{\xi} \right]$$

$$\tilde{\xi} \equiv \xi - \frac{s}{2}$$

$$W(t) = \begin{vmatrix} \cos(k_\beta s) & \sin(k_\beta s) \\ -k_\beta \sin(k_\beta s) & k_\beta \cos(k_\beta s) \end{vmatrix} = k_\beta$$

$$= 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{4\gamma L k_\beta} \hat{y} s \sin(k_\beta s)$$

$$y_2(s)'' + k_\beta^2 y_2(s) = 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{2\gamma L} \hat{y} \cos(k_\beta s)$$

Single pass BBU (Two particle model)

$$y_2(s) = c_1 \cos(k_\beta s) + c_2 \sin(k_\beta s) + 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{4\gamma L k_\beta} \hat{y} s \sin(k_\beta s)$$

Noticing that before going through the structure, particle 2 has the same trajectory as that of Particle 1, i.e.

$$y_2(0) = y_1(0) = \hat{y} \cos(0) = \hat{y}$$

$$y_2'(0) = y_1'(0) = -\hat{y} k_\beta \sin(0) = 0$$

We obtain $c_1 = \hat{y}$ and $c_2 = 0$. Thus the solution for particle 2 is

$$y_2(s) = \hat{y} \left[\cos(k_\beta s) + 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{4k_\beta \gamma L} s \sin(k_\beta s) \right]$$

$$y_1(s) = \hat{y} \cos(k_\beta s)$$

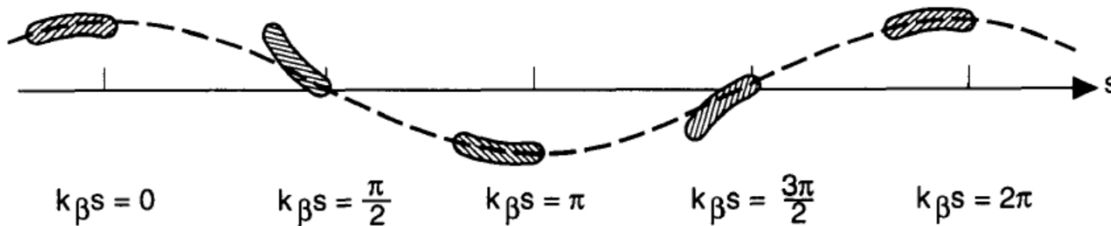
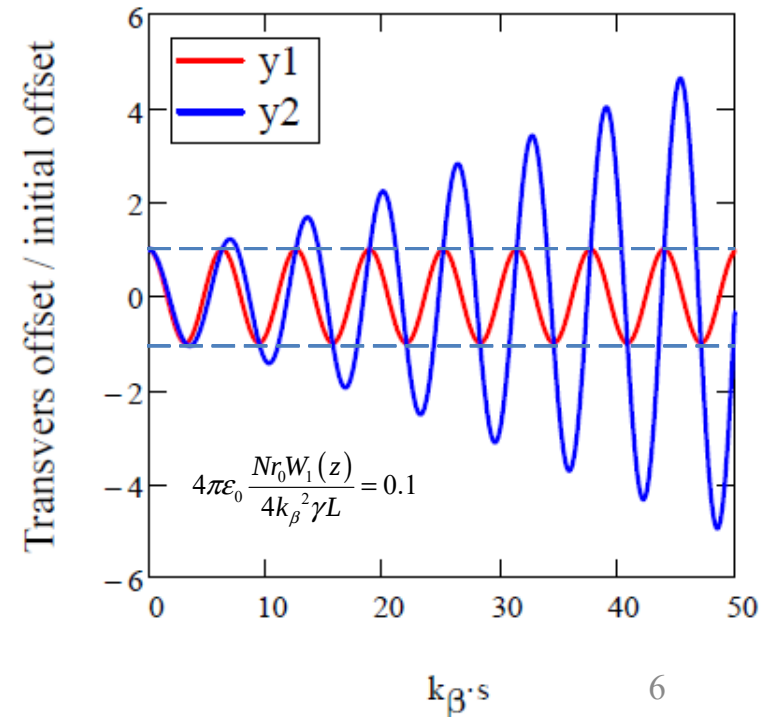


Figure 3.3. Sequence of snapshots of a beam undergoing dipole beam breakup instability in a linac. Values of $k_\beta s$ indicated are modulo 2π . The dashed curves indicate the trajectory of the bunch head.



Single pass BBU II

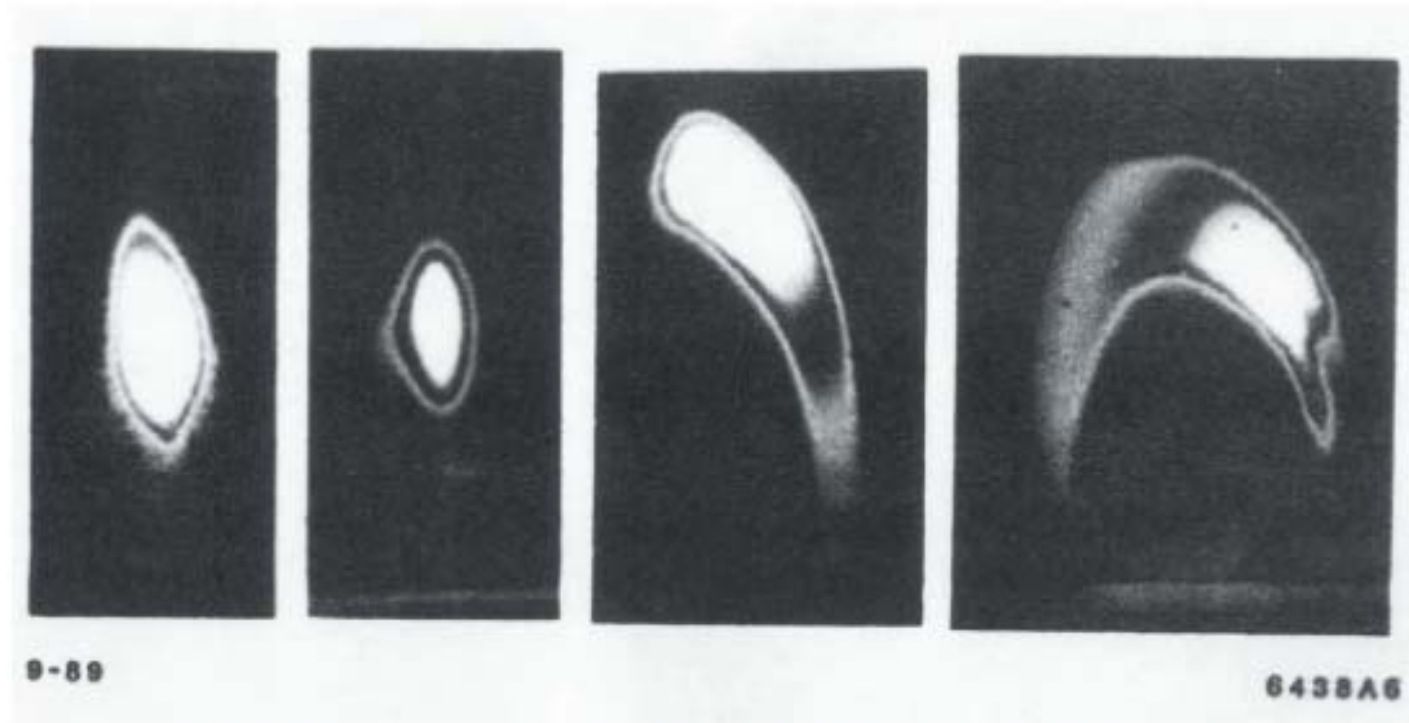


Figure 4.4: Four transverse beam profiles observed at the end of the SLAC linac are shown when the beam was carefully injected, and injected with 0.2, 0.5, and 1 mm offsets. The beam sizes σ_x and σ_y are about $120 \mu\text{m}$. (Courtesy John Seeman, 1991)

One possible cure: Balakin-Novokhatsky-Smirnov (BNS) damping

Introduce focusing variation along the bunch, i.e. head and tail have different focusing strength

$$y_2'' + (k_\beta + \Delta k_\beta)^2 y_2 = 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{2\gamma L} \hat{y} \cos(k_\beta s)$$

$$\tilde{k}_\beta \equiv k_\beta + \Delta k_\beta$$

$$\phi_2 = \sin(\tilde{k}_\beta s) \quad \phi_1 = \cos(\tilde{k}_\beta s)$$

$$y_{2,inh}(s) = 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{2\gamma L \tilde{k}_\beta} \hat{y} \int_0^s \sin(\tilde{k}_\beta s - \tilde{k}_\beta \xi) \cos(k_\beta \xi) d\xi$$

$$W(t) = \tilde{k}_\beta$$

$$= -4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{2\gamma L \tilde{k}_\beta} \hat{y} \frac{1}{2} \left[\int_0^s \sin\left(\Delta k_\beta \left(\xi - \frac{\tilde{k}_\beta}{\Delta k_\beta} s\right)\right) d\xi + \int_0^s \sin\left((\tilde{k}_\beta + k_\beta) \left(\xi - \frac{\tilde{k}_\beta}{\tilde{k}_\beta + k_\beta} s\right)\right) d\xi \right]$$

$$= 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{2\gamma L \tilde{k}_\beta} \hat{y} \frac{1}{2} \left[\frac{1}{\Delta k_\beta} + \frac{1}{\tilde{k}_\beta + k_\beta} \right] [\cos(k_\beta s) - \cos(\tilde{k}_\beta s)]$$

$$\approx -4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{4\gamma L k_\beta \Delta k_\beta} \hat{y} [\cos(\tilde{k}_\beta s) - \cos(k_\beta s)] \quad \leftarrow \text{assume } \Delta k_\beta / k_\beta \ll 1$$

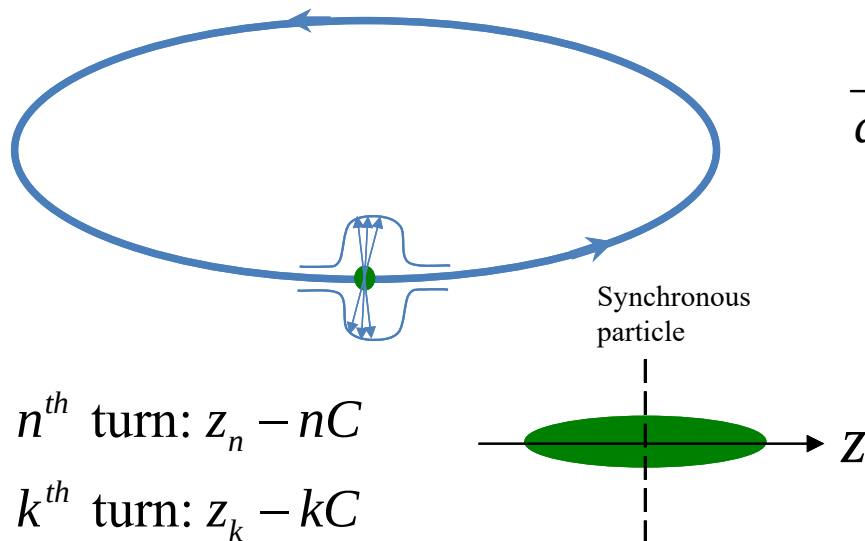
$$y_2(s) = \hat{y} \cos((k_\beta + \Delta k_\beta)s) - 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{4\gamma L k_\beta \Delta k_\beta} \hat{y} [\cos(\tilde{k}_\beta s) - \cos(k_\beta s)]$$

Condition for complete compensation:

$$4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{4\gamma L k_\beta \Delta k_\beta} = 1 \Rightarrow \Delta k_\beta = 4\pi\epsilon_0 \frac{Nr_0 W_1(z)}{4\gamma L k_\beta} \Rightarrow \boxed{y_2(s) = \hat{y} \cos(k_\beta s)}$$

Robinson Instability in Circular Machine

- As a charged particle bunch traveling through a cavity, it excites E&M fields, i.e. wakefields. To the leading order in the longitudinal direction, i.e. $m=0$, particles in the bunch lose some of their energies to the cavity, which is on top of the energy they gain from the acceleration (superposition).



$$\frac{dz_n}{dn} = -\eta C \delta_n$$

$$\text{Phase slip factor: } \eta \equiv \frac{1}{\gamma_{tr}^2} - \frac{1}{\gamma^2}$$

$$\frac{d}{dn} \delta_n = \frac{(2\pi\nu_s)^2}{\eta C} z_n + \frac{eV(z_n)}{E}$$

$$= \frac{(2\pi\nu_s)^2}{\eta C} z_n - \frac{4\pi\epsilon_0 N r_0}{\gamma} \sum_{k=-\infty}^n W_0'(z_n - nC - z_k + kC)$$

$$r_0 = \frac{1}{4\pi\epsilon_0} \frac{e^2}{mc^2}$$

z is in the range of bunch length, i.e. $z \ll C$

Robinson Instability II

$$\begin{aligned} \frac{d^2 z_n}{dn^2} + (2\pi\nu_s)^2 z_n &= \frac{4\pi\epsilon_0\eta CNr_0}{\gamma} \sum_{k=-\infty}^n W_0'(kC - nC + z_n - z_k) \\ &\approx \frac{4\pi\epsilon_0\eta CNr_0}{\gamma} \sum_{k=-\infty}^n W_0'(kC - nC) \\ &\quad + \frac{4\pi\epsilon_0\eta CNr_0}{\gamma} \sum_{k=-\infty}^n (z_n - z_k) W_0''(kC - nC) \end{aligned}$$

The first term in the RHS can be removed by defining

$$\tilde{z}_n \equiv z_n + \frac{4\pi\epsilon_0\eta CNr_0}{\gamma(2\pi\nu_s)^2} \sum_{k=-\infty}^n W_0'(kC - nC)$$

Please notice that $\sum_{k=-\infty}^n W_0'(kC - nC) = \sum_{\tilde{k}=-\infty}^0 W_0'(\tilde{k}C)$,
i.e. independent of n $\tilde{k} \equiv k - n$

$$\frac{d^2 \tilde{z}_n}{dn^2} + (2\pi\nu_s)^2 \tilde{z}_n \approx \frac{4\pi\epsilon_0\eta CNr_0}{\gamma} \sum_{k=-\infty}^n (\tilde{z}_n - \tilde{z}_k) W_0''(kC - nC)$$

Robinson Instability III

Ansatz (test solution): $\tilde{z}_n = A \exp(-in\Omega T_0)$

$$\frac{d^2 \tilde{z}_n}{dn^2} + (2\pi\nu_s)^2 \tilde{z}_n \approx \frac{4\pi\epsilon_0 \eta C N r_0}{\gamma} \sum_{k=-\infty}^n (\tilde{z}_n - \tilde{z}_k) W_0''(kC - nC)$$

$$\begin{aligned} (-i\Omega T_0)^2 + (2\pi\nu_s)^2 &= \frac{4\pi\epsilon_0 \eta C N r_0}{\gamma} \sum_{k=-\infty}^n (1 - \exp(-i(k-n)\Omega T_0)) W_0''(kC - nC) \\ &= \frac{4\pi\epsilon_0 \eta C N r_0}{\gamma} \sum_{\tilde{k}=-\infty}^0 (1 - \exp(-i\tilde{k}\Omega T_0)) W_0''(\tilde{k}C); & \text{Causality: } W'(\Delta z > 0) = 0 \\ \tilde{k} \equiv k - n & & z = ct - s \\ &= \frac{4\pi\epsilon_0 \eta C N r_0}{\gamma} \sum_{k=-\infty}^{\infty} (1 - \exp(-ik\Omega T_0)) W_0''(kC) \end{aligned}$$

$$\Omega^2 - \omega_s^2 = -\frac{4\pi\epsilon_0 \eta N r_0 c}{\gamma T_0} \sum_{k=-\infty}^{\infty} (1 - \exp(-ik\Omega T_0)) W_0''(kC); \quad \omega_s = \frac{2\pi\nu_s}{T_0}$$

Robinson Instability IV

We will use the following identity (the Poisson Sum Formula)

$$\sum_{l=-\infty}^{\infty} F(lC) = \frac{1}{C} \sum_{p=-\infty}^{\infty} \tilde{F}\left(\frac{2\pi p}{C}\right) \quad F(z) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{ikz} \tilde{F}(k) dk \quad \tilde{F}(k) = \int_{-\infty}^{\infty} e^{-ikz} F(z) dz$$

$$\begin{aligned} \Omega - \omega_s &\approx -\frac{4\pi\epsilon_0\eta Nr_0 c}{\gamma T_0 2\omega_s} \sum_{k=-\infty}^{\infty} (1 - \exp(-ik\Omega T_0)) W_0''(kC) \\ &= -\frac{4\pi\epsilon_0\eta Nr_0 c}{\gamma T_0 2\omega_s} \left\{ \sum_{k=-\infty}^{\infty} W_0''(kC) - \sum_{k=-\infty}^{\infty} G(kC) \right\} \quad G(kC) \equiv \exp\left(-i\frac{\Omega}{c}kC\right) W_0''(kC) \\ &= -\frac{4\pi\epsilon_0\eta Nr_0 c}{\gamma T_0 2\omega_s C} \left\{ \sum_{p=-\infty}^{\infty} \tilde{W}_0''\left(\frac{2\pi p}{C}\right) - \sum_{p=-\infty}^{\infty} \tilde{G}\left(\frac{2\pi p}{C}\right) \right\} \\ &\approx -i \frac{4\pi\epsilon_0\eta Nr_0}{2\gamma T_0^2 \omega_s} \sum_{p=-\infty}^{\infty} \left\{ p\omega_0 Z_{0, //}(p\omega_0) - (p\omega_0 + \omega_s) Z_{0, //}(p\omega_0 + \omega_s) \right\} \end{aligned}$$

Deriving first term in bracket

$$\begin{aligned}
 \tilde{W}_0''\left(\frac{2\pi p}{C}\right) &= \int_{-\infty}^{\infty} e^{-i\frac{2\pi p}{C}z} W_0''(z) dz \\
 &= \int_{-\infty}^{\infty} e^{-i\frac{2\pi p}{C}z} \frac{d}{dz} W_0'(z) dz \\
 &= \int_{-\infty}^{\infty} \frac{d}{dz} \left[e^{-i\frac{2\pi p}{C}z} W_0'(z) \right] dz - \int_{-\infty}^{\infty} W_0'(z) \frac{d}{dz} e^{-i\frac{2\pi p}{C}z} dz \\
 &= i \frac{2\pi p}{C} \int_{-\infty}^{\infty} W_0'(z) e^{-i\frac{2\pi p}{C}z} dz \\
 &= i \frac{p}{C} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} d\omega e^{i\omega \frac{z}{c}} Z_{0, //}(\omega) e^{-i\frac{2\pi p}{C}z} dz \\
 &= i \frac{p}{C} \int_{-\infty}^{\infty} d\omega Z_{0, //}(\omega) \int_{-\infty}^{\infty} e^{iz\left(\frac{\omega}{c} - \frac{2\pi p}{C}\right)} dz \\
 &= i \frac{cp}{C} 2\pi \int_{-\infty}^{\infty} d\omega Z_{0, //}(\omega) \delta\left(\omega - \frac{2\pi pc}{C}\right) \\
 &= ip\omega_0 Z_{0, //}(p\omega_0)
 \end{aligned}$$

$$W_0'(z) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{i\omega \frac{z}{c}} Z_{0, //}(\omega) d\omega$$

$$\begin{aligned}
\tilde{G}\left(\frac{2\pi p}{C}\right) &= \int_{-\infty}^{\infty} e^{-i\frac{2\pi p}{C}z} \exp\left(-i\frac{\Omega}{C}z\right) W_0''(z) dz \\
&= \int_{-\infty}^{\infty} e^{-i\left(\frac{2\pi p}{C} + \frac{\Omega}{C}\right)z} \frac{d}{dz} W_0'(z) dz \\
&= \int_{-\infty}^{\infty} e^{-i\frac{2\pi p'}{C}z} \frac{d}{dz} W_0'(z) dz; \quad p' = p + \frac{\Omega C}{2\pi} \\
&= \int_{-\infty}^{\infty} \frac{d}{dz} \left[e^{-i\frac{2\pi p'}{C}z} W_0'(z) \right] dz - \int_{-\infty}^{\infty} W_0'(z) \frac{d}{dz} e^{-i\frac{2\pi p'}{C}z} dz \\
&= i \frac{2\pi p'}{C} \int_{-\infty}^{\infty} W_0'(z) e^{-i\frac{2\pi p'}{C}z} dz \\
&= i \frac{p'}{C} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} d\omega e^{i\omega \frac{z}{C}} Z_{0, //}(\omega) e^{-i\frac{2\pi p'}{C}z} dz \\
&= i \frac{p'}{C} \int_{-\infty}^{\infty} d\omega Z_{0, //}(\omega) \int_{-\infty}^{\infty} e^{iz\left(\frac{\omega}{C} - \frac{2\pi p'}{C}\right)} dz \\
&= i \frac{cp'}{C} 2\pi \int_{-\infty}^{\infty} d\omega Z_{0, //}(\omega) \delta\left(\omega - \frac{2\pi p'c}{C}\right) \\
&= ip' \omega_0 Z_{0, //}(p' \omega_0) \\
&= i(p\omega_0 + \Omega) Z_{0, //}(p\omega_0 + \Omega) \\
&\approx i(p\omega_0 + \omega_s) Z_{0, //}(p\omega_0 + \omega_s)
\end{aligned}$$

Deriving second term
in bracket

$$W_0'(z) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{i\omega \frac{z}{C}} Z_{0, //}(\omega) d\omega$$

Robinson Instability IV

We will use the following identity (the Poisson Sum Formula)

$$\sum_{l=-\infty}^{\infty} F(lC) = \frac{1}{C} \sum_{p=-\infty}^{\infty} \tilde{F}\left(\frac{2\pi p}{C}\right) \quad F(z) = \frac{1}{2\pi} \int_{-\infty}^{\infty} e^{ikz} \tilde{F}(k) dk \quad \tilde{F}(k) = \int_{-\infty}^{\infty} e^{-ikz} F(z) dz$$

$$\begin{aligned} \Omega - \omega_s &\approx -\frac{4\pi\epsilon_0\eta Nr_0 c}{\gamma T_0 2\omega_s} \sum_{k=-\infty}^{\infty} (1 - \exp(-ik\Omega T_0)) W_0''(kC) \\ &\approx -i \frac{4\pi\epsilon_0\eta Nr_0}{2\gamma T_0^2 \omega_s} \sum_{p=-\infty}^{\infty} \{ p\omega_0 Z_{0, //}(p\omega_0) - (p\omega_0 + \omega_s) Z_{0, //}(p\omega_0 + \omega_s) \} \end{aligned}$$

 $\text{Re}[Z_{0, //}(p\omega_0)]$ is an even function of p .

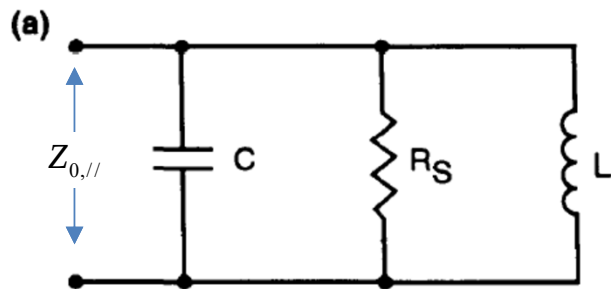
$$\tau^{-1} = \text{Im}(\Omega) = \frac{4\pi\epsilon_0\eta Nr_0}{2\gamma T_0^2 \omega_s} \sum_{p=-\infty}^{\infty} (p\omega_0 + \omega_s) \text{Re}\{Z_{0, //}(p\omega_0 + \omega_s)\}$$

Impedance Model for Fundamental mode of a Cavity

$$\frac{1}{Z_{0,//}} = \frac{1}{R_s} + \frac{i}{\omega L} - i\omega C$$

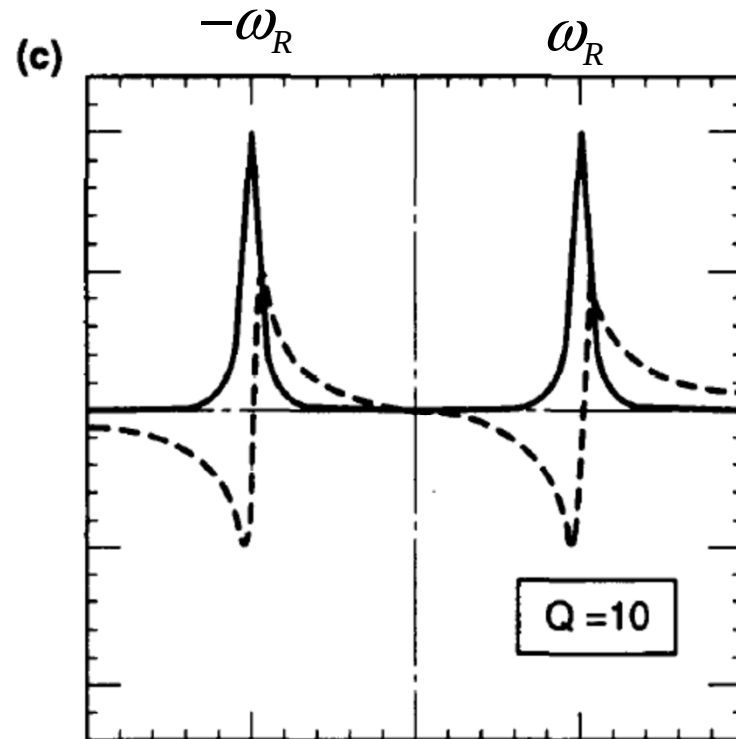
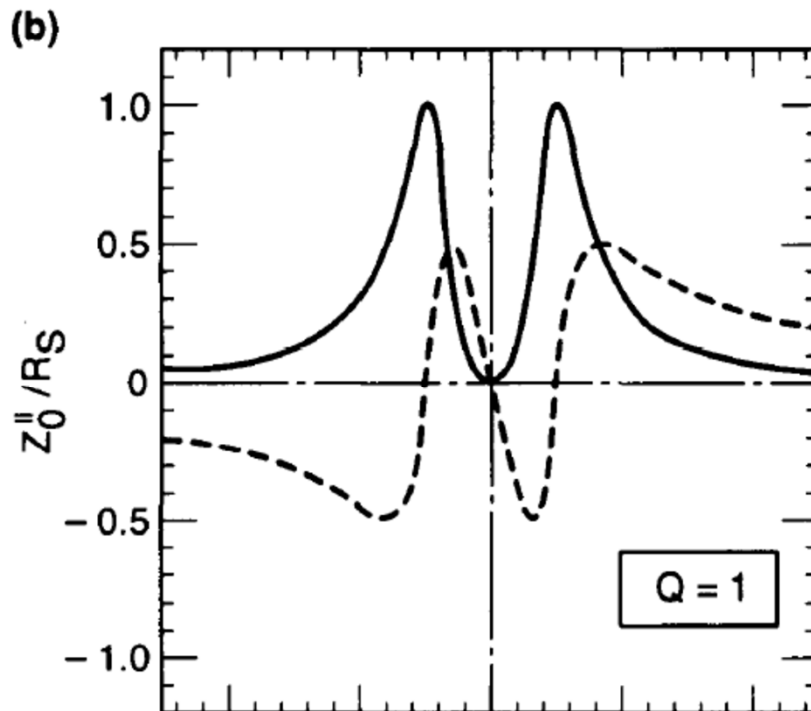


$$Z_{0,//} = \frac{R_s}{1 + iQ \left(\frac{\omega_R}{\omega} - \frac{\omega}{\omega_R} \right)}$$



For RF cavity, $\omega_R / Q \ll \omega_0$, and hence only the two term in the summation over p matters, i.e.

$$p = \pm h \approx \pm \frac{\omega_R}{\omega_0}$$



Robinson Instability V

$$\tau^{-1} = \frac{4\pi\epsilon_0\eta N r_0}{2\gamma T_0^2 \omega_s} \left\{ (h\omega_0 + \omega_s) \operatorname{Re} [Z_{0, //} (h\omega_0 + \omega_s)] + (-h\omega_0 + \omega_s) \operatorname{Re} [Z_{0, //} (h\omega_0 - \omega_s)] \right\}$$

$$\approx \frac{4\pi\epsilon_0\eta N r_0 h\omega_0}{2\gamma T_0^2 \omega_s} \left\{ \operatorname{Re} [Z_{0, //} (h\omega_0 + \omega_s)] - \operatorname{Re} [Z_{0, //} (h\omega_0 - \omega_s)] \right\} \quad \leftarrow \quad Z_{0, //} = \frac{R_s}{1 + iQ \left(\frac{\omega_R}{\omega} - \frac{\omega}{\omega_R} \right)}$$

For ω_s and $\Delta\omega \ll \frac{\omega_R}{2Q} \ll \omega_0$, the growth rate is

$$\tau^{-1} \approx 4\pi\epsilon_0 \frac{4N r_0 \eta R_s Q^2}{\pi\gamma T_0 h} \Delta\omega$$

$$\Delta\omega \equiv \omega_R - h\omega_0$$

$$\operatorname{Re} [Z_{0, //} (h\omega_0 + \omega_s)] - \operatorname{Re} [Z_{0, //} (h\omega_0 - \omega_s)]$$

$$= 16 \frac{Q^2 R_s}{h^2 \omega_0^2} \omega_s \Delta\omega$$

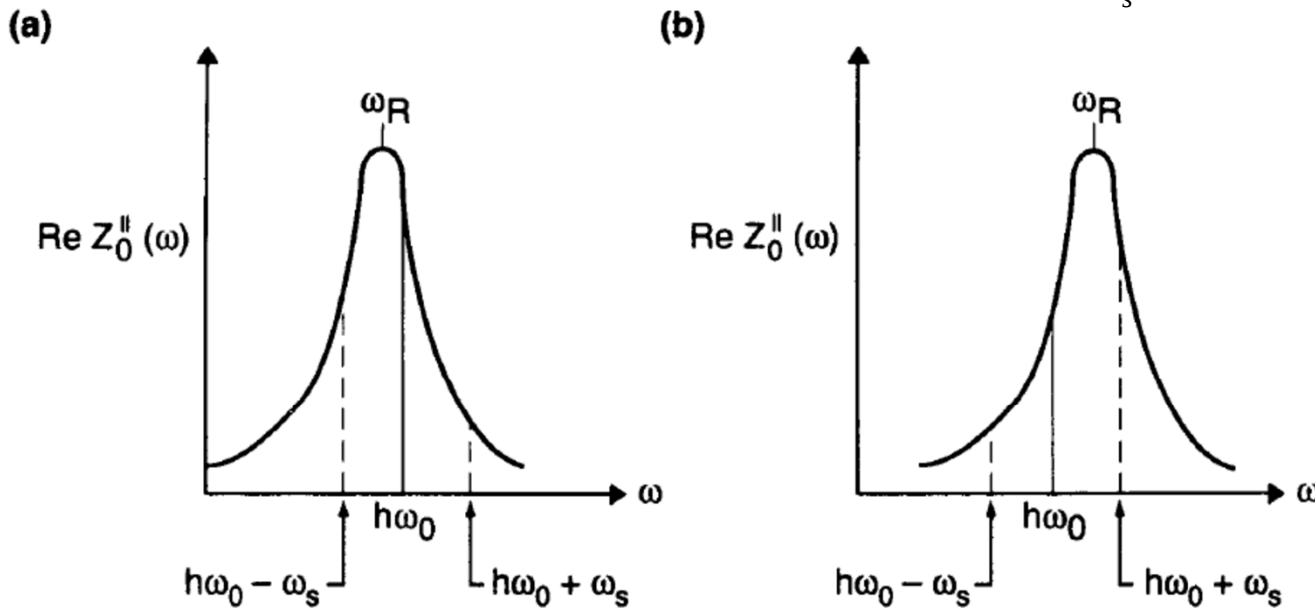


Figure 4.4. Illustration of the Robinson stability criterion. The rf fundamental mode is detuned so that ω_R is (a) slightly below $h\omega_0$ and (b) slightly above $h\omega_0$. (a) is Robinson damped above transition and antidamped below transition. (b) is antidamped above transition and damped below transition.

Derivation of the subtraction of impedance

$$Z_{0, //} = \frac{R_s}{1 + iQ \left(\frac{\omega_R}{\omega} - \frac{\omega}{\omega_R} \right)} \quad \Delta\omega \equiv \omega_R - h\omega_0$$

$$\begin{aligned} \operatorname{Re}[Z_{0, //} (h\omega_0 + \omega_s)] &= \operatorname{Re} \left\{ \frac{R_s}{1 + iQ \left(\frac{\omega_R}{h\omega_0 + \omega_s} - \frac{h\omega_0 + \omega_s}{\omega_R} \right)} \right\} \\ &= \frac{R_s}{1 + 4Q^2 \left(\frac{(\Delta\omega - \omega_s)}{h\omega_0} \right)^2} \\ &= R_s \left(1 - 4Q^2 \frac{(\Delta\omega - \omega_s)^2}{h^2 \omega_0^2} \right) \end{aligned}$$

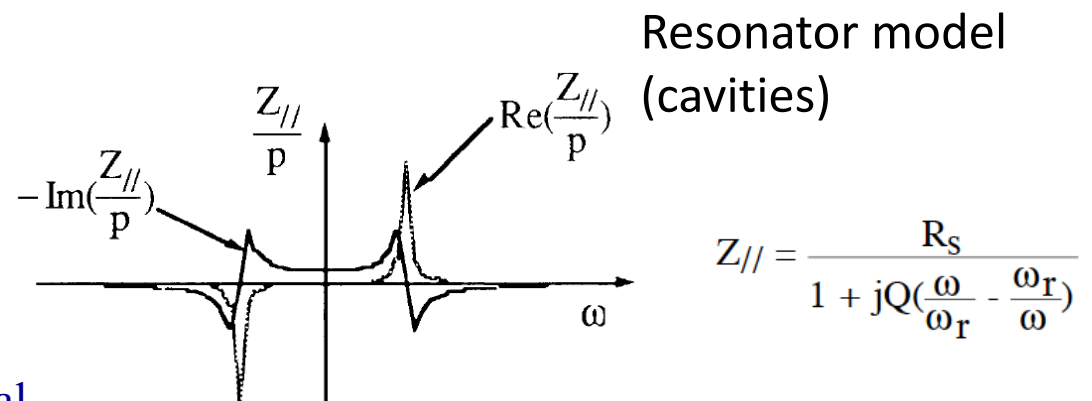
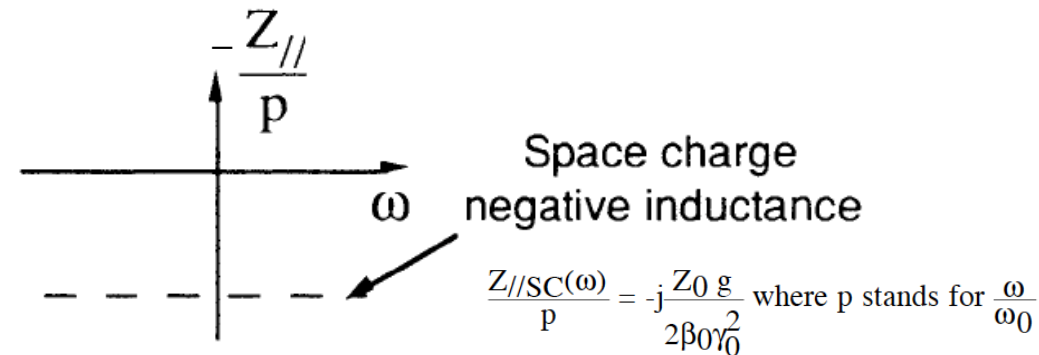
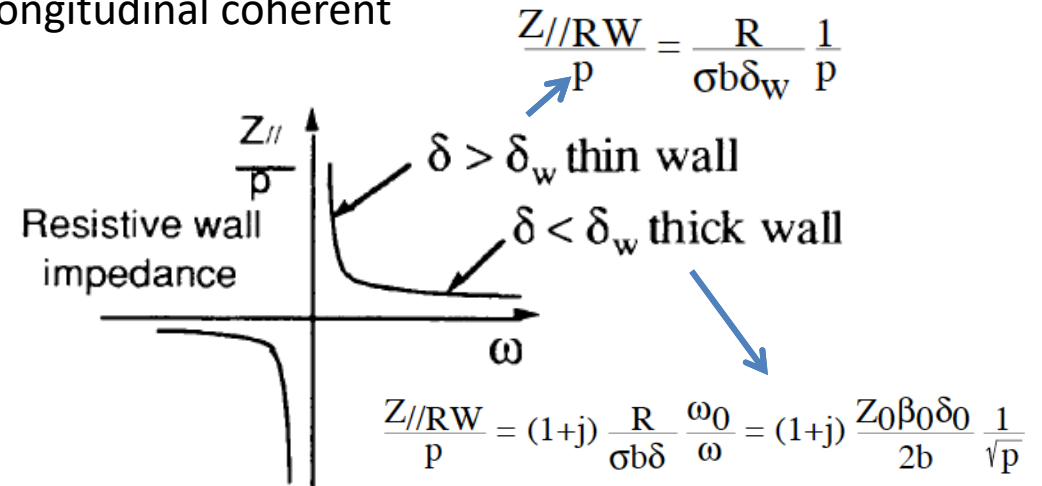
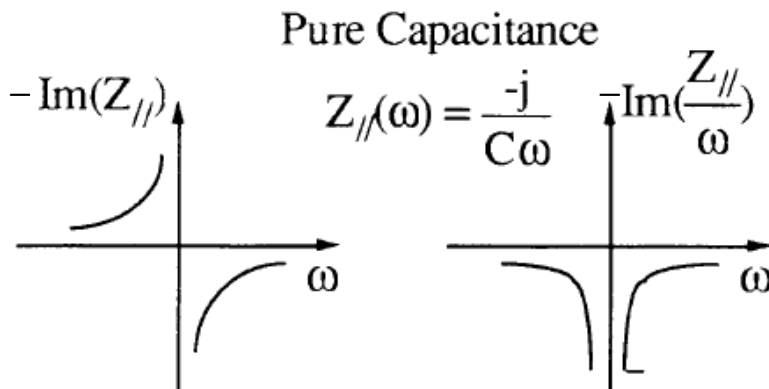
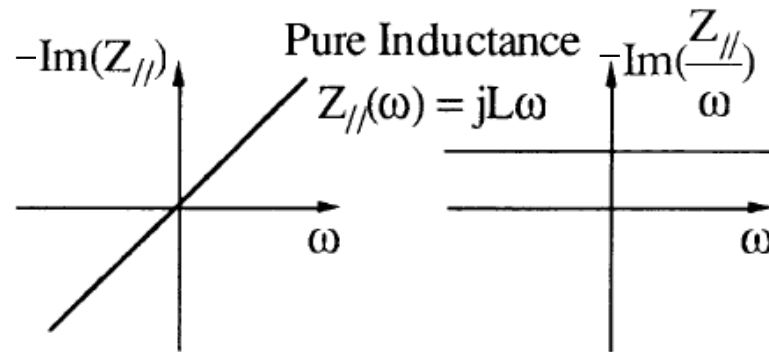
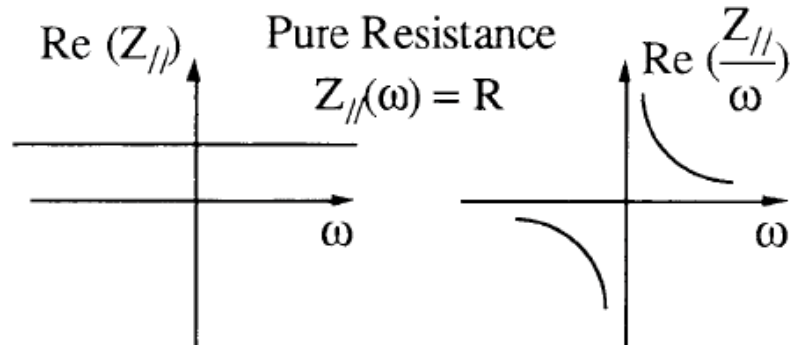
$$\begin{aligned} \operatorname{Re}[Z_{0, //} (h\omega_0 - \omega_s)] &= \operatorname{Re} \left\{ \frac{R_s}{1 + iQ \left(\frac{\omega_R}{h\omega_0 - \omega_s} - \frac{h\omega_0 - \omega_s}{\omega_R} \right)} \right\} \\ &= \frac{R_s}{1 + 4Q^2 \left(\frac{(\Delta\omega + \omega_s)}{h\omega_0} \right)^2} \\ &= R_s \left(1 - 4Q^2 \frac{(\Delta\omega + \omega_s)^2}{h^2 \omega_0^2} \right) \end{aligned}$$

$$\operatorname{Re}[Z_{0, //} (h\omega_0 + \omega_s)] - \operatorname{Re}[Z_{0, //} (h\omega_0 - \omega_s)] = 16 \frac{Q^2 R_s}{h^2 \omega_0^2} \omega_s \Delta\omega$$

Typical Longitudinal Impedance

$$j = -i$$

Taken from 'Coasting beam longitudinal coherent instabilities' by J.L. Laclare



Many pictures and derivations used in the slides are taken from the following references:

- [1] ‘Accelerator Physics’ by S.Y. Lee;
- [2] ‘Physics of Collective Beam Instabilities in High Energy Accelerators’ by A. Chao;
- [3] ‘Coasting beam longitudinal coherent instabilities’ by J.L. Laclare

What we learned today

- In linear accelerator, **single bunch transverse beam break up instability** can develop if the bunches are not carefully injected and machine transverse wake function / impedance is large. Such an instability can be compensated by introducing focusing variation along the bunch, i.e. **BNS damping**.
- In circular machine, the leading order ($m=0$) longitudinal wakefield in the cavity can cause Robinson instability. The cavity resonant frequency should be detuned away from exact harmonics of the revolution frequency to avoid such instability: above transition, the resonant frequency should be slightly below $h\omega_0$; and below transition the resonant frequency should be slightly above $h\omega_0$.